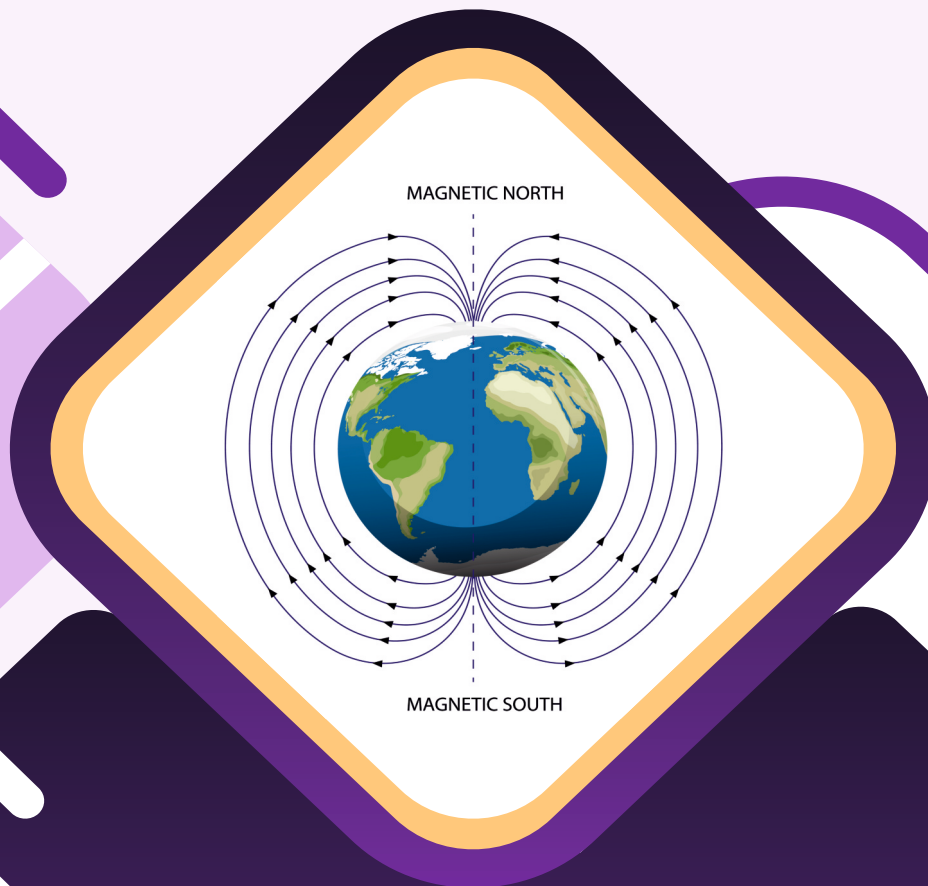




GATE | PSUs



Electrical Engineering

ELECTROMAGNETIC FIELDS

Text Book: Theory with worked out Examples and Practice Questions

Chapter 1 Static Fields & Maxwell's Equations

(Solutions for Text Book Practice Questions)

01. Ans: 1

Sol: $\vec{V} = x \cos^2 y \hat{i} + x^2 e^z \hat{j} + z \sin^2 y \hat{k}$

$$= x \cos^2 y \hat{a}_x + x^2 e^z \hat{a}_y + z \sin^2 y \hat{a}_z$$

From divergence theorem

$$\oint_V \vec{V} \cdot \hat{n} \, ds = \int_V (\nabla \cdot \vec{D}) \, dv \dots\dots\dots 1$$

$$\nabla \cdot \vec{D} = \frac{\partial}{\partial x}(x \cos^2 y) + \frac{\partial}{\partial y}(x^2 e^z) + \frac{\partial}{\partial z}(z \sin^2 y)$$

$$= \cos^2 y + \sin^2 y = 1$$

$$dv = dx dy dz$$

Putting these value in equation 1 we have

$$\oint_V \vec{V} \cdot \hat{n} \, ds = \int_0^1 \int_0^1 \int_0^1 1 \times dx dy dz$$

$$= \int_0^1 dx \int_0^1 dy \int_0^1 dz = 1$$

02. Ans: (c)

Sol: Given $\vec{A} = x y \vec{a}_x + x^2 \vec{a}_y$

Let $I = \oint \vec{A} \cdot d\vec{\ell}$, I is evaluated over the path shown in the Fig., as follows

