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ESE-2021 (MAINS)

QUESTIONS WITH DETAILED SOLUTIONS

ELECTRONICS & TELECOMMUNICATION ENGINEERING

PAPER-II

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ELECTRONICS & TELECOMMUNICATION ENGINEERING

ESE_MAINS_2021_PAPER - II

Questions with Detailed Solutions

SUBJECT WISE WEIGHTAGE

S.No	NAME OF THE SUBJECT	Marks
01	COMMUNICATION SYSTEMS	110
02	(a) CONTROL SYSTEMS (b) SIGNALS & SYSTEMS	70 + 30
03	COMPUTER ORGANIZATION AND ARCHITECTURE	90
04	ELECTROMAGNETICS	70
05	ADVANCED ELECTRONICS	60
06	ADVANCED COMMUNICATIONS	50



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(10 M)

SECTION - A

01. (a) Prove that the random process x (t, ϕ) = $\frac{\sqrt{E}}{2T} \cos(\omega_0 t + \phi)$ is ergodic, where E, T and ω_0 are

constants, and ϕ is random and UDF (0, 2π).

Sol:
$$x(t,\phi) = \frac{\sqrt{E}}{2T} \cos(\omega_0 t + \phi)$$

For a random process if ensemble averages are equals to time averages, then it is called as ergodic random process.

Ensemble averages:-

(i) Mean = M₁(t) =
$$\int_{-\infty}^{\infty} x(t,\phi) f_{\phi}(\phi) d\phi$$

$$\int_{-\infty}^{f_{\phi}(\phi)} \frac{1}{2\pi} \frac{1}{2\pi} d\phi$$

$$= \int_{0}^{2\pi} \frac{\sqrt{E}}{2T} \cos(\omega_{0}t + \phi) \frac{1}{2\pi} d\phi$$

$$= \frac{\sqrt{E}}{4\pi T} [\sin(\omega_{0}t + \phi)]_{0}^{2\pi}$$

$$= \frac{\sqrt{E}}{4\pi T} [\sin(\omega_{0}t) - \sin(\omega_{0}t)] = 0$$
M₁(t) = 0
(ii) MSQ [x(t, \phi)] = E[x²(t, \phi)] = \int_{0}^{2\pi} \frac{E}{4T^{2}} \cos^{2}(\omega_{0}t + \phi) \frac{1}{2\pi} d\phi
$$= \frac{E}{8\pi T^{2}} \int_{0}^{2\pi} \left\{ \frac{1 + \cos(2\omega_{0}t + 2\phi)}{2} \right\} d\phi$$

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$$= \frac{E}{16\pi T^2} [2\pi + 0]$$
$$MSQ[x(t,\phi)] = \frac{E}{8T^2}$$

(iii) Variance = MSQ[x(t,
$$\phi$$
)] - M₁(t)²
$$\sigma^{2} = \frac{E}{8T^{2}}$$

<u>Time averages :-</u>

(a) Mean :

$$\langle \mathbf{x}(\mathbf{t}, \boldsymbol{\phi}) \rangle = \frac{1}{\mathbf{t}_2 - \mathbf{t}_1} \int_{\mathbf{t}_1}^{\mathbf{t}_2} \mathbf{x}(\mathbf{t}, \boldsymbol{\phi}) d\mathbf{t}$$
$$= \frac{1}{T} \int_{-T/2}^{T/2} \frac{\sqrt{E}}{2T} \cos(\omega_0 \mathbf{t} + \boldsymbol{\phi}) d\mathbf{t}$$
$$= 0$$

(b) Mean square value

$$< x^{2}(t,\phi) >= \frac{1}{T} \int_{-T/2}^{T/2} \frac{E}{4T^{2}} \cos^{2}(\omega_{0}t + \phi) dt$$
$$= \frac{E}{4T^{3}} \int_{-T/2}^{T/2} \left[\frac{1 + \cos(2\omega_{0}t + 2\phi)}{2} \right] dt$$
$$= \frac{E}{4T^{3}} \left[\frac{T}{2} + 0 \right]$$
$$< x^{2}(t,\phi) >= \frac{E}{8T^{2}}$$

(c) Variance :

$$\begin{split} \sigma^2 &= <\!\!x^2(t,\!\varphi)\!\!> - \left\{<\!\!x(t,\!\varphi)\!\!>\right\}^2 \\ \sigma^2 &= \!\frac{E}{8T^2} \end{split}$$

As we can see ensemble averages are equals to time averages, so $x(t,\phi)$ is ergodic.

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Sol: These are basically 4 steps.

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- (1) By the process of chemical vapour deposition (CVD), a thin layer of $S_{i3}N_4$ is deposited on the entire wafer surface.
- (2) Next the Si_3N_4 is removed by etchant that does not attack SiO_2 .
- (3) Again, through CVD process, on insulating layer, SiO₂, is deposited.
- (4) Al is used for the interconnection.

Figure shown as:-





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01. (c	c) A two-word inst The address field The operand use by 'C'. An index	ruction is stored in n d of the instruction d during the executio register contains the	nemor (store n of t value	ry at an address designate d at A + 1) is designate he instruction is stored at X. State how 'C' is calcu	ed by the symbol A. d by the symbol B. address symbolized lated from the other
	address if the add	lressing mode of the in	nstruc	tion is	(10 M)
	(i) Direct (ii) Indirect (iii) Relative				
	(iv) Indexed				
Sol:	Instruction stored	at A+1 is designated. B	y sym	bol	
	Effective address i	is given by C.			
	Index register cont	tains the value X			
	Direct mode	Effective Address =	= B		
	Indirect mode	Effective Address =	= M[B	3]	
	Relative mode	Effective Address =	= pro	$\underbrace{\operatorname{gram}\operatorname{Counter}}_{A+2} + \underbrace{\operatorname{Relative}\operatorname{Val}}_{B}$	lue
	Indexed mode	Effective Address =	= Inde	$\underbrace{\operatorname{exregvalue}_{X}}_{X} + \underbrace{\operatorname{baseValue}_{B}}_{B}$	
		=	= X +]	В	
01. (d	l) A 75 Ω resistor	is connected to a trai	nsmiss	sion line of characteristic	impedance of 50 Ω .
X	Compute the VSV	WR at the termination	l .		- (10 M)

Compute the VSWR at the termination.

Sol:

$$Z_0 = 50\Omega$$

$$Z_L = 75\Omega$$

$$Z_L = 75\Omega$$

Reflection coefficient,
$$\Gamma_{\rm L} = \frac{Z_{\rm L} - Z_{\rm o}}{Z_{\rm L} + Z_{\rm o}} = \frac{75 - 50}{75 + 50} = \frac{25}{125} = \frac{1}{5}$$

VSWR(
$$\rho$$
) = $\frac{1 + |\Gamma_L|}{1 - |\Gamma_L|} = \frac{1 + \frac{1}{5}}{1 - \frac{1}{5}} = \frac{6}{4} = \frac{3}{2} = 1.5$

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01. (f) The autocorrelation sequence of a discrete-time stochastic process is $R(K) = \left(\frac{1}{2}\right)^{|K|}$. **Determine its Power Spectral Density.** (10 M) $R(k) = \left(\frac{1}{2}\right)^{|K|}$ Sol: $\mathbf{R}(\mathbf{k}) = \left(\frac{1}{2}\right)^{\mathbf{k}} \mathbf{u}[\mathbf{k}] (\mathbf{OR}) \left(\frac{1}{2}\right)^{\mathbf{k}}, \mathbf{K} \ge 0$ $= 2^{K} u[-K-1]$ (OR) 2^{k} , K < 0 1/2 $R(k) \longrightarrow S(\omega) PSK$ For $a^n u(n) \xrightarrow{DTFT} \frac{1}{1 - ae^{-j\omega}}$ $-a^{n}u[-n-1] \xrightarrow{\text{DTFT}} \frac{1}{1-ae^{-j\omega}}$ $\therefore S(\omega) = \frac{1}{1 - \frac{1}{2}e^{-j\omega}} + \frac{-1}{1 - 2e^{-j\omega}}$ $S(\omega) = \frac{2e^{j\omega}}{2e^{j\omega}-1} - \frac{e^{j\omega}}{e^{j\omega}-2}$ $S(\omega) = \frac{2e^{j\omega}(e^{j\omega}-2) - e^{j\omega}(2e^{j\omega}-1)}{(2e^{j\omega}-1)(e^{j\omega}-2)}$ $S(\omega) = \frac{-3e^{j\omega}}{2e^{j2\omega} - 5e^{j\omega} + 2}$ Regular Live Doubt clearing Sessions | Free Online Test Series | ASK an expert

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- 02. (a) Let s(t) be a digital NRZ signal (± A), which passes through the noisy channel. Channel introduces white Gaussian Noise (ω(t)) having PSD of N₀/2. Receiver was designed using Matched Filter, Sample & Hold Circuit and Decision-Making Circuit. Decision-Making Circuit uses maximum likelihood algorithm/technique. Compute the following:
 - (i) Output of the Sample & Hold circuit when '-A' is transmitted (5 M)
 - (ii) Variance of the Noisy Signal at the o/p of S & H Circuit. (5 M)
 - (iii) Compute the probability of error when '- A' is received/detected as '+ A' and '+A' is interpreted as '- A'.
 (10 M)

Sol:



S(t) = +A(OR) - A

n(t) represents AWGN

$$S_{N}(f) = \frac{N_{0}}{2}(W/Hz)$$

Since ML decoding algorithm is used

 $S_1(t) = A$ $S_2(t) = -A$ $P(S_1) = 1/2$ $P(S_2) = 1/2$

 $S_2(t)$ is input of receiver





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Area under both the regions is same

$$\therefore P_{e} = P[n < -A]$$

$$= P[n = -A] \qquad \therefore P_{e} = Q\left[\frac{A}{N_{0}}\right]$$

$$= 1 - Q\left[\frac{-A - 0}{\sigma}\right]$$

$$= 1 - Q\left[\frac{-A}{\sigma}\right] = 1 - \left[1 - Q\left(\frac{A}{\sigma}\right)\right]$$

$$= Q\left[\frac{A}{\sigma}\right]$$

(ii) $S_{N_0}(f) = S_N(f) |H(f)|^2$ [PSD of NOISE at output of matched filter] $S_{N_0}(f) = \frac{N_0}{2} |H(f)|^2$

Variance/power of noise at output of matched filter = $\int S_{N_0}(f) df$

$$= \frac{N_0}{2} \int |H(f)|^2 df$$
$$= \frac{N_0}{2} \int |h(t)|^2 dt$$
$$= \frac{N_0}{2} \int_0^{T_b} (-A)^2 dt$$
$$= \frac{A^2 N_0 T_b}{2} (watts)$$

(iii)
$$V_{th} = \frac{V_1 + V_2}{2} + \frac{\sigma_{n_0}^2 \ell n [P(S_2)/P(S_1)]}{V_1 - V_2}$$

and since $P(S_2) = P(S_1)$

$$V_{th} = \frac{V_1 + V_2}{2} = 0$$
(volts)

$$P_{e} = P(S_{1})P_{e}\left(\frac{S_{2}}{S_{1}}\right) + P(S_{2})P\left(\frac{S_{1}}{S_{2}}\right)$$

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02. (b) The forward path transfer function of a control system with unity feedback is

$$G(s) = \frac{K}{s(s+a)(s+30)}$$

where 'a' and 'K' are real constants.

(i) Find the value of 'a' and 'K' so that the relative damping ratio of the complex roots of the characteristic equation is 0.5 and the rise time of the units step response is approximately 1 sec.
 (15 M)

(ii) Find the steady state errors of the system when the reference input is a unit ramp function. (5 M)

Sol:
$$G(s) = \frac{K}{s(s+a)(s+30)}$$

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(i) $\xi = 0.5, t_r = 1 \sec \theta$

$$t_{r} = \frac{\pi - \tan^{-1} \left(\frac{\sqrt{1 - \xi^{2}}}{\xi} \right)}{\omega_{d}}$$
$$\omega_{d} = \left[\pi - \tan^{-1} \left(\frac{\sqrt{1 - 0.5^{2}}}{0.5} \right) \right] = \frac{2}{3} \pi = 2.094$$
$$2.094 = \omega_{n} \sqrt{1 - \xi^{2}}$$

$$2.094 = \omega_n \sqrt{1 - 0.5^2}$$

 $\Rightarrow \omega_n = 2.41 \text{rad/sec}$

CE for given data,

CE:
$$s(s+a) (s+30)+K = 0$$

CE: $s^3 + s^2(30+a)+30as+K = 0$ (1)
 \Rightarrow second order CE $\Rightarrow (s^2 + 2\xi\omega_n s + \omega_n^2) = 0$
 $\Rightarrow (s^2 + 2.41s + 5.8081) = 0$
Let the 3rd pole at s = - b



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Hence $(s+b)(s^2+2.41s+5.8081) = 0$ $s^{3} + s^{2} (2.41+b) + s(2.41b + 5.8081) + 5.8081 b = 0$ (2) Comparing equation (1) and (2)30 + a = 2.41 + b (1) 30a = 2.41b + 5.8081 (2) K= 5.8081 b____(3) From equation (2) $a = \frac{2.41b}{30} + \frac{5.8081}{30}$ $a = 0.08b + 0.1936 \tag{4}$ (4) in (1)30 + 0.08b + 0.1936 = 2.41 + b \Rightarrow b = 30.1995 From equation (3) K = (5.8081) (30.1995) = 175.4From equation (4) a = 0.08 (30.1995) + 0.1936a = 2.6095 \Rightarrow The third pole at s = -30.1995 and $-\xi\omega_n = -1.205$ The third pole is insignificant pole. Hence the second order approximation is valid. (ii) $G(s) = \frac{K}{s(s+a)(s+30)}$, H(s) = 1 $G(s) = \frac{175.4}{s(s+2.6095)(s+30)} , H(s) = 1$

$$K_{V} = \lim_{s \to 0} s G(s) = \lim_{s \to 0} s \left(\frac{175.4}{s(s+2.6095)(s+30)} \right)$$

$$K_{\rm v} = \frac{175.4}{2.6095 \times 30} = 2.2405$$

$$\Rightarrow e_{ss} = \frac{A}{K_v} = \frac{1}{2.2405} = 0.4463$$

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02. (c) Consider the following set of processes, with the length of the CPU burst given in milliseconds:-Process **Burst Time P**₁ 6 **P**₂ 8 7 P₃ 3 **P**₄ (i) Draw the Gantt chart for SJF scheduling. (5 M) (ii) What is the waiting time for Process P₁, Process P₂ and Process P₃? (5 M) (iii) Calculate the average waiting time. (5 M) (iv) Calculate the average waiting time for FCFS scheduling. (5 M) Sol: Given snapchat <u>AT PID BT CT TAT WT</u> 0 \mathbf{P}_1 6 9 9 3 0 P_2 8 24 24 16 0 P_3 7 16 16 9 0 P_4 3 0 3 3 SJF Gantt chart (i) P_4 P_1 P_3 P_2 24 0 3 9 16 P_1-6 $P_{1}-6$ P₂-8 $P_2 - 8$ $P_2 - 8$ $P_2 - 8$ P₃-7 P₃-7 $P_{3}-7$ P₄–3 (ii) WT of $P_1 = 3$ WT of $P_2 = 16$ WT of $P_3 = 9$ Regular Live Doubt clearing Sessions | Free Online Test Series | ASK an expert E Affordable Fee | Available 1M |3M |6M |12M |18M and 24 Months Subscription Packages

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(iii)	Avg W]	$\Gamma = \frac{3+}{3+}$	16+9-	$+0 = \frac{28}{10}$	$\frac{3}{2} = 7$		
	_		4	4			
(iv)	DID		DT	CT	TAT		
	<u>PID</u>	AT	<u>BL</u>	<u>CT</u>	<u>1A1</u>	<u>wr</u>	
	P ₁	0	6	6	6	0	
	P_2	0	8	14	14	6	
	P ₃	0	7	21	21	14	
	P ₄	0	3	24	24	21	
		P ₁	P_2	P ₃	P ₄		
	0	6	1	4 2	1 24	ł	
	P_1-6	P ₂ -8	8 P3 ⁻ 7 P4-	-7 P4 -3	-3		
	P ₃ -7	P ₄ -3	3	-			
	P ₄ -3						
		(0 + 6 + 1	4+21			
	∴ Avg	WT = -	4	, ,			
		_ 4	$\frac{11}{1} - 10$	25			
			4	20			
02 (a)	L of the	. ha a	tuanan			maganta	d as [V] = (v. v. v.) having Neymbols Lat
05. (a)	thore b	re be a	transn Doivor I	ntter s	Dostinat	presente	a as $[X] = \{X_1, X_2, \dots, X_N\}$ having N symbols. Let bol Voctor $[V] = \{Y_1, Y_2, \dots, Y_{N-1}\}$ boying $[M]$
	symbol	c a Ael	smitte	iavilig I symb	ols have	to nass t	hrough channel $y_1, y_2, y_3 \dots y_M$ having w_1
	(i) Deri	ve the	evnres	sion for	· I(X V)	io pass t	ni ougn channet. (15 M)
	(ii) From	n the d	erived	exnres	sion. con	nnute M	ax [] (X. Y)] expression
	Exp	lain the	e mean	ing of t	erms.		(5 M)

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Sol:	Transmission Receiver					
	$egin{array}{ccc} X_1 & Y_1 \ X_2 & Y_2 \end{array}$					
	X_3 Y_3					
	X_{N} Y_{n}					
(i)	I[X,Y]					
	Let the entropy of input be defined as H(x)				
	$H[X] = [P(x_1)log_2 P(x_1) + P(x_2)lc$	$g_2 P(x_2)$	P_{2})++ P[x_{n}]log ₂ P[x_{N}]]			
	$H[X] = -\sum_{i=1}^{N} P[x_i] \log_2 P[x_i]$					
	Let the entropy of output be defined as H	[[Y]				
	$H[Y] = [P(y_1)log_2 P(y_1) + P(y_2)log_2 P(y_2) + + P[y_m]log_2 P[y_M]]$					
	$H[Y] = -\sum_{J=1}^{M} P[y_{J}] \log_{2} P[y_{J}]$					
	Consider joint entropy between input and output given by H[X,Y]					
	$H[X,Y] = -\sum_{i=1}^{N} \sum_{j=1}^{M} P[x_{i}, y_{j}] \log_{2} P(x_{i}, y_{j})$					
	Consider the below venn-diagram repres	entatio	n			
	H[X] H[Y]					
	$\begin{pmatrix} H[X/Y] \\ I[X,Y] \end{pmatrix} H[Y/X]$					
	H[X,Y]					
	H(X,Y) = H[X] + H[Y/X]					
	(OR)					
	H[X,Y] = H[Y] + H[X/Y]					
	I[X,Y] = H[X] - H[X/Y]					
	(OR)					
	I[X,Y] = H[Y] - H[Y/X]					
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(ii)	MAX [I(X,Y)] = MAX[H(x) - H(x/y] (OF)]	R) MA	X[H(y) - H(y/x)]
	MAX [I(X,Y)] would be MAXIMUM	only	when H[x]
	(OR) H[Y] are MAXIMUM		
	$H[x]_{MAX} = \log_2 N$ and $H[y]_{MAX} = \log_2 M$		
	\therefore MAX[I(X,Y)] = log ₂ N – H[x/y]		

$$(OR)$$
$$= log_2M - H[Y/X]$$

- 03. (b) A feedback control system is shown in the following figure. The specification for the closed loop system requires that the overshoot to a step input be less than 15%.
 - (i) Determine the corresponding specification \mathbf{M}_{p} in the frequency domain for the closed

loop transfer function
$$\frac{Y(j\omega)}{R(j\omega)} = T(j\omega)$$
. (10 M)

(5 M)

(5 M)

(ii) Determine the resonant frequency ω_r.

