



**GATE | PSUs**

# **ELECTRICAL ENGINEERING**

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## **Electromagnetic Fields**

**Text Book:** Theory with worked out Examples  
and Practice Questions



# Chapter 1 Static Fields & Maxwell's Equations

(Solutions for Text Book Practice Questions)

01. Ans: 1

Sol:  $\vec{V} = x \cos^2 y \hat{i} + x^2 e^z \hat{j} + z \sin^2 y \hat{k}$   
 $= x \cos^2 y \hat{a}_x + x^2 e^z \hat{a}_y + z \sin^2 y \hat{a}_z$

From divergence theorem

$$\iiint_V \nabla \cdot \hat{n} \, ds = \int_V (\nabla \cdot \vec{D}) \, dv \dots\dots\dots 1$$

$$\nabla \cdot \vec{D} = \frac{\partial}{\partial x}(x \cos^2 y) + \frac{\partial}{\partial y}(x^2 e^z) + \frac{\partial}{\partial z}(z \sin^2 y)$$

$$= \cos^2 y + \sin^2 y = 1$$

$$dv = dx dy dz$$

Putting these value in equation 1 we have

$$\iiint_V \nabla \cdot \hat{n} \, ds = \int_0^1 \int_0^1 \int_0^1 1 \times dx dy dz$$

$$= \int_0^1 dx \int_0^1 dy \int_0^1 dz = 1$$

02. Ans: (c)

Sol: Given  $\vec{A} = x y \vec{a}_x + x^2 \vec{a}_y$

Let  $I = \oint_C \vec{A} \cdot d\vec{\ell}$ , I is evaluated over the path shown in the Fig., as follows

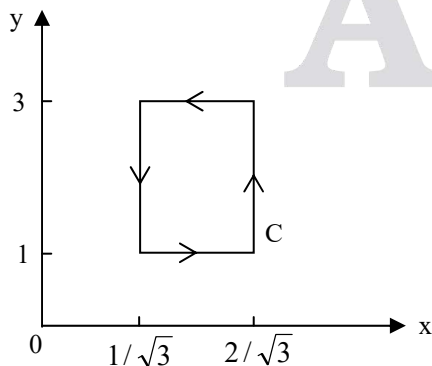


Fig.

$$I = \oint_C \vec{A} \cdot dx \vec{a}_x, y = 1, x = \text{from } \frac{1}{\sqrt{3}} \text{ to } \frac{2}{\sqrt{3}}$$

$$+ \int \vec{A} \cdot dy \vec{a}_y, x = \frac{2}{\sqrt{3}}, y = \text{from } 1 \text{ to } 3$$

$$- \int \vec{A} \cdot dx \vec{a}_x, y = 3, x = \text{from } \frac{1}{\sqrt{3}} \text{ to } \frac{2}{\sqrt{3}}$$

$$- \int \vec{A} \cdot dy \vec{a}_y, x = 1/\sqrt{3}, y = \text{from } 1 \text{ to } 3$$

$$= \int x y \, dx + \int x^2 \, dy - \int x y \, dx - \int x^2 \, dy$$

$$= y \frac{x^2}{2} \Big|_{1/\sqrt{3}}^{2/\sqrt{3}} + x^2 y \Big|_1^3 - y \frac{x^2}{2} \Big|_{1/\sqrt{3}}^{2/\sqrt{3}} - x^2 y \Big|_1^3$$

at  $y = 1 \quad x = 2/\sqrt{3} \quad y = 3 \quad x = 1/\sqrt{3}$

$$= \frac{1}{2} \left( \frac{4}{3} - \frac{1}{3} \right) + \frac{4}{3} (3-1) - \frac{3}{2} \left( \frac{4}{3} - \frac{1}{3} \right) - \frac{1}{3} (3-1)$$

$$= \frac{1}{2} + \frac{8}{3} - \frac{3}{2} - \frac{2}{3} = -1 + 2 = 1$$

03. Ans: (d)

Sol:  $\vec{F} = \rho a_\rho + \rho \sin^2 \phi a_\phi - z a_z$   
 $= F_\rho a_\rho + F_\phi a_\phi + F_z a_z$

$$\nabla \cdot \vec{F} = \frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho F_\rho) + \frac{1}{\rho} \frac{\partial}{\partial \phi} (F_\phi) + \frac{\partial}{\partial z} (F_z)$$