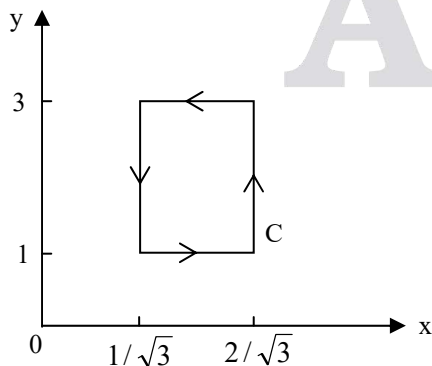


Fig.

$$I = \oint \vec{A} \cdot d\vec{\ell} = \int_{x=1/\sqrt{3}}^{x=2/\sqrt{3}} \vec{A} \cdot \vec{a}_x \, dx, y=1, x = \text{from } \frac{1}{\sqrt{3}} \text{ to } \frac{2}{\sqrt{3}}$$

$$+ \int \vec{A} \cdot d\vec{\ell} = \int_{y=1}^{y=3} \vec{A} \cdot \vec{a}_y \, dy, x = \frac{2}{\sqrt{3}}, y = \text{from } 1 \text{ to } 3$$

$$- \int \vec{A} \cdot d\vec{\ell} = \int_{x=1/\sqrt{3}}^{x=2/\sqrt{3}} \vec{A} \cdot \vec{a}_x \, dx, y=3, x = \text{from } \frac{1}{\sqrt{3}} \text{ to } \frac{2}{\sqrt{3}}$$

$$- \int \vec{A} \cdot d\vec{\ell} = \int_{y=1}^{y=3} \vec{A} \cdot \vec{a}_y \, dy, x=1/\sqrt{3}, y = \text{from } 1 \text{ to } 3$$

$$= \int x y \, dx + \int x^2 \, dy - \int x y \, dx - \int x^2 \, dy$$

$$= y \left. \frac{x^2}{2} \right|_{1/\sqrt{3}}^{2/\sqrt{3}} + x^2 y \Big|_1^3 - y \left. \frac{x^2}{2} \right|_{1/\sqrt{3}}^{2/\sqrt{3}} - x^2 y \Big|_1^3$$

$$\text{at } y=1 \quad x=2/\sqrt{3} \quad y=3 \quad x=1/\sqrt{3}$$

$$= \frac{1}{2} \left(\frac{4}{3} - \frac{1}{3} \right) + \frac{4}{3} (3-1) - \frac{3}{2} \left(\frac{4}{3} - \frac{1}{3} \right) - \frac{1}{3} (3-1)$$

$$= \frac{1}{2} + \frac{8}{3} - \frac{3}{2} - \frac{2}{3} = -1 + 2 = 1$$

03. Ans: (d)

Sol: $\vec{F} = \rho a_\rho + \rho \sin^2 \phi a_\phi - z a_z$

$$= F_\rho a_\rho + F_\phi a_\phi + F_z a_z$$

$$\nabla \cdot \vec{F} = \frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho F_\rho) + \frac{1}{\rho} \frac{\partial}{\partial \phi} (F_\phi) + \frac{\partial}{\partial z} (F_z)$$

$$= \frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho^2) + \frac{1}{\rho} \frac{\partial}{\partial \phi} (\rho \sin^2 \phi) + \frac{\partial}{\partial z} (-z)$$

$$= 2 + 2 \sin \phi \cos \phi - 1$$

$$= 1 + 2 \sin \phi \cos \phi$$

$$\nabla \cdot \vec{F} \Big|_{\phi=\pi/4} = 2, \quad \nabla \cdot \vec{F} \Big|_{\phi=0} = 1$$

$$\nabla \cdot \vec{F} \Big|_{\phi=\pi/4} = 2 \nabla \cdot \vec{F} \Big|_{\phi=0}$$