(iii) Determine the bandwidth of the closed loop system.



Sol: $\%M_p < 15\%$

$$M_{p} = e^{-\pi \xi / \sqrt{1-\xi^{2}}} \times 100\%$$

$$0.15 = e^{-\pi\xi/\sqrt{1-\xi^2}}$$

$$\xi = \sqrt{\frac{(\ell n (0.15))^2}{\pi^2 + (\ell n (0.15))^2}} = 0.5169$$

 $\xi > 0.5169$

ؾؙڹٚٛؖڝ <u>ٞڗ</u> ڐ	ACE Regineering Publications	17	Electronics & Telecommunication Eng.
(i)	M _P equivalent in frequency domain is M _r .		
	$M_{\rm r} = \frac{1}{2\xi\sqrt{1-\xi^2}} = \frac{1}{2\times0.5169\sqrt{1-0.5169^2}}$	-	
	$M_r = 1.1299 \approx 1.13$		
	$M_r < 1.13$		
(ii)	$\omega_{\rm r}, \text{ CLTF } \frac{\text{C(s)}}{\text{R(s)}} = \frac{\text{K}}{\text{s(s+10)} + \text{K}} = \frac{\text{K}}{\text{s}^2 + 10\text{s}^2}$ $\omega_{\rm n} = \sqrt{\text{K}} \text{ r/sec}$ $2\xi\omega_{\rm n} = 10 \Longrightarrow 2 \times 0.5169 \times \omega_{\rm n} = 10$ $\Rightarrow \omega_{\rm n} = 9.67 \text{ rad/sec}$ $\omega_{\rm r} = \omega_{\rm n} \sqrt{1 - 2\xi^2} = 9.67\sqrt{1 - 2 \times 0.5169^2}$ $= 6.599 \approx 6.6 \text{ rad/sec}$	s+K	

(iii) B.W =
$$\omega_n \sqrt{1 - 2\xi^2 + \sqrt{2 - 4\xi^2 + 4\xi^4}}$$
 rad/sec
= 9.67 $\sqrt{1 - 2 \times 0.5169^2 + \sqrt{2 - 4 \times 0.5169^2 + 4 \times 0.5169^4}}$
= 12.11 rad/sec

03. (c) A digital computer has a memory unit with 28 bits per word. The instruction set consists of 235 different operations. All instruction have an operation code part (op code) and an address part. Each instruction is stored in one word memory.

- (i) How many bits are reserved for operation code? (5 M)
- (ii) How many bits are left for the address part of the instruction? (5 M)
- (iii) What is the maximum size for the memory? (5 M)
- (iv) Draw the instruction format and indicate the number of bits in each part. (5 M)

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Sol:	Word length $= 28$ bits.		
	235 different operations '8'-bits ([log ₂ 23	57)	
	(i) 8 bits required for op code.		
	(ii) Address bits = Word length $-$ op code	e	
	= 28 - 8 = 20 bits		
	(iii) Size of Memory = $2^{(\text{no. of bits for address})}$		
	$= 2^{20} = 1$ MB		
	(iv) $28 \text{ bits} \rightarrow 1$ $\leftarrow \text{ opcode} \rightarrow \leftarrow \text{ Address} \rightarrow 1$ 8 -bits 20 -bits		
	20 0.02		
04. (a) Consider the Narrow Band FM wave.		

- (i) Determine the envelope of this modulated wave. What is the ratio of maximum to minimum amplitudes? (5 M)
- (ii) Determine the average power of NBFM. (5 M)

(iii) By expanding the angular argument $\theta(t) = 2\pi f_c t + \phi t$ of NBFM, wave s(t) in the form of a power series and restricting the modulation index β to a maximum value of 0.3 rad,

show that
$$\theta(t) = 2\pi f_c t + \beta \sin(2\pi f_m t) - \frac{\beta^3}{3} \sin^3(2\pi f_m t)$$

Compute the value of Harmonic distortion for $\beta = 0.3$ rad. (10 M)

Sol:

(i)

 $S(t)_{\text{NBFM}} = A_c \cos(2\pi f_c t) \cos(\beta \sin 2\pi f_m t) - A_c \sin(2\pi f_c t) \sin(\beta \sin 2\pi f_m t)$

considering $\theta = \beta \sin(2\pi f_m t)$

and for smaller values of $\boldsymbol{\theta}$

$$\cos(\theta) \simeq 1 \quad \sin(\theta) \simeq \theta$$

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 $\therefore S(t)_{\text{NBFM}} = A_c \cos(2\pi f_c t) - A_c \beta \sin(2\pi f_c t) \sin(2\pi f_m t)$ $S(t)_{\text{NBFM}} = A_c [\cos(2\pi f_c t)] - A_c \beta \sin(2\pi f_m t) [\sin(2\pi f_c t)]$ Envelope of S(t) = $|S(t)|_{NBEM} = \pm \sqrt{A_c^2 + A_c^2 \beta^2 \sin^2(2\pi f_m t)}$ $=\pm A_{a}\sqrt{1+\beta^{2}\sin^{2}(2\pi f_{m}t)}$ $\left| \mathbf{S}(\mathbf{t}) \right|_{\mathrm{MAX}} = \mathbf{A}_{\mathrm{c}} \sqrt{1 + \beta^2}$ $|\mathbf{S}(\mathbf{t})|_{\mathrm{MBL}} = -\mathbf{A}_{\mathrm{c}}\sqrt{1+\beta^2}$ $\therefore \frac{|\mathbf{S}(t)|_{\text{MAX}}}{|\mathbf{S}(t)|_{\text{MAX}}} = \frac{+A_c\sqrt{1+\beta^2}}{-A_c\sqrt{1+\beta^2}} = -1$ (ii) $S(t)_{NBFM} = A_c \cos(2\pi f_c t) - A_c \beta \sin(2\pi f_c t) \sin(2\pi f_m t)$ $=A_{c}\cos(2\pi f_{c}t)-\frac{A_{c}\beta}{2}\cos[2\pi (f_{c}-f_{m})t]+\frac{A_{c}\beta}{2}\cos[2\pi (f_{c}+f_{m})t]$ $P_{avg} = P_t = P_c + P_{USB} + P_{LSB}$ $=\frac{A_c^2}{2}+\frac{A_c^2\beta^2}{2}+\frac{A_c^2\beta^2}{2}$ $=\frac{A_c^2}{2}+\frac{A_c^2\beta^2}{4}$ $P_{avg} = P_t = \frac{A_c^2}{2} \left| 1 + \frac{\beta^2}{2} \right| (watts)$ (iii)The time domain of the FM signal is $S(t) = A_{c} \cos \left[2\pi f_{c} t + 2\pi k_{f} \int m(t) dt \right]$ In the case of single tone modulation $S(t) = A_c \cos \left[2\pi f_c t + \beta \sin 2\pi f_m t \right]$ $= A_c \cos 2\pi f_c t \cos (\beta \sin 2\pi f_m t) - A_c \sin 2\pi f_c t \sin [\beta \sin 2\pi f_m t]$ For NBFM $\beta \ll 1$ Using $\cos\theta \approx 1$ $\sin \theta \approx \theta$ $S(t) = A_c \cos 2\pi f_c t - A_c \beta \sin 2\pi f_m t \sin 2\pi f_c t$ Using the relationship A cos $2\pi f_t t + B \sin 2\pi f_t t = \sqrt{A^2 + B^2} \cos \left[2\pi f_t t + \phi\right]$ $A=A_{c} \qquad B=-A_{c}\beta\sin 2\pi f_{m}t$ $S(t) = \sqrt{A^2 + A^2 \beta^2 \sin 2\pi f_{\rm u} t} \cos \left[2\pi f_{\rm u} t + \phi\right]$

$$\phi = \tan^{-1} \left[\frac{B}{A} \right] = \tan^{-1} \left[\beta \sin 2\pi f_{m} t \right]$$

