

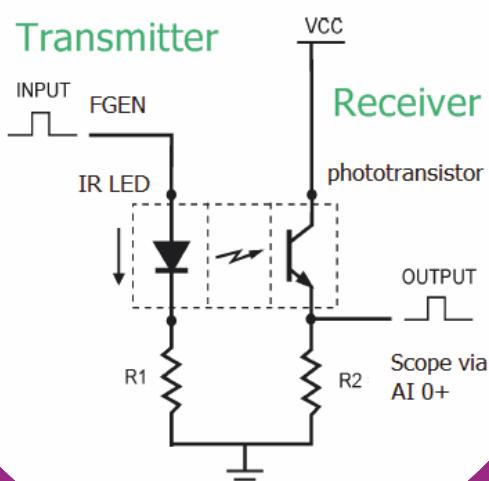


**GATE | PSUs**

# INSTRUMENTATION ENGINEERING

## Communication & Optical Instrumentation

(Text Book: Theory with worked out Examples and  
Practice Questions)



# Chapter

# 1

# Introduction

(Solutions for Text Book Practice Questions)

**01. Ans: (b)**

**Sol:** We know that

$$e^{-at}u(t) \xleftrightarrow{\text{F.T.}} \frac{1}{a + j\omega}$$

$$e^{at}u(-t) \xleftrightarrow{\text{F.T.}} \frac{1}{a - j\omega}$$

$$e^{-at}u(t) - e^{at}u(-t) \xleftrightarrow{\text{F.T.}} \frac{1}{a + j\omega} - \frac{1}{a - j\omega}$$

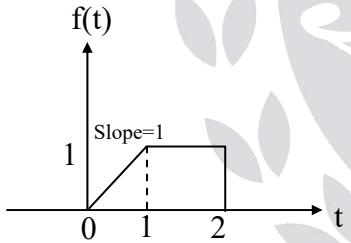
Put  $a = 0$

$$u(t) - u(-t) \xleftrightarrow{\text{F.T.}} \frac{1}{j\omega} - \frac{1}{-j\omega}$$

$$\text{sgn}(t) \xleftrightarrow{\text{F.T.}} \frac{2}{j\omega}$$

**02. Ans: (a)**

**Sol:**



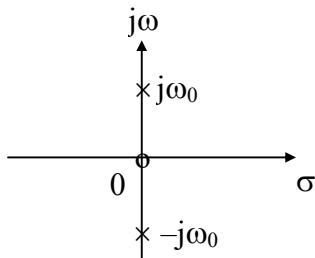
$$f(t) = r(t) - r(t-1) - u(t-2)$$

**03. Ans: (a)**

**Sol:** The convergence of Fourier transform is along the  $j\omega$ -axis in s-plane.

**04. Ans: (a)**

**Sol:**

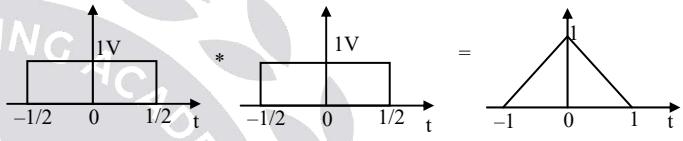


$$F(s) = \frac{s}{s^2 + \omega_0^2} \xrightarrow{\text{I.L.T.}} f(t) = \cos \omega_0 t$$

$$f(t) = \cos \omega_0 t \xrightarrow{\text{I.L.T.}} F(\omega) = \pi[\delta(\omega - \omega_0) + \delta(\omega + \omega_0)]$$

**05. Ans: (d)**

**Sol:**



**06. Ans: (c)**

**Sol:** Given  $x(t) = e^{-at^2}$

Fourier transform of  $x(t)$  is

$$\begin{aligned} X(\omega) &= \int_{-\infty}^{\infty} x(t)e^{-j\omega t} dt \\ &= \int_{-\infty}^{\infty} e^{-at^2} e^{-j\omega t} dt \\ &= \int_{-\infty}^{\infty} e^{-\left(at^2 + j\omega t\right)} dt \\ &= e^{-\frac{\omega^2}{4a}} \int_{-\infty}^{\infty} e^{-\left[\sqrt{at} + \frac{j\omega}{2\sqrt{a}}\right]^2} dt \end{aligned}$$

$$\text{Let } p = \sqrt{at} + \frac{j\omega}{2\sqrt{a}}$$

$$dp = \sqrt{a}dt$$

$$\begin{aligned} X(\omega) &= \frac{e^{-\frac{\omega^2}{4a}}}{\sqrt{a}} \int_{-\infty}^{\infty} e^{-p^2} dp \\ &\quad \int_{-\infty}^{\infty} e^{-p^2} dp = \sqrt{\pi} \end{aligned}$$

$$X(\omega) = \frac{e^{-\frac{\omega^2}{4a}}}{\sqrt{a}} \sqrt{\pi}$$

$$X(\omega) = \sqrt{\frac{\pi}{a}} e^{-\frac{\omega^2}{4a}}$$

**07. Ans: (d)**

**Sol:** The EFS expression of a periodic signal  $x(t)$

$$\text{is } x(t) = \sum_{n=-\infty}^{\infty} c_n e^{jn\omega_0 t}$$

where, ' $c_n$ ' is EFS coefficient.

Apply F.T on both sides

$$X(\omega) = \sum_{n=-\infty}^{\infty} c_n \text{FT}[e^{jn\omega_0 t}]$$

$$e^{jn\omega_0 t} \leftrightarrow 2\pi\delta(\omega - n\omega_0)$$

$$X(\omega) = 2\pi \sum_{n=-\infty}^{\infty} c_n \delta(\omega - n\omega_0)$$

So, it is a train of impulse.

**08. Ans: (a)**

**Sol:**  $V(j\omega) = e^{-j2\omega}; |\omega| \leq 1$

$$\begin{aligned} \text{Energy} &= \frac{1}{2\pi} \int_{-\infty}^{\infty} |V(j\omega)|^2 d\omega \\ &= \frac{1}{2\pi} \int_{-1}^1 |e^{-j2\omega}|^2 d\omega \\ &= \frac{1}{2\pi} \int_{-1}^1 1 d\omega \\ &= \frac{2}{2\pi} \\ &= \frac{1}{\pi} \end{aligned}$$

**09. Ans: (b)**

**Sol:** Parseval's theorem is used to find the energy of the signal in frequency domain.

$$\therefore \int_{-\infty}^{\infty} |f(t)|^2 dt = \frac{1}{2\pi} \int_{-\infty}^{\infty} |F(j\omega)|^2 d\omega$$

**10. Ans: (a)**

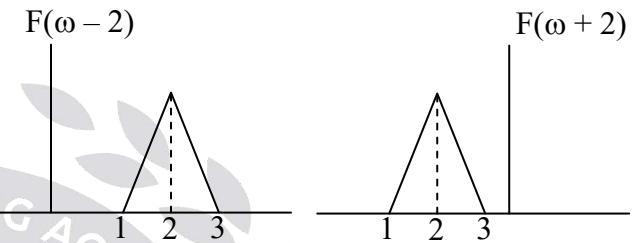
**Sol:**  $f(t) = A e^{-a|t|} \xrightarrow{\text{F.T}} F(j\omega) = \frac{2Aa}{a^2 + \omega^2}$

**11. Ans: (d)**

**Sol:**  $m(t) = f(t) \cos 2t$

Apply Fourier transform

$$M(f) = \frac{1}{2} [F(\omega - 2) + F(\omega + 2)]$$



**12. Ans: (b)**

**Sol:** For band limited signals,

$$S(f) \neq 0; |f| < W$$

$$S(f) = 0; |f| > W$$

**13. Ans: (a)**

**Sol:** In a communication system, antenna is used to convert voltage variations to field variation and vice-versa.

**14. Ans: (d)**

**Sol:** Hilbert transform of  $f(t)$  is

$$H.T\{f(t)\} = f(t) * \frac{1}{\pi t}$$

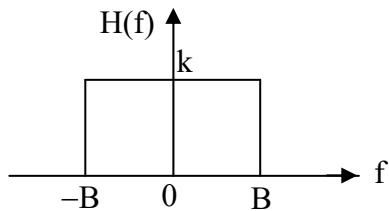
It is in the terms of 't'.

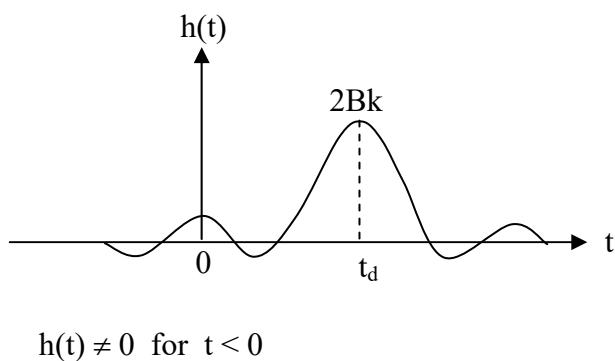
**15. Ans: (a)**

**Sol:** For an ideal LPF

$$H(f) = k e^{-j\omega t_0} \quad \text{for } -B < f < B$$

$$h(t) = F^{-1}[H(f)] = 2Bk \operatorname{sinc} 2B(t - t_d)$$





Output exists before input is applied i.e. non-causal, which is physically impossible.

**16. Ans: (b)**

**Sol:**  $\delta(at) = \frac{1}{|a|} \delta(t)$   
 $\delta(2t) = \frac{1}{2} \delta(t)$

**17. Ans: (a)**

**Sol:** By modulation we are translating the low frequency spectrum into high frequency spectrum.

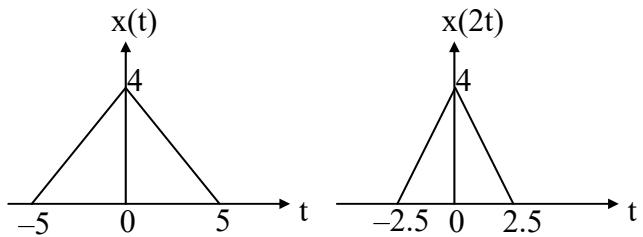
**18. Ans: (a)**

**Sol:** We know that

$$\begin{aligned} P(\text{dBm}) &= 10\log(P \times 10^3) \\ -10 &= 10\log(P \times 10^3) \\ P \times 10^3 &= 10^{-1} \\ P &= 10^{-4} = 100 \mu\text{W} \end{aligned}$$

**19. Ans: (a)**

**Sol:**  $x(2t)$  means signal time axis is compressed by 2



**20. Ans: (b)**

**Sol:** Audio frequency is between 20Hz to 20kHz

**21. Ans: (d)**

**Sol:** Telephone channel carries voice. Voice frequency is between 300 Hz to 3500 Hz. So bandwidth is 3200Hz. So we approximately consider 4kHz is the bandwidth requirement of a telephone channel.

**22. Ans: (c)**

**Sol:** From the signal spectrum  $f_H = 530$  kHz,  $f_L = 50$  kHz  
 $\text{Bandwidth} = f_H - f_L = 530$  kHz - 50 kHz  
 $= 480$  kHz

# Chapter 2 Amplitude Modulation

**01. Ans: (a)**

**Sol:**  $V(t) = A_c \cos \omega_c t + 2 \cos \omega_m t \cdot \cos \omega_c t$ .

Comparing this with the AM-DSB-SC signal

$A \cos \omega_c t + m(t) \cos \omega_c t$ , it implies that

$$m(t) = 2 \cos \omega_m t \Rightarrow E_m = 2$$

To implement Envelope detection,

$$A_c \geq E_m$$

$$\therefore (A_c)_{\min} = 2$$

**02. Ans: (d)**

**Sol:**  $m(t) = (A_c + A_m \cos \omega_m t) \cos \omega_c t$ .

$$= A_c \left( 1 + \frac{A_m}{A_c} \cos \omega_m t \right) \cos \omega_c t.$$

Given

$$A_c = 2A_m$$

$$= A_c \left( 1 + \frac{1}{2} \cos \omega_m t \right) \cos \omega_c t.$$

$$P_T = \frac{A_c^2}{2} \left[ 1 + \frac{\mu^2}{2} \right], P_s = \frac{A_c^2}{2} \left[ \frac{\mu^2}{4} \right]$$

$$\frac{P_T}{P_s} = \frac{1 + \frac{\mu^2}{2}}{\frac{\mu^2}{4}} = \frac{1 + \frac{1}{8}}{\frac{1}{16}} = \frac{9}{8} \times 16$$

$$P_T = 18 P_s$$

**03. Ans: (a)**

**Sol:**  $m(t) = 2 \cos 2\pi f_1 t + \cos 2\pi f_2 t$

$$C(t) = A_c \cos 2\pi f_c t$$

$$S(t) = [A_c + m(t)] \cos 2\pi f_c t$$

$$S(t) = A_c [1 + \frac{1}{A_c} m(t)] \cos 2\pi f_c t$$

$$K_a = \frac{1}{A_c}$$

$$A_{m1} = 2, A_{m2} = 1$$

$$\mu_1 = K_a A_{m1} = \frac{2}{A_c}, \mu_2 = K_a A_{m2} = \frac{1}{A_c}$$

$$\mu = \sqrt{\mu_1^2 + \mu_2^2}$$

$$\Rightarrow 0.5 = \sqrt{\frac{4}{A_c^2} + \frac{1}{A_c^2}}$$

$$\Rightarrow A_c = \sqrt{20}$$

**04. Ans: (c)**

**Sol:**  $m(t) = -0.2 + 0.6 \sin \omega_1 t, k_a = 1, A_c = 100$

$$S(t) = A_c [1 - 0.2 + 0.6 \sin \omega_1 t] \cos \omega_c t$$

$$= 100 [0.8 + 0.6 \sin \omega_1 t] \cos \omega_c t$$

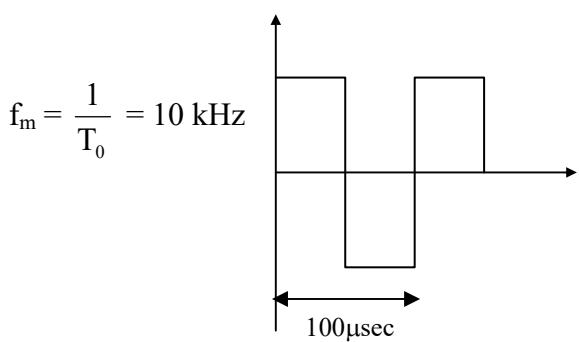
$$V_{\max} = A_c [1 + \mu] = 100 [0.8 + 0.6] = 140 \text{ V}$$