04. Ans: (c)

Sol: $\vec{D} = 2\hat{a}_x - 2\sqrt{3}\hat{a}_z \quad \vec{D} = |\vec{D}| \hat{a}_n$

$$|\vec{D}| = \sqrt{16} = 4$$

$$= \rho_s \hat{a}_n$$

$$\therefore \vec{D} = 4 \left\{ \frac{2\hat{a}_x - 2\sqrt{3}\hat{a}_z}{4} \right\}$$

$$= \rho_s \hat{a}_n \quad \therefore \rho_s = 4 \text{ C/m}^2$$

05. Ans: (d)

Sol: $V = 10y^4 + 20x^3$

$$E = -\nabla V = -60x^2\hat{a}_x - 40y^3\hat{a}_y$$

$$D = \epsilon_0 E = -60x^2\epsilon_0\hat{a}_x - 40y^3\epsilon_0\hat{a}_y$$

$$\nabla \cdot D = \rho_v$$

$$\rho_v = \frac{\partial}{\partial x}(-60x^2\epsilon_0) + \frac{\partial}{\partial y}(-40y^3\epsilon_0)$$

$$= -120x\epsilon_0 - 120y^2\epsilon_0$$

$$\rho_v(\text{at } 2, 0) = -120 \times 2\epsilon_0 - 120 \times 0^2\epsilon_0$$

$$= -240\epsilon_0$$

06. Ans: (d)

Sol: Given

$$V(x, y, z) = 50x^2 + 50y^2 + 50z^2$$

$$\vec{E}(x, y, z) \text{ in free space} = -\text{grad}(V)$$

$$= -\nabla V$$

$$= - \left[\frac{\partial}{\partial x} V \vec{a}_x + \frac{\partial}{\partial y} V \vec{a}_y + \frac{\partial}{\partial z} V \vec{a}_z \right]$$

$$= - \left[100x \vec{a}_x + 100y \vec{a}_y + 100z \vec{a}_z \right] \text{ V/m}$$

$$\vec{E}(1, -1, 1) =$$

$$- \left[100 \vec{a}_x - 100 \vec{a}_y + 100 \vec{a}_z \right] \text{ V/m}$$

$$E(1, -1, 1) = 100 \sqrt{(-1)^2 + (1)^2 + (-1)^2}$$

$$= 100\sqrt{3}$$

Direction of the electric field is given by the unit vector in the direction of \vec{E} .

$$\vec{a}_E = \frac{\vec{E}(1, -1, 1)}{|\vec{E}(1, -1, 1)|} = \frac{1}{\sqrt{3}} \left[-\vec{a}_x + \vec{a}_y - \vec{a}_z \right]$$

or in i, j, k notation, $\vec{a}_E = \frac{1}{\sqrt{3}} [-i + j - k]$

07. Ans: (b)

Sol: For valid B, $\nabla \cdot B = 0$

$$\left(\frac{\partial}{\partial x} a_x + \frac{\partial}{\partial y} a_y + \frac{\partial}{\partial z} a_z \right) (x^2 a_x - xy a_y - Kxz a_z) = 0$$

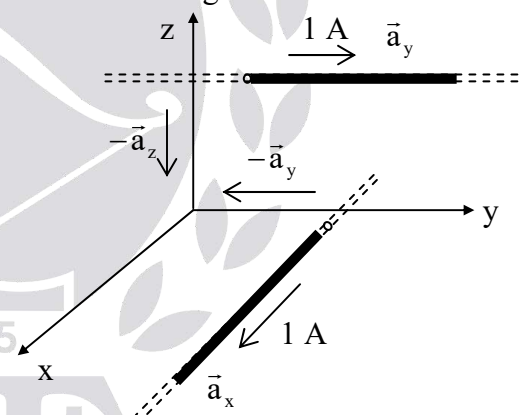
$$2x - x - Kx = 0$$

$$\Rightarrow 2 - 1 - K = 0$$

$$\therefore K = 1$$

08. Ans: (d)

Sol: The two infinitely long wires are oriented as shown in the Fig.