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$$\begin{split} &S(t) = \sqrt{A_c^2 + A_c^2 \beta^2 \sin^2 2\pi f_m t} \cos \left[2\pi f_c t + \tan^{-1} (\beta \sin 2\pi f_m t) \right] \\ &Angular argument = 2\pi f_c t + \tan^{-1} [\beta \sin 2\pi f_m t] \\ &Power series of \\ &tan^{-1}(x) = x - \frac{x^3}{3} + \dots \\ &x = \beta \sin 2\pi f_m t \\ &Angular argument = 2\pi f_c t + \beta \sin 2\pi f_m t - \frac{\beta^3}{3} \sin^3 2\pi f_m t \\ &By replacing \sin^3 (2\pi f_m t) with the help of \\ &sin(3A) = 3\sin A - 4\sin^3(A) \\ &We can rewrite \theta(t) as \\ &\theta(t) = 2\pi f_c t + \sin(2\pi f_m t) \left[\beta - \frac{3\beta^3}{12} \right] + \frac{\beta^3}{12} \sin(6\pi f_m t) \\ &\theta(t) = 2\pi f_c t + \left[\frac{4\beta - \beta^3}{4} \right] \sin(2\pi f_m t) + \frac{\beta^3}{12} \sin[2\pi (3f_m)t] \end{split}$$

Harmonic Distortion is the ratio of the sum of the powers of all harmonic components to the power of fundamental frequency.

$$(OR) \quad \frac{\sqrt{V_3^2}}{V_1}$$

 V_3 is RMS Value of third harmonic

V₁ is RMS value of 1st harmonic

Harmonic Distortion (H.D) = $\sqrt{\left(\frac{\beta^3}{12\sqrt{2}}\right)^2} / \frac{4\beta - \beta^3}{4\sqrt{2}}$

$$\Rightarrow \text{ at } \beta = 0.3$$

$$\frac{(0.3)^3}{12\sqrt{2}} \times \frac{4\sqrt{2}}{(1.2 - (0.3)^3)}$$

$$\Rightarrow \frac{(0.3)^3}{3(1.173)} = 0.00765 \text{ (OR)} 0.765\%$$

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Intersection point with imaginary axis:-

CE:
$$s^{3} + 4s^{2} + 7s + a' = 0$$

 $s^{3} \begin{vmatrix} 1 & 7 \\ s^{2} \end{vmatrix} 4 \quad a^{1}$
 $s^{1} \begin{vmatrix} \frac{28 - a'}{4} \\ 0 \end{vmatrix} > 0(s) \Rightarrow (28 - a') > 0 \Rightarrow a' < 28$
 $s^{0} \begin{vmatrix} a^{1} > 0 \\ a^{1} > 0 \\ 0 \end{vmatrix} = 0$
 $0 < a' < 28$
 $0 < 4a < 28$
 $0 < a < 7$ Stable

Marginal stable:

$$(28-a') = 0 \Longrightarrow a' = 28$$

$$4a = 28$$

a = 7 marginal stable

$$IP \Longrightarrow 4s^2 + a' = 0$$

$$4s^2 + 28 = 0 \Longrightarrow s = \pm j\sqrt{7}$$

When $a = 100 \implies s = -8.567, 2.298 \pm j6.42$



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(ii) a = 2				
CE: $s^3 + 4s^2 + 7s + 4 \times 2 = 0$				
$s^3 + 4s^2 + 7s + 8 = 0$				
Roots \Rightarrow s = -2.477, -0.761 \pm j1.627				
Root Locus Diagram: a = 2 $a = 2$ -2.477 -0.761 x	+ j 	$1.627 = \sqrt{0.761^2 + 1.627^2} = 1.796 \text{r/sec}$		
a = 2 $\Rightarrow \xi = \cos \theta = \frac{0.76}{1.796} = 0.4237$ % M _p = e ^{-\pi \xi / \sqrt{1 - \xi^2}} -\pi \times 0.423 / \sqrt{1 - 0.423^2} = 1000 (-220)				
$t_{s}(\pm 2\%) = \frac{4}{\xi\omega_{n}} = \frac{4}{0.761} = 5.25 \text{ sec}$				
$\Rightarrow a = 4$				
CE $s^3 + 4s^2 + 7s + 4 \times 4 = 0$ CE $s^3 + 4s^2 + 7s + 16 = 0$				
Roots s = -3.3387 , $0.3306 \pm j2.164$	I			
Root Locus Diagram: a=4 -3.3387 a=4 -j 2.164 a=4 -j 2.164 a=4 -j 2.164				
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a = 4	t clearin	- j 2.164 ng Sessions Free Online Test Series ASK an expert 1 3M 6M 12M 18M and 24 Months Subscription Packages		

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$$\Rightarrow \xi = \cos \theta = \frac{0.3306}{2.189} = 0.151$$

$$\% m_{p} = e^{-\pi\xi/\sqrt{1-\xi^{2}}} \times 100\%$$

$$= e^{-\pi\times0.151/\sqrt{1-0.151^{2}}} \times 100\% = 61.88\%$$

$$\Rightarrow t_{s}(\pm 2\%) = \frac{4}{\xi\omega_{n}} = \frac{4}{0.3306} = 12 \sec$$

(iii) $a = 2$, Actual over shoot $\Rightarrow M_{p} = e^{\frac{-\pi\xi}{\sqrt{1-\xi^{2}}}}$

$$\Rightarrow M_{P} = 0.23$$

$$\Rightarrow t_{s}(\pm 2\%) = \frac{4}{\xi\omega_{n}} = \frac{4}{0.761} = 5.25 \sec$$

 $a = 4$, Actual over shoot $\Rightarrow M_{p} = e^{\frac{-\pi\xi}{\sqrt{1-\xi^{2}}}}$

$$\Rightarrow M_{P} = 0.6188$$

$$\Rightarrow t_{s}(\pm 2\%) = \frac{4}{\xi\omega_{n}} = \frac{4}{\xi\omega_{n}} = 12 \sec$$

$$\Rightarrow t_{s}(\pm 2\%) = \frac{4}{\xi \omega_{n}} = \frac{4}{0.3306} = 12 \text{ se}$$

04. (c) (i) Explain programming paradigms with examples.(10 M)(ii) Write a pseudocode/program to sort given number.(10 M)

Sol:

(i) Paradigm can also be termed as method to solve some problem or do some task. Programming paradigm is an approach to solve problem using some programming language or also we can say it is a method to solve a problem using tools and techniques that are available to us following some approach. There are lots for programming language that are known but all of them need to follow some strategy when they are implemented and this methodology/strategy is paradigms. Apart from varieties of programming language there are lots of paradigms to fulfill each and every demand. They are discussed below:

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1. Imperative programming paradigm:

It is one of the oldest programming paradigm. It features close relation to machine architecture. It is based on Von Neumann architecture. It works by changing the program state through assignment statements. It performs step by step task by changing state. The main focus is on how to achieve the goal. The paradigm consists of several statements and after execution of all the result is stored.

Ex: C, FORTAN, BASIC.

Imperative programming is divided into three broad categories: Procedural, OOP and parallel processing. These paradigms are as follows:

Procedural programming paradigm-

This paradigm emphasizes on procedure in terms of under lying machine model. There is no difference in between procedural and imperative approach. It has the ability to reuse the code and it was boon at that time when it was in use because of its reusability.

Ex: C, C++, JAVA, ColdFusion, Pascal.

Object Oriented Programming

The program is written as a collection of classes and object which are meant for communication. The smallest and basic entity is object and all kind of computation is performed on the objects only. More emphasis is on data rather procedure. It can handle almost all kind of real life problems which are today in scenario.

Ex: Simula, Java, C++, Objective-C, Visual Basic .NET, Python, Ruby, Smalltalk



• Parallel processing approach

Parallel processing is the processing of program instructions by dividing them among multiple processors. A parallel processing system posses many numbers of processor with the objective of running a program in less time by dividing them. This approach seems to be like divide and conquer. Examples are NESL (one of the oldest one) and C/C++ also supports because of some library function.

2. Declarative programming paradigm:

It is divided as Logic, Functional, Database. In computer science the declarative programming is a style of building programs that expresses logic of computation without talking about its control flow. It often considers programs as theories of some logic. It may simplify writing parallel programs. The focus is on what needs to be done rather how it should be done basically emphasize on what code code is actually doing. It just declares the result we want rather how it has be produced. This is the only difference between imperative (how to do) and declarative (what to do) programming paradigms. Getting into deeper we would see logic, functional and database.

Logic programming paradigms

It can be termed as abstract model of computation. It would solve logical problems like puzzles, series etc. In logic programming we have a knowledge base which we know before and along with the question and knowledge base which is given to machine, it produces result. In normal programming languages, such concept of knowledge base is not available but while using the concept of artificial intelligence, machine learning we have some models like Perception model which is using the same mechanism.

In logical programming the main emphasize is on knowledge base and the problem. The execution of the program is very much like proof of mathematical statement, e.g., Prolog

• Functional programming paradigms

The functional programming paradigms has its roots in mathematics and it is language independent. The key principal of this paradigms is the execution of series of mathematical functions. The central model for the abstraction is the function which are meant for some

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specific computation and not the data structure. Data are loosely coupled to functions. The function hide their implementation. Function can be replaced with their values without changing the meaning of the program.