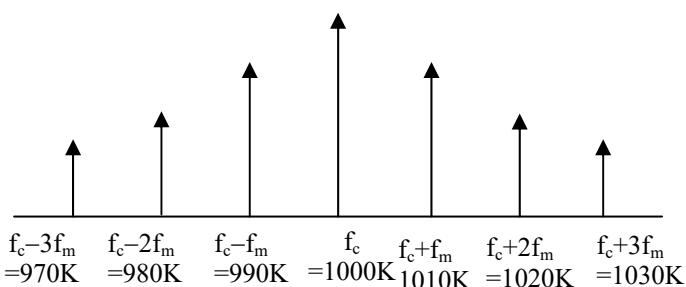
$$V_{\min} = A_c [1 - \mu] = 100 [0.8 - 0.6] = 20 \text{ V}$$

**05. Ans: (c)**

**Sol:**  $f_c = 1 \text{ MHz} = 1000 \text{ kHz}$

The given  $m(t)$  is symmetrical square wave of period  $T = 100 \mu\text{sec}$

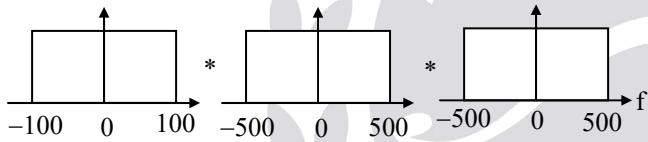




These frequencies 980k, 1020k are not present because the symmetrical square wave it consists of half wave symmetries only odd harmonics are present, even harmonics are dismissed.

**06. Ans: (d)**

$$\text{Sol: } m(t) = \text{sinc}(200t)\text{sinc}^2(1000t) \\ = \text{sinc}(200t)\text{sinc}(1000t)\text{sinc}(1000t)$$

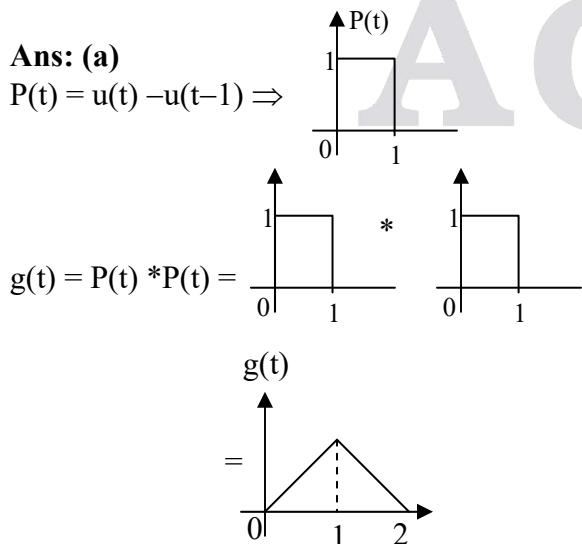


So, highest frequency component in the signal  $m(t)$  is  $100 + 500 + 500 = 1100$

$$\text{BW} = 2 \times 1100 \\ \text{BW} = 2200 \text{ Hz}$$

**07. Ans: (a)**

$$\text{Sol: } P(t) = u(t) - u(t-1) \Rightarrow$$



$$x(t) = 100(P(t) + 0.5g(t))\cos\omega_ct$$

$$= 100(1 + 0.5t)\cos\omega_ct$$

$$= A_c(1 + K_{am}(t))\cos\omega_ct$$

$$k_a = 0.5, m(t) = t$$

$$\mu = k_a[m(t)]_{\max}$$

$$\mu = 0.5 \times 1 = 0.5$$

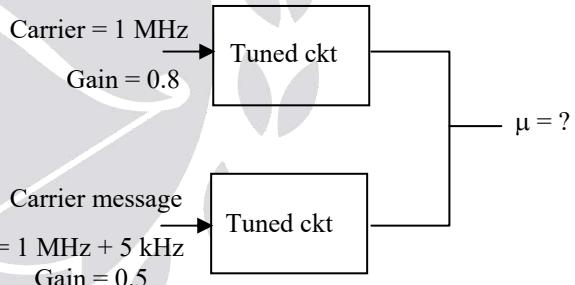
**08. Ans: (d)**

$$\text{Sol: } R_L C \leq \frac{\sqrt{1-\mu^2}}{2\pi f_m \mu}$$

So it depends on depth of modulation and the highest modulation frequency.

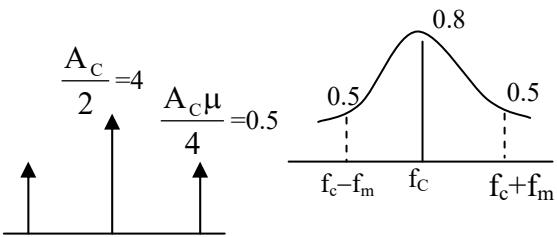
**09. Ans: (b)**

$$\text{Sol: } S(t) = 10\cos 2\pi 10^6 t + 8\cos 2\pi 5 \times 10^3 t \cos 2\pi 10^6 t$$



$$\begin{aligned} S(t) &= 0.8 \times 10 \cos 2\pi 10^6 t \\ &\quad + 0.5 \times 8 \cos 2\pi 5000 t \cos 2\pi 10^6 t \\ &= 8\left(1 + \frac{4}{8} \cos 2\pi 5000 t\right) \cos 2\pi 10^6 t \end{aligned}$$

$$\mu = \frac{4}{8} = \frac{1}{2} = 0.5$$



**10. Ans: (d)****Sol:**  $A_{\max} = 10V$ 

$$A_{\min} = 5V$$

$$\mu = 0.1$$

$$\mu = \frac{A_{\max} - A_{\min}}{A_{\max} + A_{\min}} = \frac{1}{3} = 0.33$$

$$A_C = \frac{A_{\max} + A_{\min}}{2} = \frac{10 + 5}{2} = 7.5 V$$

$$\begin{aligned} & A_C(1+\mu) = A_C + A_C\mu \\ & \Rightarrow 10V = 7.5 + 2.5 \end{aligned}$$

$$m(t) = 0$$

$$A$$

$$A_C(1-\mu) = A_C - A_C\mu$$

$$5V = 7.5 - 2.5$$

$$\text{Amplitude deviation } A_C\mu = 7.5 \times \frac{1}{3} = 2.5 V$$

$$\mu_2 = 0.1 \Rightarrow A_{c2}\mu_2 = 2.5$$

$$A_{c2} = 25 V$$

Which must be added to attain = 17.5

**11. Ans: (d)****Sol:** Modulation index

$$\mu = k_a |m(t)|_{\max}$$

$$k_a = \frac{2b}{a} = \frac{2(\text{square term coefficient})}{\text{linear term coefficient}}$$

$$|m(t)|_{\max} = 1$$

$$\mu = 2 \left( \frac{b}{a} \right)$$

$$P_{SB} = \frac{1}{2} P_c \Rightarrow P_c \frac{\mu^2}{2} = \frac{1}{2} P_c$$

$$\mu^2 = 1 \Rightarrow \left( 2 \frac{b}{a} \right)^2 = 1$$

$$\Rightarrow 2 \frac{b}{a} = 1 \Rightarrow \frac{a}{b} = 2$$

**12. Ans: 0.125****Sol:**  $s(t) = \cos(2000\pi t) + 4\cos(2400\pi t) + \cos(2000\pi t)$ 

Here  $4\cos(2400\pi t)$  is the carrier signal.

$\cos(2000\pi t)$  and  $\cos(2000\pi t)$  are the sideband message signals.

$$P_c = \frac{4^2}{2} = 8 W$$

$$P_m = \frac{1}{2} + \frac{1}{2} = 1 W$$

$$\frac{P_m}{P_c} = \frac{1}{8} = 0.125$$

**13. Ans: (a, c & d)****Sol:**  $S_{AM}(t) = 10\cos(2\pi \times 5000t) + 25\cos(2\pi \times 5200t) + 25\cos(2\pi \times 4800t)$ 

$$\therefore \text{USB Frequency} = 5200 \text{ Hz}$$
  
$$\text{LSB Frequency} = 4800 \text{ Hz}$$

$$\frac{A_c\mu}{2} = 25$$

$$\frac{10 \times \mu}{2} = 25$$

$$\therefore \mu = 5$$

a, c & d are correct.

**NOTE:** options are changed for

(a)  $\mu = 5$  (b)  $\mu = 2.5$

**14. Ans: (a & c)****Sol:**  $S_{AM}(t) = K_1\cos(2\pi \times 5000t) + K_2\cos(2\pi \times 5200t) + K_3\cos(2\pi \times 4800t)$ 

$$c(t) = 10 \cos(2\pi \times 5000t)$$

$$K_1 = 10 = A_C$$

$$\mu = 0.5$$

$$f_c + f_m = 5200 \text{ Hz}$$

$$f_c - f_m = 4800 \text{ Hz}$$

$$\therefore \frac{A_c\mu}{2} = K_2 = K_3$$

$$\therefore 2f_m = 400 \text{ Hz}$$

$$\frac{10 \times 0.5}{2} = K_2 = K_3$$

$$\therefore f_m = 200 \text{ Hz}$$

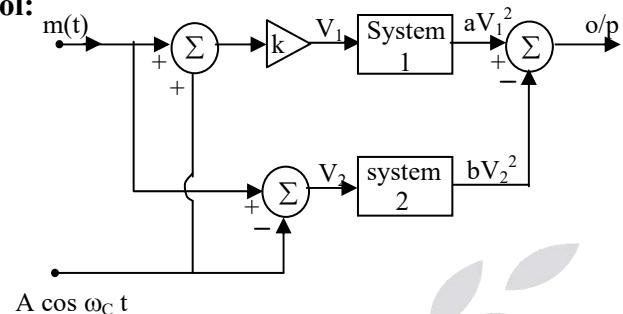
$$\therefore K_2 = K_3 = 2.5$$

a & c are correct.