The infinitely long wire in the y-z plane carrying current along the \vec{a}_y direction produces the magnetic field at the origin in the direction of $\vec{a}_y \times -\vec{a}_z = -\vec{a}_x$.

The infinitely long wire in the x-y plane carrying current along the \vec{a}_x direction produces the magnetic field at the origin in the direction of $\vec{a}_x \times -\vec{a}_y = -\vec{a}_z$.

where \vec{a}_x , \vec{a}_y and \vec{a}_z are unit vectors along the 'x', 'y' and 'z' axes respectively.

\therefore x and z components of magnetic field are non-zero at the origin.

09. Ans: (a)

Sol: $\nabla \cdot \vec{B} = 0$

A divergence less vector may be a curl of some other vector

$$\vec{B} = \nabla \times \vec{A}$$

$$\nabla \times \vec{A} = \vec{B}$$

$$\oint_l \vec{A} \cdot d\vec{l} = \int_s \vec{B} \cdot d\vec{s}$$

$\int_s \vec{B} \cdot d\vec{s}$ is equal to magnetic flux ψ through a surface.

10. Ans: (c)

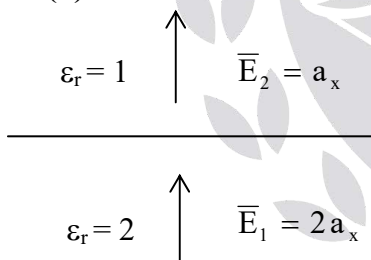
Sol: In general, for an infinite sheet of current density K A/m

$$H = \frac{1}{2} K \times \vec{a}_n$$

$$H = \frac{1}{2} (8\vec{a}_x \times \vec{a}_z) \\ = -4 \vec{a}_y \quad (\because \vec{a}_x \times \vec{a}_z = -\vec{a}_y)$$

11. Ans: (b)

Sol:



$$D_{n2} - D_{n1} = \rho_s \rightarrow (a)$$

$$D_{n2} = \epsilon E_{n2} = \epsilon_0 a_x$$

$$D_{n1} = \epsilon_0 2 \times 2 a_x = 4\epsilon_0 a_x$$

From (a)

$$(\epsilon_0 - 4\epsilon_0) a_x = \rho_s \Rightarrow \rho_s = -3\epsilon_0$$

12. Ans: (a)

Sol:

$$\mu_{r1} = 2 \quad \mu_{r2} = 1$$

$$z = 0$$

$$B_1 = 1.2\vec{a}_x + 0.8\vec{a}_y + 0.4\vec{a}_z$$

$$B_{n1} = 0.4\vec{a}_z$$

(Since $z = 0$ has normal component a_x)

$$B_{t1} = 1.2\vec{a}_x + 0.8\vec{a}_y$$

We know magnetic flux density is continuous

$$B_{n1} = B_{n2}$$

$$B_{n2} = 0.4\vec{a}_z$$

Surface charge, $\bar{k} = 0$

$$H_{t2} - H_{t1} = 0$$

$$H_{t2} = H_{t1}$$

$$\mu_1 B_{t2} = \mu_2 B_{t1}$$

$$B_{t2} = \frac{1}{2} (1.2\vec{a}_x + 0.8\vec{a}_y)$$

$$B_2 = B_{t2} + B_{n2} = 0.6\vec{a}_x + 0.4\vec{a}_y + 0.4\vec{a}_z$$

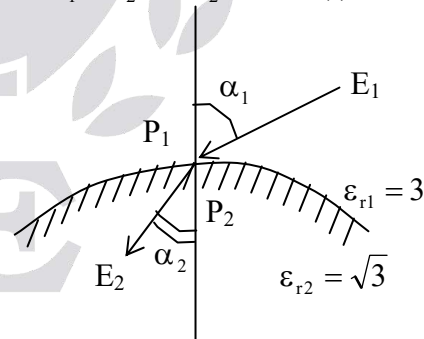
$$\mu_0 \mu_{r2} H_2 = 0.6\vec{a}_x + 0.4\vec{a}_y + 0.4\vec{a}_z$$

$$H_2 = \frac{1}{\mu_0} [0.6\vec{a}_x + 0.4\vec{a}_y + 0.4\vec{a}_z] \text{ A/m}$$