$$= \frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho^2) + \frac{1}{\rho} \frac{\partial}{\partial \phi} (\rho \sin^2 \phi) + \frac{\partial}{\partial z} (-z)$$

$$= 2 + 2 \sin \phi \cos \phi - 1$$

$$= 1 + 2 \sin \phi \cos \phi$$

$$\nabla \cdot \vec{F} \Big|_{\phi=\pi/4} = 2, \quad \nabla \cdot \vec{F} \Big|_{\phi=0} = 1$$

$$\nabla \cdot \vec{F} \Big|_{\phi=\pi/4} = 2 \nabla \cdot \vec{F} \Big|_{\phi=0}$$

04. Ans: (c)

Sol:  $\vec{D} = 2 \hat{a}_x - 2\sqrt{3} \hat{a}_z \quad \vec{D} = |\vec{D}| \hat{a}_n$

$$|\vec{D}| = \sqrt{16} = 4$$

$$= \rho_s \hat{a}_n$$

$$\therefore \vec{D} = 4 \left\{ \frac{2\hat{a}_x - 2\sqrt{3}\hat{a}_z}{4} \right\}$$

$$= \rho_s \hat{a}_n \quad \therefore \rho_s = 4 \text{ C/m}^2$$

**05. Ans: (d)**

**Sol:**  $V = 10y^4 + 20x^3$

$$E = -\nabla V = -60x^2\hat{a}_x - 40y^3\hat{a}_y$$

$$D = \epsilon_0 E = -60x^2\epsilon_0\hat{a}_x - 40y^3\epsilon_0\hat{a}_y$$

$$\nabla \cdot D = \rho_v$$

$$\rho_v = \frac{\partial}{\partial x}(-60x^2\epsilon_0) + \frac{\partial}{\partial y}(-40y^3\epsilon_0)$$

$$= -120x\epsilon_0 - 120y^2\epsilon_0$$

$$\rho_v(\text{at } 2, 0) = -120 \times 2\epsilon_0 - 120 \times 0^2\epsilon_0$$

$$= -240\epsilon_0$$

**06. Ans: (d)**

**Sol:** Given

$$V(x, y, z) = 50x^2 + 50y^2 + 50z^2$$

$$\vec{E}(x, y, z) \text{ in free space} = -\text{grad}(V)$$

$$= -\nabla V$$

$$= - \left[ \frac{\partial}{\partial x} V \vec{a}_x + \frac{\partial}{\partial y} V \vec{a}_y + \frac{\partial}{\partial z} V \vec{a}_z \right]$$

$$= - \left[ 100x \vec{a}_x + 100y \vec{a}_y + 100z \vec{a}_z \right] \text{ V/m}$$

$$\vec{E}(1, -1, 1) =$$

$$- \left[ 100 \vec{a}_x - 100 \vec{a}_y + 100 \vec{a}_z \right] \text{ V/m}$$

$$E(1, -1, 1) = 100 \sqrt{(-1)^2 + (1)^2 + (-1)^2}$$

$$= 100\sqrt{3}$$

Direction of the electric field is given by the unit vector in the direction of  $\vec{E}$ .

$$\vec{a}_E = \frac{\vec{E}(1, -1, 1)}{|E(1, -1, 1)|} = \frac{1}{\sqrt{3}} \left[ -\vec{a}_x + \vec{a}_y - \vec{a}_z \right]$$

or in i, j, k notation,  $\vec{a}_E = \frac{1}{\sqrt{3}} [-i + j - k]$

**07. Ans: (b)**

**Sol:** For valid B,  $\nabla \cdot B = 0$

$$\left( \frac{\partial}{\partial x} a_x + \frac{\partial}{\partial y} a_y + \frac{\partial}{\partial z} a_z \right) (x^2 a_x - xya_y - Kxz a_z) = 0$$

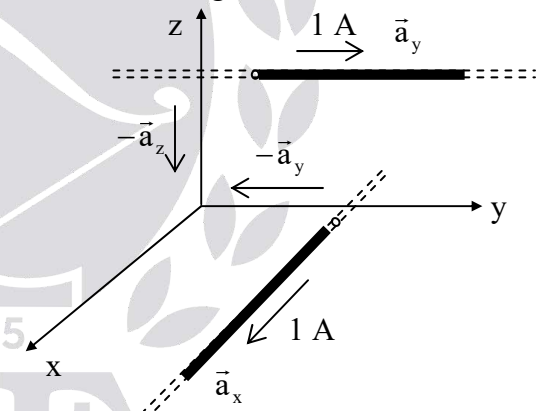
$$2x - x - Kx = 0$$

$$\Rightarrow 2 - 1 - K = 0$$

$$\therefore K = 1$$

**08. Ans: (d)**

**Sol:** The two infinitely long wires are oriented as shown in the Fig.



The infinitely long wire in the y-z plane carrying current along the  $\vec{a}_y$  direction produces the magnetic field at the origin in the direction of  $\vec{a}_y \times -\vec{a}_z = -\vec{a}_x$ .