# Chapter 3 Sideband Modulation Techniques

01. Ans: (c)

Sol:



$$A \cos \omega_C t$$

$$V_1 = k [m(t) + c(t)]$$

$$V_2 = [m(t) - c(t)]$$

$$V_0 = aV_1^2 - bV_2^2$$

$$= ak^2[m(t) + c(t)]^2 - b[m(t) - c(t)]^2$$

$$= ak^2 [m^2(t) + c^2(t) + 2m(t)c(t)]$$

$$- b[m^2(t) + c^2(t) - 2m(t)c(t)]$$

$$= [ak^2 - b]m^2(t) + [ak^2 - b]c^2(t)$$

$$+ 2[ak^2 + b][m(t)c(t)]$$

$$\text{on verification if } k = \sqrt{\frac{b}{a}}$$

$$S(t) = 4bm(t)c(t) \rightarrow \text{DSBSC Signal}$$

02. Ans: (d)

Sol: Given A = 10

$$m(t) = \cos 1000\pi t$$

$$b = 1$$

B.W = ? and power = ?

$$s(t) = 4b.A \cos 2\pi f_c t \cdot \cos 2\pi (500)t$$

$$= 40 \cdot \cos 2\pi f_c t \cdot \cos 2\pi (500)t$$

$$B.W = 2 f_m$$

$$= 2 (500)$$

$$= 1 \text{ kHz}$$

$$\text{Power} = \frac{A_c^2 A_m^2}{4}$$

$$= \frac{1600 \times 1}{4}$$

$$= 400 \text{ W}$$

03. Ans: (c)

Sol: Carrier =  $\cos 2\pi (100 \times 10^6)t$

Modulating signal =  $\cos(2\pi \times 10^6)t$

Output of Balanced modulator

$$= 0.5[\cos 2\pi (101 \times 10^6)t + \cos 2\pi (99 \times 10^6)t]$$

The Output of HPF is  $0.5 \cos 2\pi (101 \times 10^6)t$

Output of the adder is

$$= 0.5 \cos 2\pi (101 \times 10^6)t + \sin 2\pi (100 \times 10^6)t$$

$$= 0.5 \cos 2\pi [(100+1)10^6t] + \sin 2\pi (100 \times 10^6)t$$

$$= 0.5[\cos 2\pi (100 \times 10^6)t \cdot \cos 2\pi (10^6)t$$

$$- \sin 2\pi (100 \times 10^6)t \cdot \sin 2\pi (10^6)t]$$

$$+ \sin 2\pi (100 \times 10^6)t]$$

$$= 0.5 \cos 2\pi (100 \times 10^6)t \cdot \cos 2\pi (10^6)t$$

$$+ \sin 2\pi (100 \times 10^6)t [1 - 0.5 \sin 2\pi (10^6)t]$$

$$\text{Let } 0.5 \cos 2\pi (10^6)t = r(t) \cos \theta(t)$$

$$1 - 0.5 \sin 2\pi (10^6)t = r(t) \sin \theta(t)$$

The envelope is

$$r(t) = [0.25 \cos^2 2\pi (10^6)t$$

$$+ \{1 - 0.5 \sin 2\pi (10^6)t\}^2]^{1/2}$$

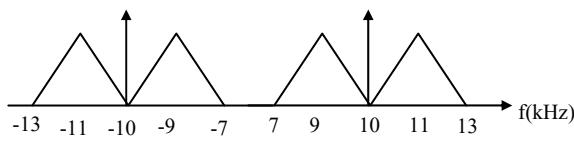
$$= [1.25 - \sin 2\pi (10^6)t]^{1/2}$$

$$= [\frac{5}{4} - \sin 2\pi (10^6)t]^{1/2}$$

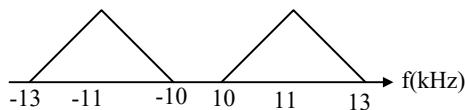


**04. Ans: (b)**

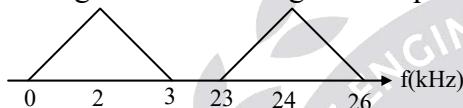
**Sol:** Output of 1<sup>st</sup> balanced modulator is



Output of HPF is



The Output of 2<sup>nd</sup> balanced modulator is consisting of the following +ve frequencies.



Thus, the spectral peaks occur at 2 kHz and 24 kHz.

**05. Ans: (c)**

**Sol:** Given

$$f_{m_1} = 100\text{Hz}, f_{m_2} = 200\text{Hz}, f_{m_3} = 400\text{Hz},$$

$$f_c = 100\text{KHz}, f_{c_{L0}} = 100.02\text{KHz}$$

$$S(t)/T_x = \frac{A_c A_m}{2} [\cos(f_c + f_{m_1})t + \cos(f_c + f_{m_2})t + \cos(f_c + f_{m_3})t]$$

$$S(t)/R_x = [S(t)/T_x] A_c \cos 2\pi f_{c_{L0}} t$$

$$\Rightarrow \frac{A_c^2 A_m}{4} [\cos(f_c + f_{c_{L0}} + f_{m_1}) + \cos(f_{m_1} - 20) + \cos(f_c + f_{c_{L0}} + f_{m_2}) + \cos(f_{m_2} - 20) + \cos(f_c + f_{c_{L0}} + f_{m_3}) + \cos(f_{m_3} - 20)]$$

Detector output frequencies:

$$80\text{Hz}, 180\text{Hz}, 380\text{Hz}$$

**06. Ans: (b)**

**Sol:** Given

SSB AM is used, LSB is transmitted

$$f_{LO} = (f_c + 10)$$

$$S(t)/T_x = \frac{A_c A_m}{2} \cos 2\pi[f_c - f_m]t$$

$$S(t)/R_x = \left[ \frac{A_c A_m}{2} \cos 2\pi(f_c - f_m)t \right] \cos 2\pi(f_c + 10)t \\ \Rightarrow \frac{A_c A_m}{4} [\cos 2\pi(2f_c + 10 - f_m)t + \cos 2\pi(10 + f_m)t]$$

i.e., from 310 Hz to 1010 Hz

**07. Ans: (b)**

**Sol:** BW of Basic group =  $12 \times 4 = 48\text{ kHz}$

BW of super group =  $5 \times 48 = 240\text{ kHz}$

**08. Ans: (d)**

**Sol:** Given 11 voice signals

B.W. of each signals = 3 kHz

Guard Band Width = 1 kHz

Lowest  $f_c = 300\text{ kHz}$

Highest  $f_c =$

$$\Rightarrow f_{c_H} + f_{m_{lost}} = 300\text{kHz} + 11(3\text{kHz}) + 10(1\text{kHz}) \\ = 343\text{ kHz}$$

$$f_{c_H} = 343\text{ kHz} - 3\text{ kHz}$$

$$= 340\text{ kHz}$$

**09. Ans: (b)**

**Sol:**  $f_{m1} = 5\text{ kHz} \rightarrow \text{AM}$

$f_{m2} = 10\text{ kHz} \rightarrow \text{DSB}$

$f_{m3} = 10\text{kHz} \rightarrow \text{SSB}$

$f_{m4} = 2\text{kHz} \rightarrow \text{SSB}$

$f_{m5} = 5\text{kHz} \rightarrow \text{AM}$

$f_g = 1\text{kHz}$

$$\text{BW} = (2f_{m1} + 2f_{m2} + f_{m3} + f_{m4} + 2f_{m5} + 4f_g) \\ = 2 \times 5 + 2 \times 10 + 10 + 2 + 2 \times 5 + 4 \times 1 \\ = 10 + 20 + 10 + 10 + 6 \\ = 56\text{ kHz}$$

$$\therefore \text{BW} = 56\text{ kHz}$$

**10. Ans: (b & c)**

**Sol:** Power in AM =  $P_C + P_{USB} + P_{LSB}$

Power in DSB-SC =  $P_{USB} + P_{LSB}$ , power in SSB-SC =  $P_{USB}$  (or)  $P_{LSB}$

$\therefore$  Power in AM > DSB-SC > VSB = SSB

Option (b) is correct

BW in AM =  $2f_{max}$

BW in DSB-SC =  $2f_{max}$

BW in SSB-SC =  $f_{max}$

BW in VSB-SC =  $f_{max} + \Delta f$

$\therefore$  BW in AM = BW in DSB-SC

> BW of VSB

> BW of SSB

Option (c) is correct

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**11. Ans: (a, c & d)**

**Sol:** For DSB-SC  $\eta = 100\%$

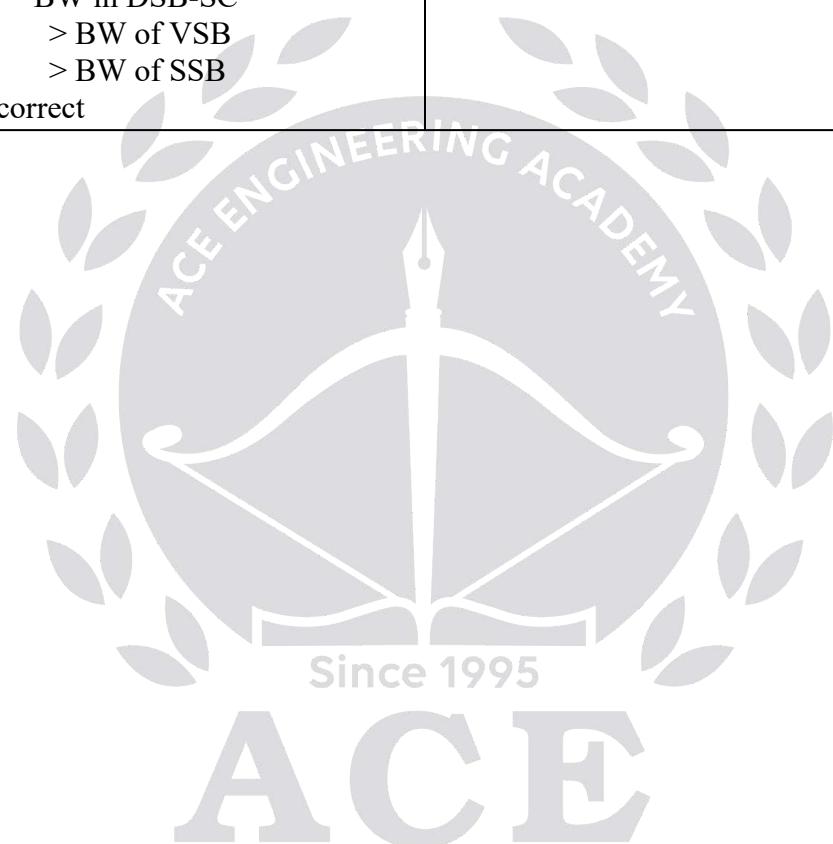
$$BW = 2f_{max} = 2 \times 3 \times 10^4 = 60(\text{kHz})$$

$$S(t) = m(t) c(t)$$

$$= 50 \cos(2\pi \times 10^7 t) \cos(2\pi \times 10^4 t) \\ + 50 \cos(2\pi \times 10^7 t) 5 \cos(5\pi \times 10^4 t) \\ + 50 \cos(2\pi \times 10^7 t) 4 \cos(6\pi \times 10^4 t)$$

$$P_t = 26.25(\text{kW})$$

(a, c & d are correct)



# Chapter 4 Angle Modulation

**01. Ans: (a)**

Sol:  $s(t) = 10 \cos(20\pi t + \pi t^2)$

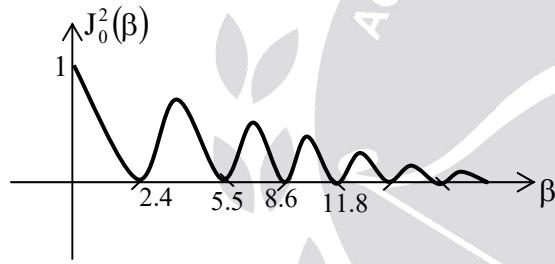
$$f_i = \frac{1}{2\pi} \frac{d\theta_i(t)}{dt}$$

$$f_i = \frac{1}{2\pi} [20\pi + 2\pi t]$$

$$\frac{df_i}{dt} = \frac{1}{2\pi} \times 2\pi \times 1 = 1 \text{ Hz/sec}$$

**02. Ans: (d)**

Sol:  $P_{fc} = \frac{A_c^2 J_0^2(\beta)}{2}$



So,  $J_0^2(\beta)$  is decreasing first, becoming zero and then increasing so power is also behave like  $J_0^2(\beta)$ .

**03. Ans: (a)**

Sol: In an FM signal, adjacent spectral components will get separated by

$$f_m = 5 \text{ kHz}$$

$$\text{Since } BW = 2(\Delta f + f_m) = 1 \text{ MHz}$$

$$= 1000 \times 10^3$$

$$\Delta f + f_m = 500 \text{ kHz}$$

$$\Delta f = 495 \text{ kHz}$$

The  $n^{\text{th}}$  order non-linearity makes the carrier frequency and frequency deviation increased by  $n$ -fold, with the base-band signal frequency ( $f_m$ ) left unchanged since  $n = 3$ ,

$$\therefore (\Delta f)_{\text{New}} = 1485 \text{ kHz} \quad \&$$

$$(f_c)_{\text{New}} = 300 \text{ MHz}$$

$$\text{New BW} = 2(1485 + 5) \times 10^3$$

$$= 2.98 \text{ MHz}$$

$$= 3 \text{ MHz}$$

**04. Ans: (d)**

Sol:  $S(t) = A_c \sum_{n=-\infty}^{\infty} J_n(\beta) \cos 2\pi(f_c + nf_m)t$

$$\Delta f = 3(2f_m) = 12 \text{ kHz}$$

$$\beta = \frac{\Delta f}{f_m} = 6$$

$$\therefore S(t) = \sum_{n=-\infty}^{\infty} 5J_n(6) \cos 2\pi(f_c + nf_m)t$$

$$f_c = 1000 \text{ kHz}, f_m = 2 \text{ kHz}$$

$$= \cos 2\pi(1008 \times 10^3)t$$

$$= \cos 2\pi(1000 + 4 \times 2) \times 10^3 t$$

$$\text{i.e., } n = 4$$

The required coefficient is  $5J_4(6)$

**05. Ans: (c)**

Sol:  $2\pi f_m = 4\pi 10^3$

$$\Rightarrow f_m = 2 \text{ kHz}$$

$$J_0(\beta) = 0 \text{ at } \beta = 2.4$$

$$\beta = \frac{k_f A_m}{f_m} \Rightarrow 2.4 = \frac{k_f \times 2}{2 \text{ kHz}}$$