Ex: JavaScript, Perl, Haskwell, Scala, Erlang, Lisp, ML, Clojure

Database/Data driven programming approach-

This programming methodology is based on data and its movement. Program statements are defined by data rather than hard-coding a series of steps. A database program is the heart of a business information system and provides file creation, data entry, update, query and reporting functions. There are several programming languages that are developed mostly for database application. For example **SQL**. It is applied to streams of structured data, for filtering, transforming, aggregating (such as computing statistics), or calling other programs. So it has its own wide application.

(ii) # include <stdio.h>

void sort_numbers_ascending(int number[], int count)

```
{
```

```
int temp, i, j, k;
for (j = 0; j < count; ++j)
{
  for (k = j + 1; k < count; ++k)
  {
    if (number[j] > number[k])
    {
        temp = number[j];
        number[j] = number[k];
        number[k] = temp;
    }
}
```

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```
printf("Numbers in ascending order:\n");
for (i = 0; i < count; ++i)
printf("%d\n", number[i]);
}
void main()
{</pre>
```

int i, count, number[20];

printf("How many numbers you are gonna enter:");

scanf("%d", &count);

printf("\nEnter the numbers one by one:");

for (i = 0; i < count; ++i)

scanf("%d", &number[i]);

sort_numbers_ascending(number, count);

}

Output:

How many numbers you are gonna enter:5

Enter the numbers one by one:

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(5 M)

SECTION - B

29

05. (a) (i) Let X be a random variable and let $Y = (X - \mu_X)/\sigma_X$. What is the mean and variance of the random variable Y? (5 M)

(ii) Compute the mean of e^{jωt} where ω is a random variable.

Sol:

(i) Let MEAN of RVX = μ_x $Y = \frac{X - \mu_x}{\sigma_x}$ $E[Y] = E\left[\frac{X - \mu_x}{\sigma_x}\right] = \frac{1}{\sigma_x}[E[X] - \mu_x]$ $\therefore E[Y] = \frac{1}{\sigma_x}[\mu_x - \mu_x] = ZERO$ $\sigma_Y^2 = E[Y^2] - E[Y]^2$ $\sigma_Y^2 = E[Y^2] = E\left[\frac{(x - \mu_x)^2}{\sigma_x^2}\right] = \frac{E(x - \mu_x)^2}{\sigma_x^2}$

$$\therefore \ \sigma_{\rm Y}^2 = \frac{1}{\sigma_{\rm X}^2} X \sigma_{\rm X}^2 = 1$$

(ii) Given $e^{j\omega t}$ in which random variable is ω

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$$e^{j\omega t} = 1 + j\omega t + \frac{(j\omega t)^2}{2!} + \frac{(j\omega t)^2}{2!} + \dots + \frac{(j\omega t)^n}{n!}$$

$$e^{j\omega t} = 1 + jt\omega - \frac{\omega^2 t^2}{2} - \frac{j\omega^3 t^3}{6} + \dots + \frac{(j\omega t)^n}{n!}$$

$$E[e^{j\omega t}] = E\left[1 + jt\omega - \frac{\omega^2 t^2}{2} - \frac{j\omega^3 t^3}{6} + \dots + \frac{(j\omega t)^n}{n!}\right]$$

$$\therefore E[e^{j\omega t}] = 1 + jtE[\omega] - \frac{t^2}{2}E[\omega^2] - j\frac{t^3}{6}E[\omega^3] - \dots$$

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- 05. (b) Describe the importance of photolithography in the fabrication of the integrated Circuits. How is the junction depth determined after the diffusion of n-type dopants in a p-type substrate with a background concentration of 10¹⁵/cm³? (10 M)
- Sol: Importance of photolithography

1) Lithography transforms complex circuit diagram into pattern which are define on the wafer in a succession of exposure of processing steps.

- 2) It is a process used in micro-fabrication to transfer geometric patterns to a films or substrate.
- 3) High exposure sensitivity : 2 or more orders of magnitude higher than that of electron beam lithography.
- 4) It can be used as physical sputtering etch and chemical assisted etch.

Junction depth

$$C(x, t) = Cs \text{ erf } \left\{ \frac{xg}{2\sqrt{Dt}} \right\}$$

05. (c) Explain the following terms with example:

(10 M)

(i) Attribute

(ii) Domain

(iii) Entity

(iv) Relationship

Sol: The ER model defines the conceptual view of a database. It works around real-world entities and the associations among them. At view level, the ER model is considered a good option for designing databases.

(i) Attributes

Entities are represented by means of their properties, called **attributes**. All attributes have values. For example, a student entity may have name, class, and age as attributes.

There exists a domain or range of values that can be assigned to attributes. For example, a student's name cannot be a numeric value. It has to be alphabetic. A student's age cannot be negative, etc.

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Types of Attributes

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- **Simple attribute** Simple attributes are atomic values, which cannot be divided further. For example, a student's phone number is an atomic value of 10 digits.
- **Composite attribute** Composite attributes are made of more than one simple attribute. For example, a student's complete name may have first_name and last_name.
- Derived attribute Derived attributes are the attributes that do not exist in the physical database, but their values are derived from other attributes present in the database.
 For example, average_salary in a department should not be saved directly in the database, instead it can be derived. For another example, age can be derived from data_of_birth.
- **Single-value attribute** Single-value attributes contain single value. For example- Social Security Number.
- **Multi-value attribute** Multi-value attributes may contain more than one values. For example, a person can have more than one phone number, email_address, etc.

These attribute types can come together in a way like -

- simple single-valued attributes
- simple multi-valued attributes
- composite single-valued attributes
- composite multi-valued attributes

(ii) Domain

Each column of a relational table is defined on a domain. A domain is a set of values. A datatype, which is also defined for each column, consists of a domain of values and a set of operations on those values. The sets S_1 , S_2 , and S_3 are sets of values. In the context of a database, they are domains of columns.

When assigned to a column of a table, a domain defines the set of the only values, and only the values, which are valid in row-level instances of that column. For example, the domain of a customer status column is the set of all valid customer status codes.

Sometimes domains include all the values permitted by the datatype of the column they are assigned to. At other times, domains contain only some of those values.

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There are three domains, D_1 , D_2 and D_3 . The first two domains are not ordered, shown by using braces; the third one is ordered, shown by using brackets. These domains are the sets S_1 , S_2 , and S_3 , but understood as functioning as domains for the columns of database tables. Later on, we will assign them to $T_X.C_1$, $T_X.C_2$, and $T_X.C_3$, the columns of table T_X .

 $D_1 = \{C_1, C_2, C_3\}$

 $\mathbf{D}_2 = \{\mathbf{A}, \mathbf{B}, \mathbf{C}\}$

 $D_3 = \{Platinum, Gold, Silver\}$

(iii) Entity

An entity can be a real-world object, either animate or inanimate, that can be easily identifiable. For example, in a school database, students, teachers, classes, and courses offered can be considered as entities. All these entities have some attributes or properties that give them their identity.

An entity set is a collection of similar types of entities. An entity set may contain entities with attribute sharing similar values. For example, a Students set may contain all the students of a school; likewise a Teachers set may contain all the teachers of a school from all faculties. Entity sets need not be disjoint.