13. Ans: (b)

Sol: Tangential components of electric fields are continuous ($E_{t1} = E_{t2}$)

$$E_1 \sin \alpha_1 = E_2 \sin \alpha_2 \text{ --- (1)}$$



Normal component of electric flux densities are continuous across a charge free interface

$$D_{n1} = D_{n2}$$

$$3E_1 \cos \alpha_1 = \sqrt{3}E_2 \cos \alpha_2 \text{ --- (2)}$$

$$\alpha_1 = 60^\circ$$

$$\frac{(1)}{(2)} \Rightarrow \frac{\tan \alpha_1}{3} = \frac{\tan \alpha_2}{\sqrt{3}} \Rightarrow \tan \alpha_2 = 1$$

$$\alpha_2 = 45^\circ$$

14. Ans: (c)

Sol: Given flux $\phi = (t^3 - 2t) \text{ mWb}$

Magnitude of induced emf $|e'| = \left| \frac{d\phi}{dt} \right|_{t=4 \text{ sec}}$

$$|e'| = 3t^2 - 2 \Big|_{t=4 \text{ sec}}$$

$$= 3(4)^2 - 2$$

$$= 46 \text{ mWb}$$

This 'e' for one turn; but for 100 turns

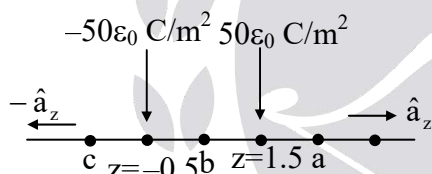
$$|e| = N|e'| = 100 \times 46 \text{ mWb}$$

$$|e| = 4.6 \text{ volts}$$

15. Ans: (a, b & d)

Sol:

(a)



Consider a point located at a for which $z > 1.5$ and $z > -0.5$ as shown in figure.

At this point $\hat{a}_n = \hat{a}_z$ for both the surface charge densities. Hence

$$\vec{E}(z) = \frac{50\epsilon_0}{2\epsilon_0} \hat{a}_z + \left(\frac{-50\epsilon_0}{2\epsilon_0} \right) \hat{a}_z = 0 \text{ V/m}$$

(b) Consider a point located at b for which $1.5 > z > -0.5$. For surface charge density of $50\epsilon_0 \text{ C/m}^2$, $\hat{a}_n = -\hat{a}_z$ where as for $-50\epsilon_0 \text{ C/m}^2$, $\hat{a}_n = \hat{a}_z$

$$\therefore \vec{E}(z) = \frac{50\epsilon_0}{2\epsilon_0} (-\hat{a}_z) + \left(\frac{-50\epsilon_0}{2\epsilon_0} \right) (\hat{a}_z) = -50\hat{a}_z \text{ V/m}$$

(c) Consider a point located at c for which $z < 1.5$ and $z < -0.5$. At this point $\hat{a}_n = -\hat{a}_z$.

$$\therefore \vec{E}(z) = \frac{50\epsilon_0}{2\epsilon_0} (-\hat{a}_z) + \left(\frac{-50\epsilon_0}{2\epsilon_0} \right) (\hat{a}_z) = 0 \text{ V/m}$$

$$\text{Hence we have } \vec{E} = \begin{cases} 0 & z > 1.5 \\ -50\hat{a}_z & 1.5 > z > -0.5 \\ 0 & z < -0.5 \end{cases}$$

(d) In the region $-0.5 < z < 1.5$ ($1.5 > z > -0.5$)

$\vec{E} = -50\hat{a}_z$ and $A = (x, y, z)$ and

$B = (x, y, -0.5)$.

$$\begin{aligned} V_{AB} &= -\int_B^A \vec{E} \cdot d\vec{L} \\ &= -\int_B^A (-50\hat{a}_z) (dx \hat{a}_x + dy \hat{a}_y + dz \hat{a}_z) \\ &= 50 \int_{-0.5}^z dz = 50[z]_{-0.5}^z = 50(z + 0.5) \\ &= 50z + 25 \end{aligned}$$