$$k_f = 2.4 \text{ KHz/V}$$

$$\text{at } \beta = 5.5$$

$$5.5 = \frac{2.4k \times 2}{f_m}$$

$$\Rightarrow f_m = 872.72 \text{ Hz}$$

**06. Ans: (c)**

**Sol:**  $\beta = 6$

$$J_0(6) = 0.1506 ; J_3(6) = 0.1148$$

$$J_1(6) = 0.2767 ; J_4(6) = 0.3576$$

$$J_2(6) = 0.2429 ;$$

$$\frac{P_{f_c \pm 4f_m}}{P_T} = ? \quad P_T = \frac{A_c^2}{2R}$$

$$P_{f_c \pm 4f_m} = \frac{A_c^2}{R} \left[ \frac{J_0^2(\beta)}{2} + J_1^2(\beta) + J_2^2(\beta) + J_3^2(\beta) + J_4^2(\beta) \right]$$

$$P_{f_c \pm 4f_m} = \frac{A_c^2}{R} \left[ \frac{J_0^2(\beta)}{2} + J_1^2(\beta) + J_2^2(\beta) + J_4^2(\beta) \right]$$

$$\frac{P_{f_c \pm 4f_m}}{P_T} = \frac{0.2879}{\frac{1}{2}} = 0.5759 = 57.6 \%$$

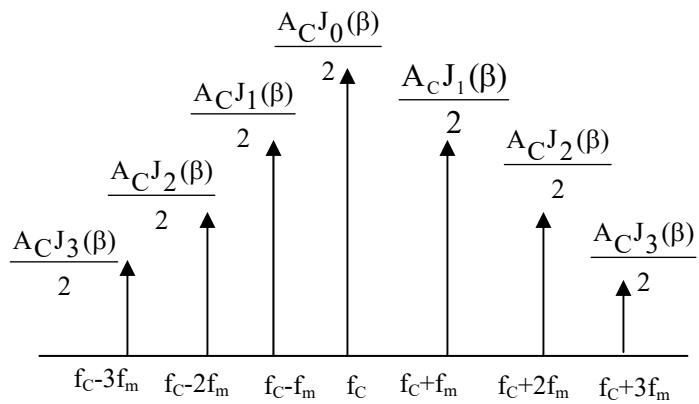
**07. Ans: (c)**

**Sol:**  $m(t) = 10 \cos 20\pi t$

$$f_m = 10 \text{ Hz}$$

inserting correct signal and frequency

$$\beta = \frac{k_f A_m}{f_m} = \frac{5 \times 10}{10} = 5$$



From  $f_c$  to  $f_c + 4f_m$  pass through ideal BPF  
Powers in these frequency components

$$P = \frac{A_c^2}{2R} J_0^2(\beta) + 2 \frac{A_c^2}{2R} J_1^2(\beta) + 2 \frac{A_c^2}{2R} J_2^2(\beta)$$

$$+ 2 \frac{A_c^2}{2R} J_3^2(\beta) + 2 \frac{A_c^2}{2R} J_4^2(\beta)$$

$$= \frac{A_c^2}{2R} \left[ (-0.178)^2 + 2(-0.328)^2 + 2(0.049)^2 \right] + 2(0.365)^2 + 2(0.391)^2$$

$$= 41.17 \text{ Watts}$$

**08. Ans: (d)**

**Sol:**  $P_t = \frac{A_c^2}{2R} (R = 1\Omega)$

$$= \frac{100}{2} = 50 \text{ W}$$

$$\% \text{ Power} = \frac{\text{Power in components}}{\text{total power}} \times 100$$

$$= \frac{41.17}{50} \times 100$$

$$= 82.35\%$$

**09. Ans: (d)**

**Sol:** In frequency modulation the spectrum contains  $f_c \pm nf_1 \pm mf_2$ , where  $n$  &  $m = 0, 1, 2, 3, \dots$

**10. Ans: (c)**

**Sol:** Given  $f_c = 1 \text{ MHz}$

$$f_{\max} = f_c + k_f A_m$$

$$k_p = 2\pi k_f$$

$$k_f = \frac{k_p}{2\pi} = \frac{\pi}{2\pi}$$

$$= \frac{1}{2}$$



$$\begin{aligned}
 &= \left(10^6 + \frac{1}{2} \times 10^5\right) = \left(10^6 + 0.5 \times 10^5\right) \\
 &= \left(10^6 + 5 \times 10^4\right) \\
 &= \left(10^3 + 50\right) 10^3 \\
 &= (10^3 + 50) \text{ k} \\
 &= 1050 \text{ kHz.}
 \end{aligned}$$

$$f_{\min} = f_c - k_f A_m$$

$$\begin{aligned}
 &= \left(10^6 - \frac{1}{2} \times 10^5\right) \\
 &= \left(10^6 - 0.5 \times 10^5\right) \\
 &= \left(10^6 - 5 \times 10^4\right) \\
 &= \left(10^3 - 50\right) 10^3 \\
 &= (10^3 - 50) \text{ k} \\
 &= 950 \text{ kHz}
 \end{aligned}$$

11. Ans: (d)

$$\text{Sol: } \beta = \frac{\Delta f}{f_m}$$

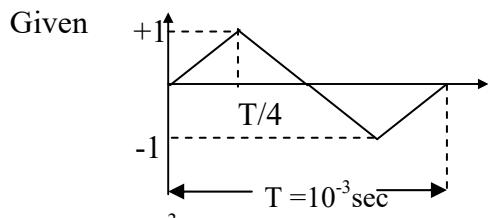
$$\Delta \phi = \frac{\Delta f}{f_m}$$

$$\Delta f = \Delta \phi f_m$$

$$= k_p A_m f_m$$

12. Ans: (c)

Sol: Given



$$f_c = 100 \times 10^3 \text{ Hz}$$

$$k_f = 10 \times 10^3 \text{ Hz}$$

$$m(t)|_{\max} = +1, m(t)|_{\min} = -1$$

$$\begin{aligned}
 f_i &= f_c \pm \Delta f \\
 &= f_c \pm k_f A_m \\
 &= 100 \times 10^3 \pm 10 \times 10^3 (\text{m}(t)) \\
 &= 110 \text{ kHz} \& 90 \text{ kHz}
 \end{aligned}$$

13. Ans: (c)

$$\text{Sol: } S(t) = A_c \cos (2\pi f_c t + k_p m(t))$$

$$\begin{aligned}
 f_i &= \frac{1}{2\pi} \frac{d}{dt} \theta_i(t) \quad \overbrace{\theta_i(t)} \\
 &= \frac{1}{2\pi} \frac{d}{dt} (2\pi f_c t + k_p m(t)) \\
 &= f_c + \frac{1}{2\pi} k_p \frac{d}{dt} m(t) \\
 f_{\max} &= f_c + \frac{k_p}{2\pi} \frac{1}{\left(\frac{10^{-3}}{4}\right)} = f_c + \frac{k_p}{2\pi} \times 4 \times 10^3 \\
 &= 100 \text{ kHz} + \frac{\pi}{2\pi} \times 4 \times 10^3 \\
 &= 102 \text{ kHz} \\
 f_{\min} &= f_c - k_p \frac{1}{\left(\frac{10^{-3}}{4}\right)} \\
 &= f_c - 2 \text{ kHz} \\
 f_{\min} &= 98 \text{ kHz}
 \end{aligned}$$

14. Ans: (c)

Sol: Given,

$$S(t) = A_c \cos (\theta_i(t))$$

$$= A_c \cos (\omega_c t + \phi(t))$$

$$m(t) = \cos (\omega_m t)$$

$$f_i(t) = f_c + 2\pi k (f_m)^2 \cos \omega_m t$$

$$f_i = \frac{1}{2\pi} \frac{d\theta_i(t)}{dt}$$



$$\theta_i(t) = \int 2\pi f_i(t) dt$$

$$\theta_i(t) = \int 2\pi [f_c + 2\pi k(f_m)^2 \cos \omega_m t] dt$$

$$\theta_i(t) = 2\pi f_c t + (2\pi f_m)^2 k \frac{\cos \omega_m t}{\omega_m}$$

$$\theta_i(t) = \omega_c t + \omega_m k \sin \omega_m t$$

15. Ans: (b)

Sol:  $\Delta f_{\max} = K_f |m(t)|_{\max}$

$$= \frac{100}{2\pi} \times [10]$$

$$\Delta f_{\max} = \left( \frac{500}{\pi} \right) \text{Hz}$$

16. Ans: (b)

Sol: Given that

$$s(t) = \cos[\omega_c t + 2\pi m(t)] \text{volts}$$

$$f_i = \frac{1}{2\pi} \frac{d}{dt} [\omega_c t + 2\pi m(t)]$$

$$= \frac{1}{2\pi} \frac{d}{dt} [2\pi f_c t + 2\pi m(t)]$$

$$f_i = f_c + \frac{d}{dt} [m(t)]$$

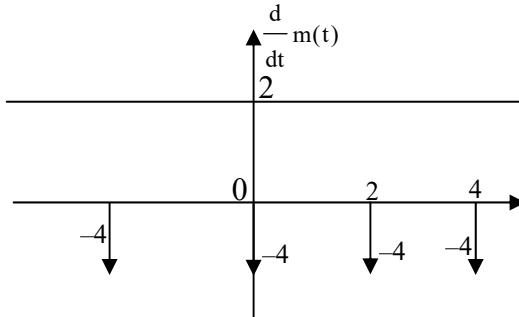
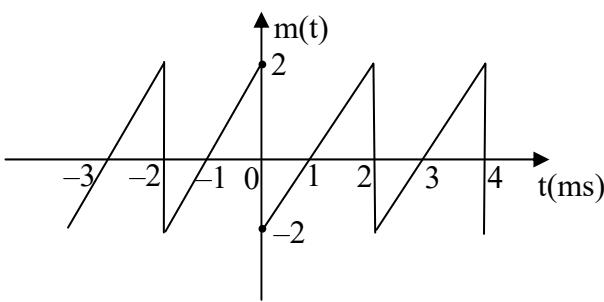
we know that  $f_i = f_c + k_f m(t)$

$$\text{Here } k_f m(t) = \frac{d}{dt} [m(t)]$$

$$\Delta f = \max \{k_f m(t)\}$$

$$\Delta f = \max \left[ \frac{d}{dt} m(t) \right]$$

$$\Delta f = 2 \text{kHz}$$



17. Ans: (a)

Sol:  $\beta_p = k_p \max [|m(t)|] = 1.5 \times 2 = 3$

$$\beta_f = \frac{k_f \max [|m(t)|]}{f_m}$$

$$= \frac{3000 \times 2}{1000} \\ = 6$$

18. Ans: (a)

Sol: Using Carson's rule we obtain

$$\text{BW}_{PM} = 2(\beta_p + 1)f_m = 8 \times 1000 = 8000 \text{Hz}$$

$$\text{BW}_{FM} = 2(\beta_f + 1)f_m = 14 \times 1000 = 14000 \text{Hz}$$

19. Ans: 70 kHz

Sol:  $s(t) = A_c \cos[2\pi f_c t + k_p m(t)]$

$$f_i = f_c + \frac{k_p}{2\pi} \frac{d}{dt} x(t) \\ = 20k + \frac{5}{2\pi} \times 5 \frac{d}{dt} (\sin 4\pi 10^3 t - 10\pi \cos 2\pi 10^3 t) \\ = 20k + \frac{25}{2\pi} \times \left[ \cos(4\pi 10^3 t - 10\pi \cos 2\pi 10^3 t) \right. \\ \left. (4\pi 10^3 + 10\pi \sin 2\pi 10^3 t \times 2\pi 10^3) \right]$$

$$f_{i(t=0.5\text{ms})} = 20k + \frac{25}{2\pi} \times \cos(4\pi + 10\pi) \times 4\pi \times 10^3$$