(iv) Relationship

The association among entities is called a relationship. For example, an employee **works_at** a department, a student **enrolls** in a course. Here, Works_at and Enrolls are called relationships.

Relationship Set

A set of relationships of similar type is called a relationship set. Like entities, a relationship too can have attributes. These attributes are called **descriptive attributes**.

Degree of Relationship

The number of participating entities in a relationship defines the degree of the relationship.

- Binary = degree 2
- Ternary = degree 3
- n-ary = degree-n

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Mapping Cardinalities

Cardinality defines the number of entities in one entity set, which can be associated with the number of entities of other set via relationship set.

• **One-to-one** - One entity from entity set A can be associated with at most one entity of entity set B and vice versa.



• **One-to-many** - One entity from entity set A can be associated with more than one entities of entity set B however an entity from entity set B, can be associated with at most one entity.



• Many-to-one – More than one entities from entity set A can be associated with at most one entity of entity set B, however an entity from entity set B can be associated with more than one entity from entity set A.



• Many-to-many – One entity from A can be associated with more than one entity from B and vice versa.



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05. (d) A reflector antenna used for a cellular base station backhaul ratio link operates at 38 GHz
with a gain of 39 dB, a radiation efficiency of 90%, and a diameter of 30 cm. Find the
aperture efficiency of this antenna. (10 M)
Sol:
$$f = 38 \text{ GHz}, \ \lambda = \frac{3 \times 10^8}{38 \times 10^9} = \frac{3}{380} \text{ MHz}$$

Gain = 39 dB = 10^{3.9}
Radiation Efficiency = 90%
Diameter = 30 cms
Aperture Efficiency of Antenna = ?
 $\eta_{up} = \frac{A_e}{\Lambda_p}$
 $A_e = \text{Effective Aperture}$
 $A_p = \text{Physical Aperture}$
 $G = \frac{4\pi A_e \times (380)^2 \eta}{9}$
 $10^{3.9} = \frac{4\pi A_e \times (380)^2 \eta}{9}$
 $\therefore A_e = \frac{0.03939}{0.9} = 0.04376$
 $A_p = \pi r^2 = \frac{\pi D^2}{4} = \frac{\pi \times (0.3)^2}{4} = 0.070685$
 $\eta_{up} = \frac{A_e}{\Lambda_p} = \frac{0.04376}{0.070685} = 61.9\%$

05. (e) Design a pipelined architecture to compute the value of the following summation by using 8-bit adders and 8-bit registers:

Sum = A + B + C + D + E + F + G + H

Assume that all the inputs are of 8-bits and the output 'Sum' is also restricted to 8-bits. Moreover, all the inputs and outputs are registered. Also compute its latency. (10 M)

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- **Sol:** \rightarrow Given expression is A + B + C + D + E + F + G + H
 - \rightarrow It is performed in Arithmetical pipelined CPU
 - \rightarrow Arithmetical pipelined CPU is designed with multiple ALU's.
 - \rightarrow Since number of input operands is 8; them number of ALUs is 4 with size of 8 bit each
 - \rightarrow Inputs are applied through 8 bit Regs and output is also stored in 8 bit Reg



Let CPU clock is f_{clk} , then segment delay time $(T_{seg}) = \frac{1}{f_{clk}} = T'$ state

R to R_8 Registers are considered as stage S_1 , four 8 bit ALUs are considered as stage S_2 . Both ALUs output is fed to 2. Register for storing partial Result stage 3.

- \rightarrow Note: One more ALU is not required
- \rightarrow The output registers (x and y) result are fed to one of the ALU's in stage 2 (S₂)
- \rightarrow Final result is placed in stage S₃

Latency computation

Let T segment = $T_{Reg} = T_{ALU} = 1$ clk

- \rightarrow 3 clocks are sufficient to get partial result in x and y stages.
- \rightarrow After 3 clocks 'x' holds A + B + C + D and y holds E + F + G + H.

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- \rightarrow Three more clocks are required to feed the partial results of (A + B +C + D) and (E + F + G + H) to input registers, ALU operation and for storing the final result.
- \rightarrow Hence total number of clocks required is six.
- → Let the CPU is designed with 5th ALU then, after 3 clocks x and y gets the partial Result of (A + B + C + D) and (E + F + G + H).
- \rightarrow Fourth clock is required to operate <u>ALU5</u> and after completion of 5th clock the final result is saved in output register.

Note: Let CPU has 4 ALUs it requires 6 clocks and only 5 clocks are sufficient when cpu is designed with 5th ALU.

05. (f) Write down the procedure to compute orthogonal basis function for two given signals (x₁(t) and x₂(t)). (10 M)

Sol: Consider the problem of approximating a real signal $x_1(t)$ in terms of another real signal $x_2(t)$ over the interval (t_1, t_2)

$$x_1(t) \,\simeq\, C x_2(t) \ ; \ h \leq t \leq t_2$$

Error in this approximation is

$$e(t) = x_1(t) - Cx_2(t)$$
; $t_1 \le t \le t_2$
We need to minimise the error signal that is minimize its size, which is energy E_e over (t_1, t_2)

$$E_{e} = \int_{t_{1}}^{t_{2}} e^{2}(t) dt = \int_{t_{1}}^{t_{2}} [x_{1}(t) - Cx_{2}(t)]^{2} dt$$

Here E_e is a function of parameter "C".

To minimize E_e , necessary condition is $\frac{dE_e}{dC} = 0$.

$$\frac{d}{dC} \left[\int_{t_1}^{t_2} x_1^2(t) dt \right] - \frac{d}{dC} \left[2C \int_{t_1}^{t_2} x_1(t) x_2(t) dt \right] + \frac{d}{dC} \left[C^2 \int_{t_1}^{t_2} x_2^2(t) dt \right] = 0$$

$$\Rightarrow -2 \int_{t_1}^{t_2} x_1(t) x_2(t) dt + 2C \int_{t_1}^{t_2} x_2^2(t) dt = 0$$

$$\int_{t_1}^{t_2} x_1(t) x_2(t) dt + 2C \int_{t_1}^{t_2} x_2^2(t) dt = 0$$

$$C = \frac{\int_{t_1}^{t_1} x_1(t) x_2(t) dt}{\int_{t_1}^{t_2} x_2^2(t) dt}$$

If the component of $x_1(t)$ of the form $x_2(t)$ is zero (i.e., C = 0) the signals $x_1(t)$ & $x_2(t)$ are orthogonal over (t_1, t_2)

:. The signals $x_1(t) \& x_2(t)$ are orthogonal over the interval (t_1, t_2) if $\int_{-\infty}^{t_2} x_1(t) x_2(t) dt = 0$

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So, $\alpha = 101.09 \times 8.686 \text{dB/m}$ $\alpha = 964.9277 \text{dB/m}$ so $964.9277 \text{dB} \rightarrow 1\text{m}$ $100 \text{dB} \rightarrow \ell = ?$ $\ell = \frac{100}{964.9277} = 0.10363 \text{m} = 10.36 \text{cm}$

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06. (b) Realize a full adder Sum = A ⊕ B ⊕ C in output by using only minimum number of multiplexer based logic blocks as shown below. The 'Sum' output is obtained by appropriately setting all the inputs of these logic blocks.

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(20 M)

Sol: $S = A \oplus B \oplus C = m_1 + m_2 + m_4 + m_7$

$$S = \overline{ABC} + \overline{ABC} + A\overline{BC} + ABC$$
$$S = \overline{A} \left[\overline{B.C} + \overline{B.C} \right] + A \left[\overline{B.C} + \overline{B.C} \right]$$

Choose

 $A_3 = A_6 = B$; $A_1 = \overline{C}$, $A_2 = C$; $A_7 = A$ $A_4 = C$, $A_5 = \overline{C}$; $A_8 = 0$ ACE 39 $\overline{\mathbf{C}}$ F_1 ▶F С F_2 $\overline{A_7 + A_8} = \overline{A + 0}$ $\overline{\mathbf{C}}$ $F = \overline{(\overline{A})}I_0 + \overline{A}.I_1$ $= A.F_1 + \overline{A} \cdot F_2$ where: $F_1 = \overline{B}.\overline{C} + B.C$ $F_2 = \overline{B.C} + B.\overline{C}$ $F = A \left[\overline{B.C} + B.C \right] + \overline{A} \left[\overline{B.C} + B.\overline{C} \right]$

$$= \overline{ABC} + \overline{ABC} + \overline{ABC} + \overline{ABC}$$

 $F = A \oplus B \oplus C$