The infinitely long wire in the x-y plane carrying current along the  $\vec{a}_x$  direction produces the magnetic field at the origin in the direction of  $\vec{a}_x \times -\vec{a}_y = -\vec{a}_z$ .

where  $\vec{a}_x$ ,  $\vec{a}_y$  and  $\vec{a}_z$  are unit vectors along the 'x', 'y' and 'z' axes respectively.

$\therefore$  x and z components of magnetic field are non-zero at the origin.

**09. Ans: (a)**

**Sol:**  $\nabla \cdot \bar{B} = 0$

A divergence less vector may be a curl of some other vector

$$\bar{B} = \nabla \times \bar{A}$$

$$\nabla \times \bar{A} = \bar{B}$$

$$\oint_l \bar{A} \cdot d\bar{l} = \int_s \bar{B} \cdot d\bar{s}$$

$\int_s \bar{B} \cdot d\bar{s}$  is equal to magnetic flux  $\psi$  through a surface.

**10. Ans: (c)**

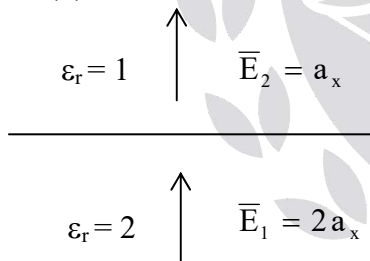
**Sol:** In general, for an infinite sheet of current density  $K$  A/m

$$H = \frac{1}{2} K \times a_n$$

$$H = \frac{1}{2} (8\bar{a}_x \times \bar{a}_z) = -4\bar{a}_y \quad (\because \bar{a}_x \times \bar{a}_z = -\bar{a}_y)$$

**11. Ans: (b)**

**Sol:**



$$D_{n_2} - D_{n_1} = \rho_s \rightarrow (a)$$

$$D_{n_2} = \epsilon E_{n_2} = \epsilon_0 a_x$$

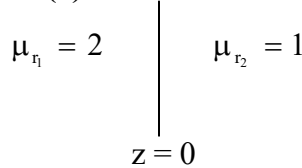
$$D_{n_1} = \epsilon_0 2 \times 2 a_x = 4\epsilon_0 a_x$$

From (a)

$$(\epsilon_0 - 4\epsilon_0) a_x = \rho_s \Rightarrow \rho_s = -3\epsilon_0$$

**12. Ans: (a)**

**Sol:**



$$B_1 = 1.2\bar{a}_x + 0.8\bar{a}_y + 0.4\bar{a}_z$$

$$B_{n_1} = 0.4\bar{a}_z$$

(Since  $z = 0$  has normal component  $a_x$ )

$$B_{t_1} = 1.2\bar{a}_x + 0.8\bar{a}_y$$

We know magnetic flux density is continuous

$$B_{n_1} = B_{n_2}$$

$$B_{n_2} = 0.4\bar{a}_z$$

Surface charge,  $\bar{k} = 0$

$$H_{t_2} - H_{t_1} = 0$$

$$H_{t_2} = H_{t_1}$$

$$\mu_1 B_{t_2} = \mu_2 B_{t_1}$$

$$B_{t_2} = \frac{1}{2} (1.2\bar{a}_x + 0.8\bar{a}_y)$$

$$B_2 = B_{t_2} + B_{n_2} = 0.6\bar{a}_x + 0.4\bar{a}_y + 0.4\bar{a}_z$$

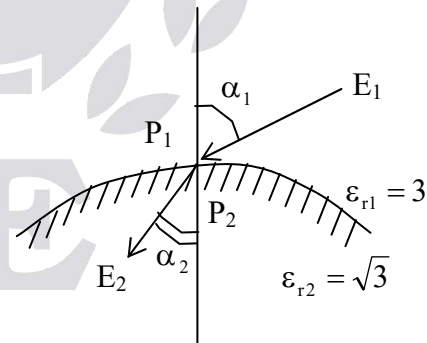
$$\mu_0 \mu_{r_2} H_2 = 0.6\bar{a}_x + 0.4\bar{a}_y + 0.4\bar{a}_z$$

$$H_2 = \frac{1}{\mu_0} [0.6\bar{a}_x + 0.4\bar{a}_y + 0.4\bar{a}_z] \text{ A/m}$$