$$= 20k + \frac{25}{2\pi} \times 4\pi \times 10^3$$

$$= 20k + 50k$$

$$f_{i(t=0.5\text{ms})} = 70 \text{kHz}$$

**20. Ans: (a, b & c)**

**Sol:**  $s(t) = 100\cos[2\pi \times 10^7 t + 10\sin(8\pi \times 10^3 t)]$

$$\Delta f_i(t) = \frac{1}{2\pi} \frac{d}{dt} [10\sin(8\pi \times 10^3 t)]$$

$$\Delta f_i(t) = 40 \times 10^3 \cos[8\pi \times 10^3 t]$$

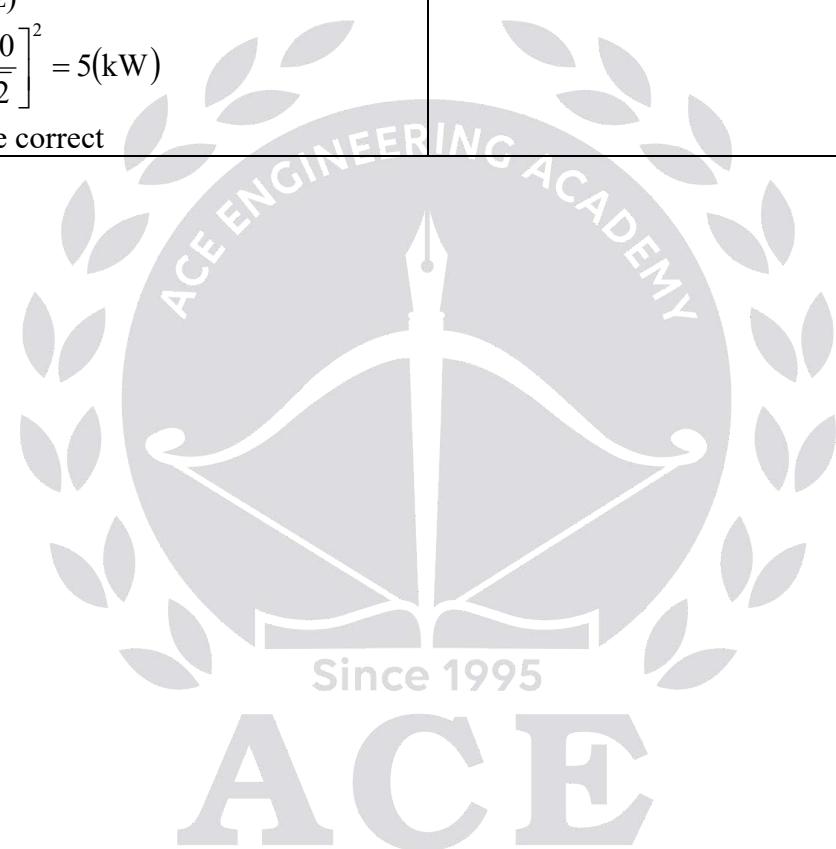
$$\Delta f_{\max} = 40(\text{kHz})$$

$$\beta = \frac{\Delta f_{\max}}{f_{\max}} = \frac{40 \times 10^3}{4 \times 10^3} = 10$$

$$\text{BW} = 2[\beta+1] f_{\max} = 2 [10 + 1] 4 \times 10^3 \\ = 88(\text{kHz})$$

$$P_T = P_C = \left[ \frac{100}{\sqrt{2}} \right]^2 = 5(\text{kW})$$

$\therefore$  a, b & c are correct

**21. Ans: (a, c & d)**

# Chapter

# 5

# Radio Receivers

**01. Ans: (d)**

**Sol:** The image channel selectivity of super heterodyne receiver depends upon Pre selector and RF amplifier only.

**02. Ans: (b)**

**Sol:** The image (second) channel selectivity of a super heterodyne communication receiver is determined by the pre selector and RF amplifier.

**03. Ans: (d)**

**Sol:** Given  $f_s = 4$  to  $10$  MHz

$$\text{IF} = 1.8 \text{ MHz}$$

$$f_{si} = ?$$

$$\begin{aligned} f_{si} &= f_s + 2 \times \text{IF} \\ &= 7.6 \text{ MHz} \text{ to } 13.6 \text{ MHz} \end{aligned}$$

**04. Ans: (a)**

**Sol:** Image frequency  $f_{si} = f_s + 2 \times \text{IF}$

$$\begin{aligned} &= 700 \times 10^3 + 2(450 \times 10^3) \\ &= 1600 \text{ kHz} \end{aligned}$$

Local oscillator frequency,  $f_l = f_s + \text{IF}$

$$\begin{aligned} (f_l)_{\max} &= (f_s)_{\max} + \text{IF} = 1650 + 450 \\ &= 2100 \text{ kHz} \end{aligned}$$

$$\begin{aligned} (f_l)_{\min} &= (f_s)_{\min} + \text{IF} = 550 + 450 \\ &= 1000 \text{ kHz} \end{aligned}$$

$$R = \frac{C_{\max}}{C_{\min}} = \left( \frac{f_{l_{\max}}}{f_{l_{\min}}} \right)^2 = \left( \frac{2100}{1000} \right)^2 = 4.41$$

**05. Ans: (a)**

**Sol:**  $f_s(\text{range}) = 88 - 108 \text{ MHz}$

Given condition  $f_{IF} < f_{LO}$ ,  $f_{si} > 108 \text{ MHz}$

$$f_{si} = f_s + 2 \times \text{IF}$$

$$f_{si} > 108 \text{ MHz}$$

$$f_s + 2\text{IF} > 108 \text{ MHz}$$

$$88 \text{ MHz} + 2 \times \text{IF} > 108 \text{ MHz}$$

$$\text{IF} > 10 \text{ MHz}$$

Among the given options IF =  $10.7 \text{ MHz}$

**06. Ans: (a)**

**Sol:** Range of variation in local oscillator frequency is

$$\begin{aligned} f_{L_{\min}} &= f_{s_{\min}} + \text{IF} \\ &= 88 + 10.7 \end{aligned}$$

$$f_{L_{\min}} = 98.7 \text{ MHz}$$

$$\begin{aligned} f_{L_{\max}} &= f_{s_{\max}} + \text{IF} \\ &= 108 + 10.7 \end{aligned}$$

$$f_{L_{\max}} = 118.7 \text{ MHz}$$

**07. Ans: 5**

**Sol:**  $f_s = 58 \text{ MHz} - 68 \text{ MHz}$

When  $f_s = 58 \text{ MHz}$

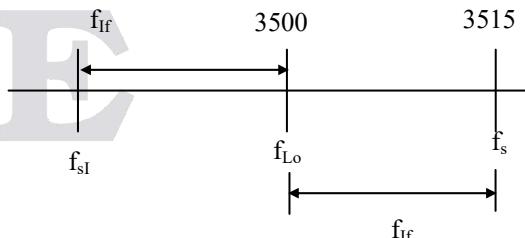
$$f_{si} = f_s + 2\text{IF} > 68 \text{ MHz}$$

$$2\text{IF} > 10 \text{ MHz}$$

$$\text{IF} \geq 5 \text{ MHz}$$

**08. Ans: 3485 MHz**

**Sol:**



$$f_{If} = 15 \text{ MHz}$$

$$f_{Lo} = 3500 \text{ MHz}$$

$$f_s - f_{Lo} = f_{If}$$

$$f_s = f_{Lo} + f_{If} = 3515 \text{ MHz}$$

$$\begin{aligned} f_{si} &= \text{image frequency} = f_s - 2 f_{If} \\ &= 3515 - 2 \times 15 \\ &= 3485 \text{ MHz} \end{aligned}$$

**09. Ans: (a, b & c)**

Sol:  $\rightarrow f_{IM} = f_S + 2f_{IF} = 555 \times 10^3 + 2(455 \times 10^3)$   
 $= 1465 \text{ kHz}$

$$\rightarrow f_{IF} = f_{lo} - f_S = 1010 \times 10^3 - 555 \times 10^3$$
 $= 455 \times 10^3 \text{ Hz}$

$$\rightarrow IRR = \sqrt{1+Q^2\rho^2} = 113$$

$$Q = 50$$

$$\rho = \frac{f_{IM}}{f_S} - \frac{f_S}{f_{IM}} = \frac{1465}{555} - \frac{555}{1465}$$

$\therefore$  a, b & c are correct.

**10. Ans: (b & c)**

Sol:  $\rightarrow f_{lo} - f_S = f_{IF}$   
 $f_{lo} = f_{IF} + f_S$   
 $= 555 \times 10^3 + 1500 \times 10^3$   
 $= 2055 \text{ kHz}$

$$\rightarrow f_{IM} = f_S + 2f_{IF}$$
 $= 1500 \times 10^3 + 2(555 \times 10^3)$ 
 $= 2610 \text{ kHz}$

$\therefore$  b & c are correct.



# Chapter 6 Baseband Data Transmission

**01. Ans: (d)**

$$\text{Sol: } \Delta = \frac{V_{\max} - V_{\min}}{2^n}$$

$$\Delta \propto \frac{1}{2^n}; \quad \frac{\Delta_1}{\Delta_2} = \frac{2^{n_2}}{2^{n_1}}$$

$$\frac{0.1}{\Delta_2} = \frac{2^{n+3}}{2^n}$$

$$\Delta_2 = 0.1 \times \frac{1}{8} \\ = 0.0125$$

**02. Ans: (3)**

$$\text{Sol: } (\text{BW})_{\text{PCM}} = \frac{n f_s}{2}$$

Where 'n' is the number of bits to encode the signal and  $L = 2^n$ , where 'L' is the number of quantization levels.

$$L_1 = 4 \Rightarrow n_1 = 2$$

$$L_2 = 64 \Rightarrow n_2 = 6$$

$$\frac{(\text{BW})_2}{(\text{BW})_1} = \frac{n_2}{n_1} = \frac{6}{2} = 3$$

$$(\text{BW})_2 = 3 (\text{BW})_1$$

**03. Ans: (c)**

**Sol:** Given,

Two signals are sampled with  $f_s = 44100 \text{ s/sec}$  and each sample contains '16' bits

Due to additional bits there is a 100% overhead.

Output bit rate =?

$$R_b = n |f_s|$$

$$|f_s| = 2f_s = 2 [44100]$$

( $\because$  two signals sampled simultaneously)

$$n^l = 2n$$

( $\because$  due to overhead by additional bits)

$$R_b = 4 (nf_s) = 2.822 \text{ Mbps}$$

**04. Ans (c)**

**Sol:** Number of bits recorded over an hour  
 $= R_b \times 3600 = 10.16 \text{ G.bits}$

**05. Ans: (c)**

$$\text{Sol: } p(t) = \frac{\sin(4\pi W t)}{4\pi W t (1 - 16W^2 t^2)}$$

$$\text{At } t = \frac{1}{4W}; P\left(\frac{1}{4W}\right) = \frac{0}{0}$$

Use L-Hospital Rule

$$\begin{aligned} \lim_{t \rightarrow \frac{1}{4W}} p(t) &= \lim_{t \rightarrow \frac{1}{4W}} \frac{4\pi W \cos(4\pi W t)}{4\pi W - 64\pi W^3 (3t^2)} \\ &= \frac{4\pi W (-1)}{4\pi W - 64\pi W^3 3\left(\frac{1}{16W^2}\right)} \\ &= \frac{-4\pi W}{-8\pi W} = 0.5 \end{aligned}$$

**06. Ans: 35**

**Sol:** Given bit rate  $R_b = 56 \text{ kbps}$ , Roll off factor  $\alpha = 0.25$   
 BW required for base band binary PAM system

$$\text{BW} = \frac{R_b}{2} [1 + \alpha] = \frac{56}{2} [1 + 0.25] \text{ kHz} = 35 \text{ kHz}$$

**07. Ans: 16**

**Sol:**  $R_b = nf_s = 8 \text{ bit/sample} \times 8 \text{ kHz} = 64 \text{ kbps}$

$$\begin{aligned} (B_T)_{\min} &= \frac{R_b}{2 \log_2 M} \\ &= \frac{R_b}{2 \log_2 4} = \frac{R_b}{2 \times 2} \\ &= \frac{R_b}{4} = \frac{64}{4} \\ &= 16 \text{ kHz} \end{aligned}$$

**08. Ans: (b)**

**Sol:** Given  $f_s = 1/T_s = 2k$  symbols/sec

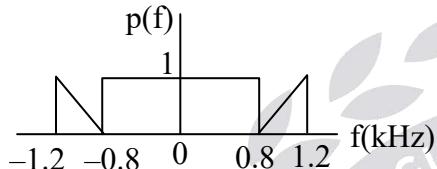
$$\text{If } P(f) \xrightarrow{\text{F.T.}} p(t),$$