06. (c) Two multimode step index fibers have Numerical Aperture of 0.2 and 0.4 respectively. Both fibers have 1.48 as their refractive index of core. Calculate the insertion loss at a joint in each fiber caused due to 5° angular misalignment of axes of fiber core. Medium between fibers is air. (20 M)

The angular coupling efficiency is given Sol:

$$\eta_{ang} = \frac{16(n_1 / n)^2}{\left[1 + (n_1 / n)^4\right]} \left[1 - \frac{n\theta}{\pi n_1 (2\Delta)^{\frac{1}{2}}}\right]$$

The numerical aperture is related to the relative refractive index difference following as

 $NA \cong n_1(2\Delta)^{1/2}$

Hence:

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$$\eta_{\text{ang}} \approx \frac{16(n_1/n)^2}{\left[1 + (n_1/n)^4\right]} \left[1 - \frac{n\theta}{\pi NA}\right]$$

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For the NA = 0.2 fiber:

$$\eta_{\text{ang}} \cong \frac{16(1.48)^2}{[1+1.48]^4} \left[1 - \frac{5\pi/180}{\pi 0.2} \right]$$
$$= 0.797$$

The insertion loss due to the angular misalignment may be obtained as

 $Loss_{ang} = -10 \, \log_{10} \eta_{ang} = -10 \, \log_{10} 0.797$

For the NA = 0.4 fiber:

$$\eta_{ang} \approx 0.926 \left[1 - \frac{5\pi/180}{\pi 0.4} \right]$$

= 0.862

The insertion loss due to the angular misalignment is therefore:

 $Loss_{ang} = -10 \log_{10} 0.862$

07. (a) The radial components of the radiated power density of an antenna is given by

$$W_{rad} = \hat{a}_r W_r = \hat{a}_r A_0 \frac{\sin \theta}{r^2} W / m^2$$

where 'A₀' is the peak value of the power density, ' θ ' is the usual spherical coordinate, and ' \hat{a}_r ' is the radial unit vector. Find the maximum directivity of the antenna. Write an expression for the directivity as a function of directional angles ' θ ' and ' ϕ '. (10 + 10 M) Given:

The radiated power density of an antenna is

$$\vec{W}_{rad} = W_r \hat{a}_r = A_0 \frac{\sin \theta}{r^2} \hat{a}_r W / m^2$$

Sol:

The radiation intensity is given by

$$U(\theta, \phi) \text{ or } U(\theta) = r^2 W_{rad} = r^2 A_0 \frac{\sin \theta}{r^2}$$

 $U(\theta, \phi)$ or $U(\theta) = A_o \sin \theta$



Average power radiated from the antenna is

$$P_{rad} = \iint_{\theta \phi} U(\theta, \phi) \sin \theta d\theta d\phi$$
$$= \iint_{\theta=0}^{\pi} \iint_{\phi}^{2\pi} A_{o} \sin \theta \sin \theta d\theta d\phi$$
$$= A_{o} \left[\iint_{\theta=0}^{\pi} \sin^{2} \theta d\theta \right] \left[\iint_{\phi=0}^{2\pi} d\phi \right]$$
$$= A_{0} \left[\iint_{\theta=0}^{\pi} \frac{1 - \cos 2\theta}{2} d\theta \right] (2\pi)$$
$$= A_{o} \times \frac{\pi}{2} \times 2\pi$$

 $P_{rad} = \pi^2 A_o Watt$

As radiation intensity is only a function of ' θ ' and hence the directivity as a function of directional angle is represented by

$$D = 4\pi \frac{U(\theta)}{P_{rad}}$$
$$= 4\pi \times \frac{A_o \sin \theta}{\pi^2 A_o}$$
$$D = \left(\frac{4}{\pi}\right) \sin \theta$$
$$\therefore D(\theta) = 1.2732 \sin \theta$$

The maximum radiation is directed along $\theta = \frac{\pi}{2}$, thus $U_{max} = A_o$

Maximum directivity af antenna is given by,

$$D = 4\pi \frac{U_{max}}{P_{rad}} = 4\pi \times \frac{A_o}{\pi^2 A_o} = \frac{4}{\pi}$$
$$\therefore D = 1.2732$$





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07. (b) Write an 8085 program to generate the following waveform with the help of 8085 microprocessor kit and an 8-bit DAC connected to an output port 'A' of 8255. The output voltage range of DAC is 0 V to 10 V. The address of port 'A' and Control register of 8255 are 00H and 03H respectively.



(20 M)

- Sol: \rightarrow Given that 8-bit DAC is connected to port A of 8255 that is interfaced to 8085.
 - \rightarrow DAC's output voltage range is 0V to 10V
 - \rightarrow PA address of 8255 is 00H

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- \rightarrow CWR address of 8255 is 03H
- \rightarrow The waveform to be generated is as given below



 \rightarrow IO mode 0 operation is to be used for 8255.

Control word for choosing IO mode 0 i.e., simple I/O is 1 0 0 0 0 0 0 i.e., 80H

→ By loading 80H into CWR register, PA will be programmed as output port in simple I/O mode

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 \rightarrow

Digital input to DAC	Analog output of DAC
00H	0V
80H	5V
FFH	10V

\rightarrow Program:

	MVI A, 80H ;		80H is control word
	OUT 03H ;		PA configured as output port in mode 0
NEXT:	XRA A ;		(A) = 00H (Digital equivalent of 0V)
	OUT 00H ;		DAC output will be 0V
	CALL ZERO;		0V level maintained for some time
	MVI A, 80H ;		(A) = 80H (Digital equivalent of 5V)
	OUT 00H ;		DAC output will be 5V level
	CALL FIVE ;		5V level maintained for some time
RISE:	INR A		
	OUT 00H ;		Sawtooth starts
	CPI FFH		
	JNZ RISE ;		Sawtooth continued till 10V reaches
	MVI A, 80H ;		(A) = 80H (Digital equivalent of 5V)
	OUT 00H ;		DAC output will be 5V
	CALL FIVE ;		5V level maintained for some time
	JMP NEXT;		For next cycle, same operation will be repeated
ZERO:	MVI C, FFH ;		ZERO subroutine
AGAIN:	DCR C		
	JNZ AGAIN		
	RET		
FIVE:	MVI C, 88H ;		FIVE subroutine
REPEAT:	DCR C		
	JNZ REPEAT		
	RET		
	HLT		
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07. (c) Consider the GPS receiver system given below. The guaranteed minimum L1(1575 MHz) carrier power received by an antenna on Earth having a gain of 0 dBi is S_i = - 160 dBW. A GPS receiver is usually specified as requiring a minimum carrier to noise ratio, relative to a 1 Hz BW, of C/N (Hz). If the receiver antenna actually has a gain G_A, and a noise temperature T_A, derive an expression for the maximum allowable amplifier noise figure, F, assuming an amplifier gain, G, and a connecting line loss, L. Evaluate this expression for C/N= 32 dB-Hz, G_A = 5 dB, T_A = 300 K, G = 10dB and L = 25 dB.



(20)	M
(–)	





 $S_i/dB = -160 \ dBW = 10 \ log_{10} \left(\frac{S_i}{1}\right)$

$$S_i = 10^{-16} W$$

The signal power in the output of this GPS receiver will be $C = \frac{G_A.G.Si}{L}$

$$N_0 \times (IHZ) = N$$

 \Rightarrow noise available at antenna output in a one sided BW B is kT_AB W

$$T_{LNA} = (F_{LNA} - 1) 290 K$$

 $T_{\rm LOSS} = (F_{\rm LOSS} - 1) 290 \text{ K}$

We have $F_{LOSS} = L$

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From the formula for a cascade;

$$T_{\rm C} = T_{\rm LNA} + \frac{T_{\rm LOSS}}{G} = \left[F_{\rm LNA} - 1 + \frac{L - 1}{G}\right] 290 {\rm K}$$

Therefore, the effective input referenced noise of the LNA - Lossy line in BW B is

$$KT_{C}B = \left[F_{LNA} - 1 + \frac{L - 1}{G}\right]k(290k)B$$

& total paise power in a BW B at I/P is

$$KT_{A}B + KT_{C}B$$
$$N = \left[T_{A} + \left(F_{LNA} - 1 + \frac{L - 1}{G}\right)290\right]KB$$

B = 1 HZ & apply cascade gain GL^{-1}

$$N = GL^{-1} \left[T_{A} + \left(F_{LNA} - 1 + \frac{L - 1}{G} \right) 290 \right] K$$

$$\therefore \frac{C}{N} = \frac{G_A Si}{K \left[T_A + \left(F_{LNA} - 1 + \frac{L - 1}{G} \right) \times 290 \right]} >, r \text{ this is min } \frac{C}{N} \text{ needed.}$$

From above inequality

$$F_{LNA} \le \frac{G_A Si}{Kr.290} - \frac{T_A}{290} + 1 - \left(\frac{L-1}{G}\right)$$

Evaluate expression with

$$\begin{aligned} \frac{C}{N} &= r = 32 \text{ dB Hz} \rightarrow 1524.89 \\ G_A &= \text{SdB} \rightarrow 3.16 \\ T_A &= 300 \text{ k} \\ G &= 10 \text{ dB} \rightarrow 10.0 \\ L &= 25 \text{ dB} \rightarrow 316.23 \\ F_{LNA} &\leq \frac{3.16 \times 10^{-16}}{(1584.09)(1.38 \times 10^{-23})(290)} - \frac{300}{290} + 1 - \left(\frac{316.23 - 1}{10}\right) \\ F_{LNA} &\leq \frac{3.16 \times 10^{-16}}{(1584.09)(1.38 \times 10^{-23})(290)} - \frac{300}{290} + 1 - \left(\frac{316.23 - 1}{10}\right) \end{aligned}$$

 $F_{LNA} \le 18.26 = 12.6 \text{ dB}$