**13. Ans: (b)**

**Sol:** Tangential components of electric fields are continuous ( $E_{t_1} = E_{t_2}$ )

$$E_1 \sin \alpha_1 = E_2 \sin \alpha_2 \text{ -----(1)}$$



Normal component of electric flux densities are continuous across a charge free interface

$$D_{n_1} = D_{n_2}$$

$$3E_1 \cos \alpha_1 = \sqrt{3}E_2 \cos \alpha_2 \text{ -----(2)}$$

$$\alpha_1 = 60^\circ$$

$$\frac{(1)}{(2)} \Rightarrow \frac{\tan \alpha_1}{3} = \frac{\tan \alpha_2}{\sqrt{3}} \Rightarrow \tan \alpha_2 = 1$$

$$\alpha_2 = 45^\circ$$

14. Ans: (c)

Sol:  $N = 100$

$$\phi = t^3 - 2t \text{ mWb}$$

According to Faraday's law

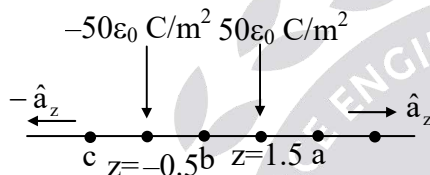
$$E = N \frac{d\phi}{dt} \Big|_{t=4\text{sec}}$$

$$= 100 \times (3t^2 - 2) \text{ mV} = 4.6 \text{ V}$$

15. Ans: (a, b & d)

Sol:

(a)



Consider a point located at a for which  $z > 1.5$  and  $z > -0.5$  as shown in figure. At this point  $\hat{a}_n = \hat{a}_z$  for both the surface charge densities. Hence

$$\bar{E}(z) = \frac{50\epsilon_0}{2\epsilon_0} \hat{a}_z + \left( \frac{-50\epsilon_0}{2\epsilon_0} \right) \hat{a}_z = 0 \text{ V/m}$$

(b) Consider a point located at b for which  $1.5 > z > -0.5$ . For surface charge density of  $50\epsilon_0 \text{ C/m}^2$ ,  $\hat{a}_N = -\hat{a}_z$  where as for  $-50\epsilon_0 \text{ C/m}^2$ ,  $\hat{a}_n = \hat{a}_z$

$$\therefore \bar{E}(z) = \frac{50\epsilon_0}{2\epsilon_0} (-\hat{a}_z) + \left( \frac{-50\epsilon_0}{2\epsilon_0} \right) (\hat{a}_z) = -50\hat{a}_z \text{ V/m}$$

(c) Consider a point located at c for which  $z < 1.5$  and  $z < -0.5$ . At this point  $\hat{a}_n = -\hat{a}_z$ .

$$\therefore \bar{E}(z) = \frac{50\epsilon_0}{2\epsilon_0} (-\hat{a}_z) + \left( \frac{-50\epsilon_0}{2\epsilon_0} \right) (\hat{a}_z) = 0 \text{ V/m}$$

$$\text{Hence we have } \bar{E} = \begin{cases} 0 & z > 1.5 \\ -50\hat{a}_z & 1.5 > z > -0.5 \\ 0 & z < -0.5 \end{cases}$$

(d) In the region  $-0.5 < z < 1.5$  ( $1.5 > z > -0.5$ )

$\bar{E} = -50\hat{a}_z$  and  $A = (x, y, z)$  and

$B = (x, y, -0.5)$ .

$$V_{AB} = -\int_B^A \bar{E} \cdot d\bar{L}$$

$$= -\int_B^A (-50\hat{a}_z) (dx \hat{a}_x + dy \hat{a}_y + dz \hat{a}_z)$$

$$= 50 \int_{-0.5}^z dz = 50[z]_{-0.5}^z = 50(z + 0.5)$$

$$= 50z + 25$$

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