Condition for zero ISI is given by

$$\frac{1}{T_s} \sum_{n=-\infty}^{\infty} P(f - n/T_s) = p(0)$$

$$\Rightarrow \sum_{n=-\infty}^{\infty} P(f - n/T_s) = p(0)T_s$$

$p(0) = \text{area under } P(f)$

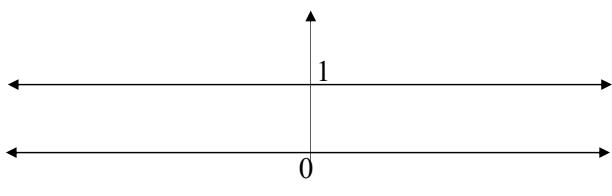
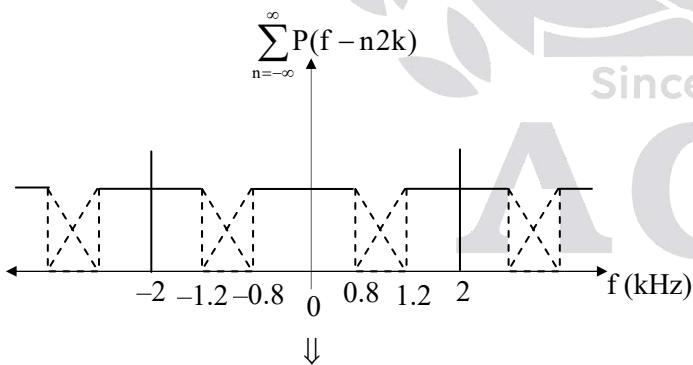


$$\text{Area} = 2 \times \frac{1}{2} (1)(0.4)k + 2 \times 0.8k = 2k$$

$$p(0) T_s = 2k \times \frac{1}{2k} = 1$$

$$\Rightarrow \sum_{n=-\infty}^{\infty} P(f - n/T_s) = 1$$

The above condition is satisfied by only option (b)



$$\therefore \sum_{n=-\infty}^{\infty} P(f - n2k) = 1$$

Option (a) is correct if pulse duration is from -1 to +1

Option (c) is correct if the transition is from 0.8 to 1.2, -0.8 to -1.2

Option (d) is correct if the triangular duration is from -2 to +2

**09. Ans: 200**

**Sol:**  $m(t) = \sin 100\pi t + \cos 100\pi t$

$$= \sqrt{2} \cos [100\pi t + \phi]$$

$$\Delta = 0.75 = \frac{V_{\max} - V_{\min}}{L} = \frac{\sqrt{2} - (-\sqrt{2})}{L} = \frac{2\sqrt{2}}{L}$$

$$L = \frac{2\sqrt{2}}{0.75} \approx 4 = 2^n$$

$$\text{So } n = 2$$

$$f = 50 \text{ Hz so Nyquist rate} = 100$$

$$\text{So, the bit rate} = 100 \times 2 = 200 \text{ bps}$$

**10. Ans: (b)**

**Sol:** Given

$$f_{m_1} = 3.6 \text{ kHz} \Rightarrow f_{s_1} = 7.2 \text{ kHz}$$

$$f_{m_2} = f_{m_3} = 1.2 \text{ kHz} \Rightarrow f_{s_2} = f_{s_3} = 2.4 \text{ kHz}$$

$$f_s = f_{s_1} + f_{s_2} + f_{s_3}$$

$$= 12 \text{ kHz}$$

$$\text{No. of Levels used} = 1024$$

$$\Rightarrow n = 10 \text{ bits}$$

$$\therefore \text{Bit rate} = nf_s$$

$$= 10 \times 12 \text{ kHz}$$

$$= 120 \text{ kbps}$$

**11. Ans: (a)**

**Sol:**  $(f_s)_{\min} = (f_{s_1})_{\min} + (f_{s_2})_{\min}$

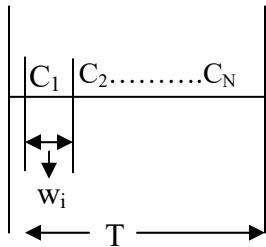
$$+ (f_{s_3})_{\min} + (f_{s_4})_{\min}$$

$$= 200 + 200 + 400 + 800$$

$$= 1600 \text{ Hz}$$

12. Ans: (c)

Sol:



$$\text{Minimum B.W of TDM is } \sum_{i=1}^N w_i$$

13. Ans: (b)

Sol: Number of patients = 10

ECG signal B.W = 100Hz

$$(Q_e)_{\max} \leq (0.25) \% V_{\max}$$

$$\frac{2V_{\max}}{2 \times 2^n} \leq \frac{0.25}{100} V_{\max}$$

$$2^n \geq 400$$

$$n \geq 8.64$$

$$n = 9$$

$$\begin{aligned} \text{Bit rate of transmitted data} &= 10 \times 9 \times 200 \\ &= 18 \text{ kbps} \end{aligned}$$

14. Ans: (a)

Sol: Peak amplitude  $\rightarrow A_m$

Peak to peak amplitude  $A_m$

$$\frac{-\Delta}{2} \leq Q_e \leq \frac{\Delta}{2}$$

$$\text{PCM maximum tolerable } \frac{\Delta}{2} = 0.2\% A_m$$

$$\Delta = \frac{\text{Peak to peak}}{L} \Rightarrow \frac{2A_m}{2L} = \frac{0.2}{100} A_m$$

$$(\because \Delta = \frac{2A_m}{L})$$

$$\Rightarrow L = 500$$

$$2^n = 500$$

$$n = 9$$

$$R_b = n(f_s)_{TDM} + 9$$

$$f_s = R_N + 20\% R_N = R_N + 0.2 R_N$$

$$f_s = 1.2 R_N = 1.2 \times 2 \times \omega$$

$$f_s = 2.4 \text{ K samples/sec}$$

$$(f_s)_{TDM} = 5(f_s)$$

$$= 5 \times 2.4 \text{ K}$$

$$= 12 \text{ K sample/sec}$$

$$R_b = (nf_s) + 0.5\%(nf_s)$$

$$= (9 \times 12k) + \frac{0.5}{100} (9 \times 12k)$$

$$= 108540 \text{ bps}$$

15. Ans: (b)

Sol: To avoid slope over loading, rate of rise of the o/p of the Integrator and rate of rise of the Base band signal should be the same.

$\therefore \Delta f_s$  = slope of base band signal

$$\Delta \times 32 \times 10^3 = 125$$

$$\Delta = 2^{-8} \text{ Volts.}$$

16. Ans: (b)

Sol:  $x(t) = E_m \sin 2\pi f_m t$

$$\frac{\Delta}{T_s} < \left| \frac{dm(t)}{dt} \right| \rightarrow \text{slope overload distortion}$$

takes place

$$\Delta f_s < E_m 2\pi f_m$$

$$\Rightarrow \frac{\Delta f_s}{2\pi} < E_m f_m \quad (\because \Delta = 0.628)$$

$$\Rightarrow \frac{0.628 \times 40K}{2\pi} < E_m f_m$$

$$f_s = 40 \text{ kHz} \Rightarrow 4 \text{ kHz} < E_m f_m$$

Check for options

- (a)  $E_m \times f_m = 0.3 \times 8 \text{ K} = 2.4 \text{ kHz}$   
(4K < 2.4 K)
- (b)  $E_m \times f_m = 1.5 \times 4\text{K} = 6 \text{ kHz}$   
(4K < 6 K) correct
- (c)  $E_m \times f_m = 1.5 \times 2 \text{ K} = 3 \text{ kHz}$   
(4K < 3K)
- (d)  $E_m \times f_m = 30 \times 1 \text{ K} = 3 \text{ kHz}$   
(4K < 3K)

**17. Ans: (a)**

**Sol:** Given

$$m(t) = 6 \sin(2\pi \times 10^3 t) + 4 \sin(4\pi \times 10^3 t)$$

$$\Delta = 0.314 \text{ V}$$

$$\text{Maximum slope of } m(t) = \frac{d}{dt}(m(t)) / t = \frac{\pi}{2}$$

$$= 2\pi \times 10^3 (6) + 4\pi \times 10^3 [4] = 28\pi \times 10^3$$

**18. Ans: (c)**

**Sol:** Pulse rate which avoid distortion

$$\Delta f_s = \frac{d}{dt} m(t)$$

$$f_s = \frac{28\pi \times 10^3}{0.314}$$

$$f_s = 280 \times 10^3 \text{ pulses/sec}$$

**19. Ans: (a, b & c)**

**Sol:** a.  $r_b = (Nn + EB)f_s$

$$r_b = (80 + 5) 5000 = 425(\text{kbps})$$

b.  $r_b = Nnf_s$

$$r_b = 10(8+1) 5000 = 450(\text{kbps})$$

c.  $r_b = (Nn + EB)f_s$

$$r_b = (80 + 10) 5000 = 450(\text{kbps})$$

d.  $r_b = Nnf_s$

$$r_b = 10(8+0.8) 5000 = 440(\text{kbps})$$

$\therefore$  a, b & c are correct

**20. The message signal**

$$m(t) = \text{Sinc}(400t) \times \text{Sinc}(600t)$$

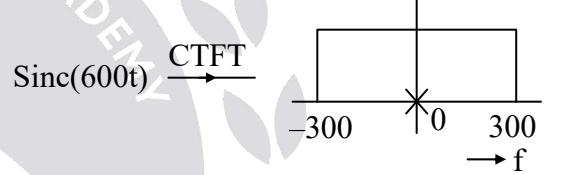
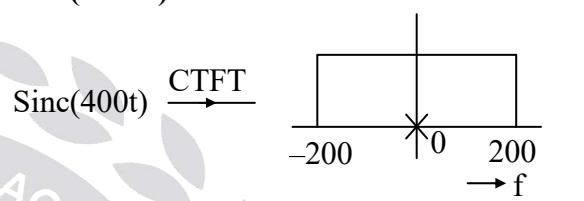
is sampled then which of the following option is/are correct.

**NOTE:** options are changed

- (a) Nyquist rate = 2 kHz
- (b) Nyquist rate = 1 kHz
- (c) Nyquist interval = 0.5 ms
- (d) Nyquist interval = 1 ms

**20. Ans: (b & d)**

**Sol:**



$M(f)$  frequency will range from  
-500 to 500 Hz

$$\therefore f_q = 2f_{\max} = 1 \text{ kHz}$$

$$T_{\text{MAX}} = \frac{1}{f_q} = 1 \text{ ms}$$

b & d are correct

# Chapter

# 7

# Bandpass Data Transmission

**01.** Ans: (c)

Sol:  $(BW)_{BPSK} = 2f_b = 20 \text{ kHz}$   
 $(BW)_{QPSK} = f_b = 10 \text{ kHz}$

**02.** Ans: (b)

Sol:  $f_H = 25 \text{ kHz}; f_L = 10 \text{ kHz}$

∴ Center frequency

$$= \left( \frac{25+10}{2} \right) \text{ kHz}$$

$$= 17.5 \text{ kHz}$$

∴ Frequency offset,

$$\Omega = 2\pi (25 - 17.5) \times 10^3$$

$$= 2\pi (7.5) \times 10^3$$

$$= 15 \times 10^3 \pi \text{ rad/sec.}$$

The two possible FSK signals are orthogonal, if  $2\Omega T = n\pi$

$$\Rightarrow 2(15\pi) \times 10^3 \times T = n\pi$$

$$\Rightarrow 30 \times 10^3 \times T = n \text{ (integer)}$$

This is satisfied for,  $T = 200 \mu\text{sec.}$

**03.** Ans: (a)

Sol:  $r_b = 8 \text{ kbps}$

Coherent detection

$$\Delta f = \frac{n r_b}{2}$$

Best possible  $n = 1$

$$\Delta f = \frac{8K}{2} = 4K$$

To verify the options  $\Delta f = 4k$

i.e.  $f_{C2} - f_{C1} = 4K$

(a)  $20 \text{ K} - 16 \text{ K} = 4 \text{ K}$

(b)  $32 \text{ K} - 20 \text{ K} = 12 \text{ K}$

(c)  $40 \text{ K} - 20 \text{ K} = 20 \text{ K}$

(d)  $40 \text{ K} - 32 \text{ K} = 8 \text{ K}$

**04.** Ans: (a)

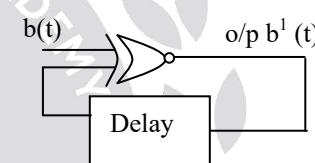
Sol: Non coherent detection of PSK is not possible. So to overcome that, DPSK is implemented. A coherent carrier is not required to be generated at the receiver.

**05.** Ans: (c)

Sol: In QPSK baud rate =  $\frac{\text{bit rate}}{2} = \frac{34}{2} = 17 \text{ Mbps}$

**06.** Ans: (d)

Sol:



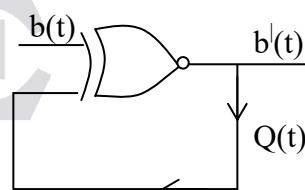
b(t)	0	1	0	0	1
b^1(t)(Ref.bit)	0	0	1	0	0
Phase	$\pi$	$\pi$	0	$\pi$	$\pi$

**07.** Ans: (b)

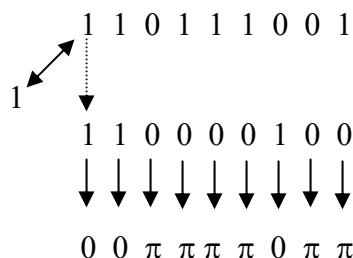
Sol: Given

Bit stream 110 111001

Reference bit = 1



$$b^1(t) = b(t) \odot Q(t)$$



**08. Ans: (d)**

Sol:  $r_b = 1.544 \times 10^6$

$$\alpha = 0.2$$

$$BW = \frac{r_b}{\log_2 M} (1 + \alpha)$$

$$= \frac{1.544 \times 10^6}{2} (1 + 0.2) \quad (\because M = 4)$$

$$BW = 926.4 \times 10^3 \text{ Hz}$$

**09. Ans: 0.25**

Sol:  $BW = 1500 \text{ Hz}$

BW required for M-ary PSK is

$$\frac{R_b [1 + \alpha]}{\log_2 16} = 1500 \text{ Hz}$$

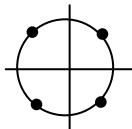
$$\Rightarrow R_b [1 + \alpha] = 1500 \times 4 = 6000$$

$$\Rightarrow (1 + \alpha) = \frac{6000}{4800}$$

$$\text{Roll off factor} \Rightarrow \alpha = \frac{6000}{4800} - 1 = 0.25$$

**10. Ans: (b)**

Sol:



Here only phase is changing.