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(field and cutoff frequency) for the lowest order TE mode of this structure. Assume the metal plates are infinitely wide.



(20 M)

Sol:

Field equations by modifying Maxwell's equations are given by

$$H_{x} = \frac{j}{K_{c}^{2}} \left(\omega \varepsilon \frac{\partial E_{z}}{\partial y} - \beta \frac{\partial H_{z}}{\partial x} \right)$$

$$H_{y} = \frac{-j}{K_{c}^{2}} \left(\omega \varepsilon \frac{\partial E_{z}}{\partial x} + \beta \frac{\partial H_{z}}{\partial y} \right)$$

$$E_{x} = \frac{-j}{K_{c}^{2}} \left(\beta \frac{\partial E_{z}}{\partial x} + \omega \mu \frac{\partial H_{z}}{\partial y} \right)$$

$$E_{y} = \frac{j}{K_{c}^{2}} \left(-\beta \frac{\partial E_{z}}{\partial y} + \omega \mu \frac{\partial H_{z}}{\partial x} \right)$$
where $K_{c}^{2} = K^{2} - \beta^{2}$ & $K = \omega \sqrt{\mu \varepsilon}$

TE wave:

Transverse electric (TE) wave also referred as H-wave are characterized by $E_z = 0 \& H_z \neq 0$ and hence above equation becomes

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$$E_{x} = \frac{-j\omega\mu}{K_{c}^{2}} \frac{\partial H_{z}}{\partial y} \dots \dots (3)$$
$$E_{y} = \frac{j\omega\mu}{K_{c}^{2}} \frac{\partial H_{z}}{\partial x} \dots \dots (4)$$

By solving wave equation

$$H_z(y) = A \cos K_d y$$
; for $0 < y < W (K_c = K_d)$

$$= B \cos K_a(d-y)$$
; for W < y < d (K_c = K_a)

where:

K_d : Cut off wave number in the dielectric

K_c : Cut off wave number in the air dielectric

$$\beta = \sqrt{\epsilon_{\rm r} K_0^2 - K_d^2} = \sqrt{K_0^2 - K_a^2}$$

Also H_z has choosen to satisfy $E_x = 0$ at y = 0, d From the above equation (3)

Since
$$E_x \cong \frac{\partial H_z}{\partial y}$$

 $E_x(y) = \frac{-j\omega\mu}{K_c^2} \frac{\partial H_z}{\partial y} = \frac{j\omega\mu}{K_d} A \sin K_d y$; for $0 \le y < W$
 $= \frac{-j\omega\mu}{K_a} B \sin K_a (d-y)$; for $W \le y \le d$

From the equation of $H_z(y)$ & $E_x(y)$ at y = W, gives

A $\cos K_{d}W + B \cos K_{a} (d - W) = 0$ and(5)

By simplifying the above two equations (5) & (6) $K_d \tan K_a(d-W) + K_a \tan K_d W = 0$

The above equation gives us final field equations.

Cut off frequency:

$$\overline{\beta} = \sqrt{\varepsilon_{\rm r} K_0^2 - K_d^2}$$

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at $\omega = \omega_c$ $\overline{\gamma} = 0$ (or) $\overline{\beta} = 0$ $\varepsilon_r K_0^2 = K_d^2$ $\sqrt{\varepsilon_r} \omega_c \sqrt{\mu_0 \varepsilon_0} = \frac{n\pi}{d}$; n = 0, 1, 2, 3, ... $\sqrt{\varepsilon_r} 2\pi$ $f_c \sqrt{\mu_0 \varepsilon_0} = \frac{n\pi}{d}$ $f_c = \frac{n}{2d\sqrt{\varepsilon_r} \sqrt{\mu_0 \varepsilon_0}}$; For dielectric filled $f_c = \frac{n}{2d\sqrt{\mu_0 \varepsilon_0}}$; for air filled The lowest order possible mode for n = 1, is TE₁

$$f_{c}(TE_{1}) = \frac{1}{2d\sqrt{\varepsilon_{r}}\sqrt{\mu_{0}\varepsilon_{0}}}$$

08. (b) (i) Find the response y(n) of the system shown below to the input



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Sol:
(i)
$$y(n) = x(n)^{*}h(n) - x(n)^{*}h(n - 1)$$

 $= x(n)^{*}[h(n) - h(n - 1)]$
 $= x(n)^{*}[b^{n}u(n) - b^{n-1}u(n-1)]$
 $= \{u(n + 4) - u(n - 9)\}^{*}\{b^{n}u(n) - b^{n-1}u(n - 1)\}$
 $\downarrow_{Take Z.T.}$
 $Y(z) = X(z)H(z) - z^{-1}X(z)H(z)$
 $x(n) = u(n+4) - u(n-9)$
 $= X(z)H(z)(1 - z^{-1})$
 $X(z) = \frac{z^{4} - z^{-9}}{1 - z^{-1}}$
 $= \frac{(1 - z^{-1})}{(1 - bz^{-1})} \cdot \frac{z^{4} - z^{-9}}{(1 - z^{-1})}$
 $Y(z) = \frac{z^{4} - z^{-9}}{1 - bz^{-1}}$
 $\psi_{1Z.T}$
 $y(n) = (b)^{n+4}u(n+4) - (b)^{n-9}u(n-9)$
(ii)
 $x_{1(n)} = \frac{2x_{1(n)} + y_{1(n)}}{2x_{1(n)} + y_{1(n)} +$

 $\frac{|4x_{1}(n-1)|}{|2|} \qquad x_{2}(n) \left[\frac{1}{2}x_{2}(n-3)\right] \qquad y_{2}(n)$ $y_{1}(n) = 2x_{1}(n) + 4x_{1}(n-1) \qquad y_{2}(n) = x_{2}(n-2) + \frac{1}{2}x_{2}(n-3)$ $\frac{Y_{1}(z)}{X_{1}(z)} = 2 + 4z^{-1} \qquad \frac{Y_{2}(z)}{X_{2}(z)} = z^{-2} + \frac{1}{2}z^{-3}$ But $Y_{1}(z) = X_{2}(z)$ $\frac{X_{2}(z)}{X_{1}(z)} = 2 + 4z^{-1} \qquad x(n-n_{0}) \xleftarrow{Z.T} z^{-n_{0}}X(z)$ $\frac{Y_{2}(z)}{X_{2}(z)} \cdot \frac{X_{2}(z)}{X_{1}(z)} = \left[z^{-2} + \frac{1}{2}z^{-3}\right] [2 + 4z^{-1}]$ $\frac{Y_{2}(z)}{X_{1}(z)} = 2z^{-2} + 4z^{-3} + z^{-3} + 2z^{-4} \dots (A)$

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$$Y_{2}(z) = (2z^{-2} + 5z^{-3} + 2z^{-4}) X(z)$$

$$y_{2}(n) = 2x(n-1) + 5x_{1}(n-3) + 2 x_{4}(n-4).$$

$$\underbrace{x_{1}(n)}_{\frac{1}{2}x_{1}(n-2)+} \underbrace{y_{1}(n)}_{\frac{1}{2}x_{1}(n-3)} \underbrace{y_{2}(n)}_{\frac{1}{2}x_{2}(n-1)} \xrightarrow{y_{2}(n)} y_{2}(n)$$
But $Y_{1}(z) = X_{2}(z)$

$$y_{1}(n) = x_{1}(n-2) + \frac{1}{2}x_{4}(n-3) \qquad y_{2}(n) = 2x_{2}(n) + 4x_{2}(n-1)$$

$$\underbrace{Y_{1}(z)}_{X_{1}(z)} = z^{-2} + \frac{1}{2}z^{-3} \qquad \underbrace{Y_{2}(z)}_{X_{2}(z)} = 2 + 4z^{-1}.....(2)$$

$$\underbrace{X_{2}(z)}_{X_{1}(z)} = z^{-2} + \frac{1}{2}z^{-3} \dots \dots \dots (1)$$
Multiply (1) & (2)
$$\underbrace{Y_{2}(z)}_{X_{1}(z)} = \left(z^{-2} + \frac{1}{2}z^{-3}\right)(2 + 4z^{-1})\dots \dots (B)$$

As equations (A) & (B), even if we reverse the sequence, $y_2(n) \& x_1(n)$ holds the same relation as both the systems are L.T.I.

08. (c) A 10 kW transmitter amplitude modulates a carrier with a tone $m(t) = sin (2000\pi t)$, using 50% modulation. Propagation losses between the transmitter and the receiver attenuate the signal by 90 dB. The receiver has a front-end noise $N_0 = -113$ dBW/Hz and includes a BPF $B_T = 2\omega = 10$ kHz. What is the post-detection SNR, assuming the receiver uses an envelope detector? (20 M)

Sol:
$$f_m = 1000 \text{ Hz}$$

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$$\mu = 0.5$$

Loss = 90 dB = 10^{-9} N_D = -113 dBW/Hz = $10^{-11.3}$ W/Hz BW of BPF = 10 kHz

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The component coming at I/P of Envelope Detector is r(t) = s(t) + n(t)

$$r(t) = A_{c} [1 + K_{a}m(t)]\cos(2\pi f_{c}t) + n_{I}(t)\cos(2\pi f_{c}t) - n_{q}(t)\sin(2\pi f_{c}t)$$
$$r(t) = A_{c} [1 + K_{a}m(t) + n_{I}(t)]\cos(2\pi f_{c}t) + n_{q}(t)\sin(2\pi f_{c}t)$$

O/P of Envelope detector is $|\mathbf{r}(t)|$

$$\therefore |\mathbf{r}(t)| = \sqrt{[\mathbf{A}_{c}[\mathbf{l} + \mathbf{K}_{a}\mathbf{m}(t)] + \mathbf{n}_{I}(t)]^{2} + \mathbf{n}_{q}^{2}(t)}$$
$$|\mathbf{r}(t)| = \sqrt{\mathbf{A}_{c}^{2}(\mathbf{l} + \mathbf{K}_{a}\mathbf{m}(t))^{2} + \mathbf{n}_{I}^{2}(t) + 2\mathbf{A}_{c}(\mathbf{l} + \mathbf{K}_{a}\mathbf{m}(t))\mathbf{n}_{I}(t) + \mathbf{n}_{q}^{2}(t)}$$

Considering
$$\sqrt{n_q^2(t)} \ll A_c$$

i.e $|n_I(t)| \ll A_c$ and $|n_q(t)| \ll A$
the NOISE terms $n_I^2(t)$ and $n_q^2(t)$ terms are dropped.

$$|\mathbf{r}(t)| = \sqrt{\mathbf{A}_{c}^{2}(1 + \mathbf{K}_{a}\mathbf{m}(t))^{2} + 2\mathbf{A}_{c}(1 + \mathbf{K}_{a}\mathbf{m}(t))\mathbf{n}_{I}(t)}$$
$$|\mathbf{r}(t)| = \mathbf{A}_{c}[1 + \mathbf{K}_{a}\mathbf{m}(t)] + \mathbf{n}_{I}(t)$$
$$\therefore \text{ O/P signal power neglecting DC terms is } \frac{\mathbf{A}_{c}^{2}\mu^{2}}{2}$$

Power of signal =
$$10^4 \times 10^{-9} = 10^{-5}$$
 W

at Rx Input

 $10^{-5} = \frac{A_c^2}{2} \left[1 + \frac{\mu^2}{2} \right]$ $10^{-5} = \frac{A_c^2}{2} \left[1 + \frac{1}{8} \right]$ $\frac{A_c^2}{2} = \frac{8}{9} \times 10^{-5}$ Solve the second s

Signal power at O/P of Rx = $\frac{8}{9} \times 10^{-5} \times \frac{1}{4} = \frac{2}{9} \times 10^{-5} = 2.22 \,\mu\text{W}$

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Power of Noise component at O/P of filter = $N_0 \times (2f_m) = 10^{-11.3} \times (10 \times 10^3) = 5.01 \times 10^{-8}$ W

$$\left(\frac{S}{N}\right)_{O/P \text{ at ED}} = \frac{2.22 \times 10^{-6}}{5.01 \times 10^{-8}} = 44.31 = 16.46 \text{ dB}$$

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