From options (b) is the optimum answer.

**11. Ans: (b)**

Sol: Here 16-points are available in constellation which are varying in both amplitude and phase. So, it 16QAM.

**12. Ans: (d)**

Sol:  $BW = \frac{r_b}{\log_2 M} (1 + \alpha)$

$$36 \times 10^6 = \frac{r_b}{2} (1 + 0.2) \quad (\because M = 4, \text{QPSK})$$

$$r_b = 60 \times 10^6 \text{ bps}$$

**NOTE: new question 13<sup>th</sup> is added in text book**

13. Which among the following modulation schemes consume less bandwidth

- (a) B-PSK
- (b) Q-PSK
- (c) 64-PSK
- (d) 64-QAM

**13. Ans: (c & d)**

Sol: Bandwidth of 64-PSK =  $\frac{2r_b}{6} = \frac{r_b}{3}$

Bandwidth 64-QAM = Bandwidth of 64-PSK

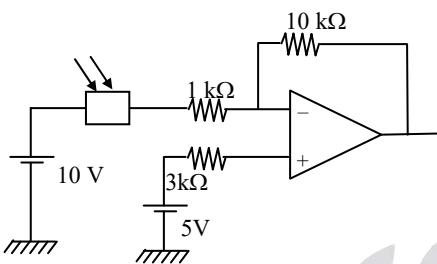
**14. Ans: (a, b & d)**

Sol: M-ary ASK constellation plot will always come on a single line (either x-axis or y-axis).

# Chapter 9 Optical Sources & Detectors

01.

Sol:



1<sup>st</sup> case:

$$R_p \rightarrow 1 \text{ k}\Omega, \text{ no } 10 \text{ V source}$$

2<sup>nd</sup> case:

$$R_p \rightarrow 5 \text{ k}\Omega \rightarrow 10 \text{ V source is present}$$

$$\text{So, } V = V_{01(\text{Only } 10\text{V})} + V_{02(\text{Only } 5\text{V})}$$

$$V = \frac{-10 \text{ k}\Omega}{1 \text{ k}\Omega + R_p}$$

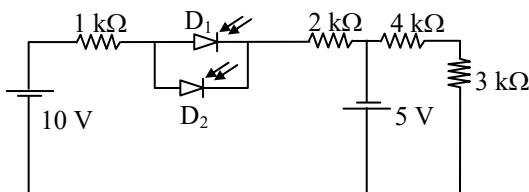
$$= \left( \frac{-10 \text{ k}\Omega}{1 \text{ k}\Omega + 5 \text{ k}\Omega} \right) \times 10 + \left( 1 + \frac{10 \text{ k}\Omega}{1 \text{ k}\Omega + 1 \text{ k}\Omega} \right) \times 5$$

$$V = \left( \frac{-10 \text{ k}\Omega}{6 \text{ k}\Omega} \times 10 \right) + \left( 1 + \frac{10 \text{ k}\Omega}{2 \text{ k}\Omega} \right) \times 5$$

$$V = 13.33 \text{ V}$$

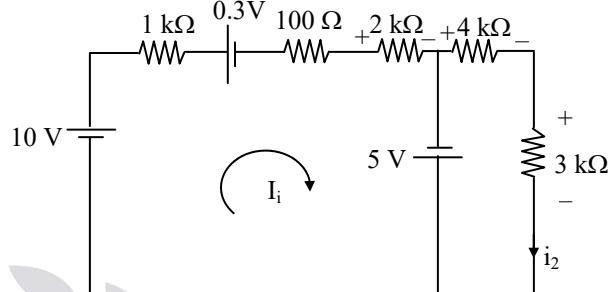
02.

Sol:



D<sub>1</sub>, D<sub>2</sub> are in forward bias

D<sub>2</sub>-ON, D<sub>1</sub>-OFF



$$V_{2k} = ?$$

$$V_{3k} = ?$$

$$i_2 = \frac{-5 \text{ V}}{4 \text{ k}\Omega + 3 \text{ k}\Omega} = \frac{-5 \text{ V}}{7 \text{ k}\Omega} = -0.714 \text{ mA}$$

$$V_{3k} = i_2 \times 3 \text{ k}\Omega \\ = (-0.714) \times 3 \times 10^3 \\ = -2.14 \text{ V}$$

From circuit

$$I_i = 1.41 \text{ mA}$$

So

$$V_{2k} = 1.41 \text{ mA} \times 2 \text{ k}\Omega = 2.8 \text{ V}$$

03. Ans: (c)

Sol: Given data.

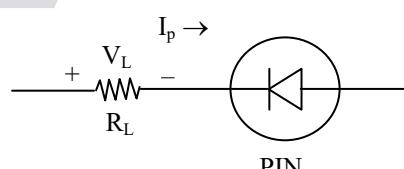
$$C_j = 6 \text{ pF}$$

$$A = 10 \text{ mm}^2$$

$$R = 0.5 \text{ A/W}$$

$$I = 1 \text{ mW/cm}^2$$

$$R_L = 100 \text{ k}\Omega$$



$$V_L = ?$$

We know

$$V_L = I_p \times R_L$$

$$R = \frac{I_p}{P_0}$$

$$P_0 = A \times I$$



$$I_p = \frac{0.5A}{W} \times A \times I$$

$$I_p = \frac{0.5A}{W} \times 10\text{ mm}^2 \times \frac{1\text{ mW}}{10\text{ mm}^2}$$

$$I_p = \left( 0.5 \times \frac{10}{100} \times 1\text{ m} \right) \text{Amp}$$

$$I_p = 5 \times 10^{-5} \text{ amp}$$

$$V_L = I_p \times R_L = 5 \times 10^{-5} \times 100 \text{ k}\Omega$$

$$\therefore V_L = 5 \text{ volts}$$

**04. Ans: (c)**

**Sol:** Given:

$$\eta = 0.65$$

$$\lambda = 900 \text{ nm}$$

$$P_0 = 0.5 \mu\text{W}$$

$$I_m = 10 \mu\text{A}$$

$$M = ?$$

$$M = \frac{I_m}{I_p} = \frac{10 \mu\text{A}}{I_p}$$

We know

$$\eta = \frac{EI_p}{P_0 q}$$

$$0.65 = \frac{hcI_p}{\lambda P_0 q}$$

$$\Rightarrow 0.65 = \left( \frac{6.6 \times 10^{-34} \times 3 \times 10^8}{900 \times 0.5 \times 10^{-6} \times 1.6 \times 10^{-19}} \right) \times I_p$$

$$\Rightarrow I_p = 2.36 \times 10^{-7}$$

$$M = \frac{10 \mu\text{A}}{2.36 \times 10^{-7} \text{ A}}$$

$$= 42.4 \approx 43$$

**05. Ans: -1V**

**Sol:** Output is independent  $V_r$

**06. Ans: 2**

**Sol:** Given

$$\text{Area} = 10 \text{ mm}^2$$

$$\text{Sensitivity} = 0.5 \text{ A/W}$$

$$\text{Intensity} = 4 \text{ W/m}^2$$

Photodiode current

$$I_p = \text{Area} \times \text{sensitivity} \times \text{Intensity}$$

$$I_p = 10 \text{ mm}^2 \times 0.5 \text{ A/W} \times 4 \text{ W/m}^2$$

$$I_p = 20 \mu\text{A}$$

I to V converter sensitivity is 100 mV/ $\mu\text{A}$

$$\text{So, } V_o = \frac{100 \text{ mV}}{\mu\text{A}} \times 20 \mu\text{A}$$

$$= 2 \text{ Volt}$$

**07. Ans: 75.18**

$$\text{Sol: } \frac{I}{P} = \frac{\eta e \lambda}{hc}$$

$$I = \frac{\eta e \lambda}{hc} \times P$$

$$= \frac{0.75 \times 1.6 \times 10^{-19} \times 830 \times 10^{-9} \times 100 \times 10^{-6}}{6.624 \times 10^{-34} \times 2 \times 10^8}$$

$$I = 75.18 \mu\text{A}$$

**08. Ans: (a, b & d)**

**Sol:** The sensitivity of photovoltaic cell is almost constant when it is short circuited & is almost negligible when the load resistance is about 10 k $\Omega$ . The sensitivity of a photovoltaic cell decreases with increase of load resistance.

**09. Ans: (a & b)**

**Sol:** The photodiode is used in the detection of both visible & invisible light.

# Chapter 10

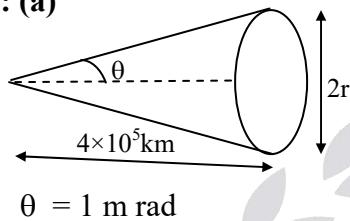
# LED's & LASERS

**01. Ans: (b)**

Sol:  $2i = 115^\circ .34' = 115.566^\circ$ ,  
 $i = 57.783^\circ$ ,  $u = \tan i = \tan 57.783^\circ$   
 $= 1.587$

**02. Ans: (a)**

Sol:



$$\theta = 1 \text{ m rad}$$

$$\tan\theta = \frac{r}{4 \times 10^5 \times 1000} = 1 \text{ mrad}$$

$$(\tan\theta \approx \theta)$$

$$r = 4 \times 10^5 \text{ meters}$$

$$= 400 \text{ km}$$

$$\text{Diameter} = 2 \times r$$

$$= 2 \times 400 \text{ km}$$

$$= 800 \text{ km}$$

**03. Ans: (b)**

Sol: Given:

$$L = 500 \text{ mm}$$

$$\text{Bandwidth} = 1500 \text{ MHz}$$

$$\Delta f = ?$$

Number of longitudinal oscillating modes

$$= \frac{BW}{\Delta f}$$

We know

$$\Delta f = \frac{C}{2L}$$

Number of longitudinal oscillating modes

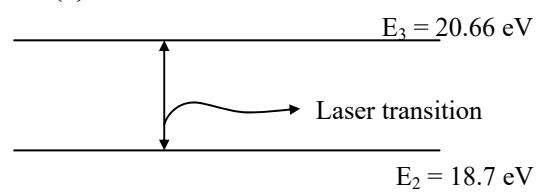
$$= \frac{1500 \text{ MHz}}{\left( \frac{3 \times 10^8}{2 \times 500 \times 10^{-3}} \right)}$$

$$= \frac{1500 \times 10^6}{3 \times 10^8} \times 1000 \times 10^{-3}$$

$$= 5$$

**04. Ans: (c)**

Sol:



Ground

$$E_1 = 0 \text{ eV}$$

**05. Ans: (c)**

Sol:  $E_3 - E_2 = \frac{hc}{\lambda}$

$$\lambda = \frac{hc}{E_3 - E_2} = \frac{6.625 \times 10^{-34} \times 3 \times 10^8}{(20.66 - 18.7) \times 1.6 \times 10^{-19} \text{ J}}$$

$$= 633.8 \text{ nm}$$

**06. Ans: (d)**

Sol: Given

$$\lambda = 6328 \text{ } \text{Å}^0$$

$$\text{Bandwidth} = 1 \text{ MHz}$$

$$C_l = ?$$

We know

$$C = \frac{C_\ell}{C_t}$$

$$C_l = 3 \times 10^8 \times \frac{1}{1 \text{ MHz}} \quad (\because C_t = \frac{1}{f})$$

$$C_l = 300 \text{ m}$$

**07. Ans: 40**

Sol: Area for photodiode D<sub>1</sub>

$$A_1 = 10 \text{ mm} \times (5 \text{ mm} + 0.1 \text{ mm})$$

$$= 51 \times 10^{-6} \text{ m}^2$$

Area for photodiode D<sub>2</sub>

$$A_2 = 10 \text{ mm} \times (5 \text{ mm} - 0.1 \text{ mm})$$

$$= 49 \times 10^{-6} \text{ m}^2$$

$$P_1 = 50 \left( \frac{W}{m^2} \right) \times 51 \times 10^{-6} (\text{m}^2)$$

$$P_1 = 50 \times 51 \times 10^{-6} \text{ (W)}$$

$$P_2 = 50 \left( \frac{W}{m^2} \right) \times 49 \times 10^{-6} \text{ (m}^2\text{)}$$

$$P_2 = 50 \times 49 \times 10^{-6} \text{ (W)}$$

Difference between photo currents

$$\Delta I = I_{D1} - I_{D2}$$

= Photodiode sensitivity  $\times \Delta P$

$$= 0.4 \left( \frac{A}{W} \right) \times (P_1 - P_2)$$

$$= 0.4 \times 50(51 - 49) \times 10^{-6}$$

$$= 0.4 \times 50 \times 2 \times 10^{-6}$$

$$= 40 \text{ } (\mu\text{A})$$

**08. Ans: 2**

$$\text{Sol: } E_g = \frac{hC}{\lambda}$$

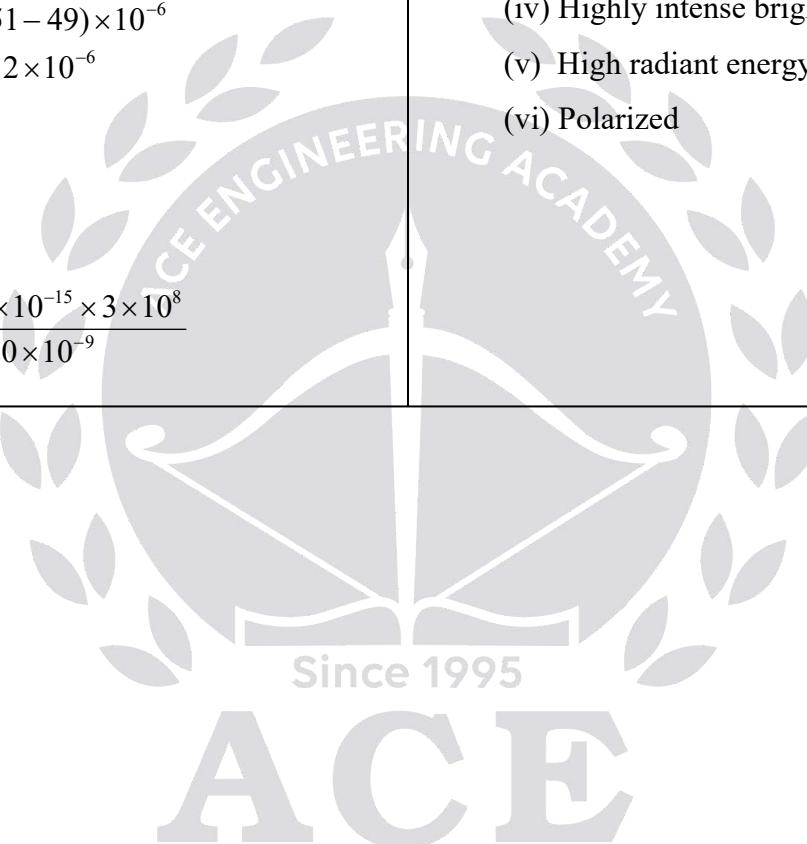
$$E_g = \frac{4.13567 \times 10^{-15} \times 3 \times 10^8}{620 \times 10^{-9}}$$

$$= 2 \text{ eV}$$

**09. Ans: (a, b, c & d)**

**Sol:** The laser light exhibits some peculiar properties compared with the conventional light which make it unique, these are

- (i) Monochromatic
- (ii) Coherence
- (iii) Directionality
- (iv) Highly intense brightness
- (v) High radiant energy
- (vi) Polarized



# Chapter 11 Interferometers

**01.**

**Sol:** Given data:

$$t = 5 \text{ } \mu\text{m}$$

$$n = 5$$

$$\lambda = 589 \text{ nm}$$

$$\mu_g = ?$$

We know

$$t(\mu_g - 1) = n\lambda$$

$$\Rightarrow 5 \times 10^{-6}(\mu_g - 1) = 5 \times 589 \times 10^{-9}$$

$$\Rightarrow (\mu_g - 1) = \frac{5 \times 589 \times 10^{-9}}{5 \times 10^{-6}}$$

$$\Rightarrow (\mu_g - 1) = 0.589$$

$$\Rightarrow \mu_g = 1.589$$

**02.**

**Sol:** Given data:

$$\lambda = 515 \text{ nm}$$

$$\text{Refractive index } (\mu) = 1.6$$

$$\theta_R = 45^\circ$$

$$t = ?$$

we know

$$t(\mu - 1) = n\lambda$$

$$t = \frac{n\lambda}{(\mu - 1)}$$

$$\Rightarrow t = \frac{515 \times 10^{-9}}{1.6 - 1} = 8.58 \times 10^{-7}$$

$$\Rightarrow t = 0.85 \text{ } \mu\text{m}$$

**03.**

**Sol:** Given data

$$t = 1.5 \text{ } \mu\text{m}$$

$$\lambda = 0.5 \text{ } \mu\text{m}$$

$$n = ?$$

We know

$$t = \frac{n\lambda}{2}$$

$$\Rightarrow 1.5 \times 10^{-6} = \frac{n \times 0.5 \times 10^{-6}}{2}$$

$$\Rightarrow \frac{1.5 \times 10^{-6} \times 2}{0.5 \times 10^{-6}} = n$$

$$\Rightarrow n = 6$$

**04.**

**Sol:** Given data:

$$n = 100$$

$$\lambda = 6328 \text{ A}^\circ$$

$$t = 20 \text{ cm}$$

$$\mu = ?$$

We know

$$2t(\mu - 1) = n\lambda$$

$$\Rightarrow 2 \times 20 \times 10^{-2}(\mu - 1) = 100 \times 6328 \times 10^{-10}$$

$$\mu = 1.0001582 \approx 1$$

**05.****Sol:** Given data

$$R.I = \mu_g = 1.53$$

$$\mu_{\text{air}} = 1.0$$

$$R = \left( \frac{\mu_g - \mu_{\text{air}}}{\mu_g + \mu_{\text{air}}} \right)^2$$

$$R = 0.044$$

$$R = 4.4 \% \text{ of loss}$$

**06. Ans: (b & c)****Sol:** A Michelson interferometer consists of

- (i) Movable mirror
- (ii) Fixed mirror
- (iii) Source (monochromatic)
- (iv) Detector
- (v) Half silvered glass plate

**07. Ans: (c & d)****Sol:** The phenomenon of interference is shown both by longitudinal and by transverse waves.

# Chapter 12

# Fiber Optics

**01.** Ans: (d)

$$\begin{aligned} \text{Sol: } NA &= \sqrt{n_1^2 - n_2^2} \\ &= \sqrt{(1.44)^2 - (1.4)^2} \\ &= 0.34 \end{aligned}$$

**02.** Ans: (c)

Sol: Given data

$$\epsilon_r = 2.5$$

$$n = ?$$

n = refractive index

We know,

$$n = \sqrt{\epsilon_r \mu_r}$$

$\epsilon_r$  = relative permittivity

$\mu_r$  = relative permeability

$$n = \sqrt{2.5} \quad (\because \mu_r = 1)$$

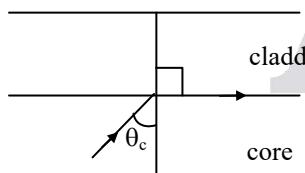
$$= 1.58$$

**03.** Ans: (d)

Sol:  $n_1 = 1.6$

$$n_2 = 1.422$$

$$\theta_c = ?$$



$$\frac{\sin \theta_c}{\sin 90^\circ} = \frac{n_2}{n_1}$$

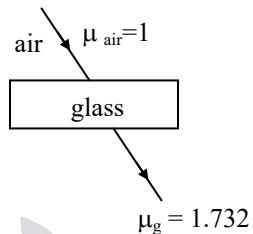
$$\theta_c = \sin^{-1}\left(\frac{1.422}{1.64}\right)$$

$$= 60.12^\circ$$

$$\approx 60^\circ$$

**04.** Ans: (c)

Sol:  $\mu_g = 1.732$



$$\tan \theta_B = \frac{\mu_g}{\mu_{air}} = 1$$

$$\theta_B = \tan^{-1}(1.732)$$

$$= 60^\circ$$

**05.** Ans: (a)

Sol: Given  $\mu_{glass} = 1.720$

$$R = \left( \frac{\mu_{air} - \mu_{glass}}{\mu_{air} + \mu_{glass}} \right)^2 \times 100$$

$$\begin{aligned} R &= \left( \frac{1 - 1.72}{1 + 1.72} \right)^2 \times 100 \\ &= 7 \% \end{aligned}$$

**06.** Ans: (d)

$$\text{Sol: } \theta_c = \sin^{-1}\left(\frac{n_2}{n_1}\right)$$

Given

$$n_1 = 1.641$$

$$n_2 = 1.422$$

$$\theta_c = \sin^{-1}\left(\frac{1.422}{1.641}\right)$$

$$= 60^\circ$$

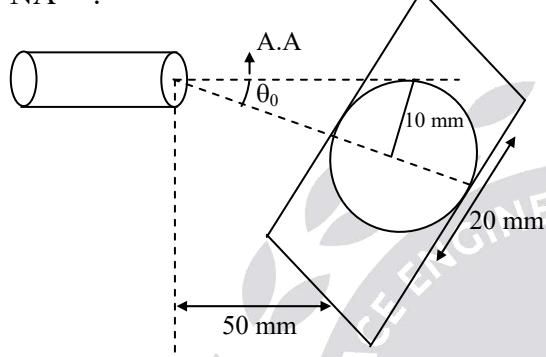
**07. Ans: (d)**

$$\text{Sol: } \frac{\mu_t}{\mu_g} = \frac{1.33}{1.5} = \frac{C}{V_t} \times \frac{V_g}{C}$$

$$\frac{V_t}{V_g} = \frac{1.55}{1.33}$$

**08. Ans: (b)**

**Sol:** NA = ?



$$NA = \sqrt{n_1^2 - n_2^2}$$

$$NA = \mu_0 \sin \theta_0$$

$$NA = \sin \theta_0$$

$$NA = \frac{10}{\sqrt{10^2 + 50^2}} \\ = 0.196$$

$$\approx 0.2$$

**09. Ans: 0.75**

$$\text{Sol: } \frac{n_1}{n_2} = \frac{t_1}{t_2} = 0.75 \quad (n \propto t)$$

**10. Ans: (a, b, c & d)**

**Sol:** Factors affecting the propagation of light through optical sensors:

- (i) The size of fiber
- (ii) The amount of light injected into fiber
- (iii) The coherence of light source
- (iv) The composition of fibers
- (v) The N.A of the source & fiber

**11. Ans: (a, b, & c)**

**Sol:** In case of optical fiber to get TIR the condition is RI of core  $\geq$  RI of cladding.

We know R.I of glass is greater than R.I of plastic so from this information we can say that option (a), (b) & (c) are correct.

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# Chapter 13 UV VIS Spectrophotometer

**01. Ans: 4.35**

**Sol:** In a TOF mass spectrometer

$$t = L \sqrt{\frac{m}{2eV}}$$

$L = 85 \text{ cm}$

$$m_A = 200 \times 1.66 \times 10^{-27}$$

$$m_B = 300 \times 1.66 \times 10^{-27}$$

$$\text{eV} = 1.6 \times 10^{-19} \times 2 \times 10^3$$

$$t_A = L \sqrt{\frac{m_A}{2eV}}$$

$$= 0.85 \sqrt{\frac{200 \times 1.66 \times 10^{-27}}{2 \times 1.6 \times 10^{-19} \times 2 \times 10^3}} = 19.36 \mu\text{sec}$$

$$t_B = L \sqrt{\frac{m_B}{2eV}}$$

$$= 0.85 \sqrt{\frac{300 \times 1.66 \times 10^{-27}}{2 \times 1.6 \times 10^{-19} \times 2 \times 10^3}} = 23.71 \mu\text{sec}$$

$$\Delta t = t_B - t_A = 4.35 \mu\text{sec}$$

**02. Ans: 0.707 m**

**Sol:** In case of mass spectrometer

$$t = L \sqrt{\frac{m}{2eV}}$$

$$\text{for ion A} \rightarrow t_A = L_A \sqrt{\frac{m_A}{2eV}}$$

$$\text{for ion B} \rightarrow t_B = L_B \sqrt{\frac{m_A}{2eV}}$$

$$\frac{t_p}{t_B} = \frac{L_A}{L_B} \sqrt{\frac{m_A}{m_B}}$$

$$\frac{m_A}{m_B} = \frac{1}{2} \text{ (given)}$$

We want to find distance of ion B crossed from starting point when ion A reached at the end of tube i.e.  $t_A = t_B$

$$= \frac{1}{L_B} \sqrt{\frac{1}{2}}$$

$$L_B = \frac{1}{\sqrt{2}} = 0.707 \text{ m}$$

**03. Ans: 524**

**Sol:** Resolving power of mass spectrometer

$$= \frac{\text{mass of sulphur}}{\text{mass of sulphur} - \text{mass of oxygen}}$$

$$= \frac{32.0600}{32.0600 - 31.9988}$$

$$= 523.86$$

$$\cong 524$$

**04. Ans: (a & b)**

**Sol:** A mass spectrum is a graph obtained by performing mass spectrometry.

It is a relation between the mass to charge ratio of ion signal.

A mass spectrum used for working out the relative atomic mass or relative molecular mass of the substance.

**05. Ans: (b, c & d)**

**Sol:** Mass spectroscopy is an analytical technique in which sample is converted into rapidly moving ions which are then separated & characterized. The composition analysis of an alloy, a natural gas, a solid is not done using mass spectrometer.