



GATE | PSUs

MECHANICAL

ENGINEERING



MECHANICAL ENGINEERING

STRENGTH OF MATERIALS

Volume-1 : Study Material with Classroom Practice Questions

Strength of Materials

Solutions for Vol - I _ Classroom Practice Questions

Chapter- 1 Simple Stresses and Strains

Fundamental, Mechanical Properties of Materials, Stress Strain Diagram

01. Ans: (b)

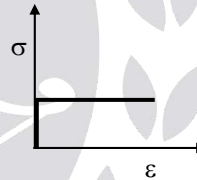
Sol:

- **Ductility:** The property of materials to allow large deformations or large extensions without failure (large plastic zone) is termed as ductility.
- **Brittleness:** A brittle material is one which exhibits a relatively small extensions or deformations prior to fracture. Failure without warning (No plastic zone) i.e. no plastic deformation.
- **Tenacity:** High tensile strength.
- **Creep:** Creep is the gradual increase of plastic strain in a material with time at constant load.
- **Plasticity:** The property by which material undergoes permanent deformation even after removal of load.
- **Endurance limit:** The stress level below which a specimen can withstand cyclic stress indefinitely without failure.
- **Fatigue:** Decreased Resistance of material to repeated reversal of stresses.

02. Ans: (a)

Sol:

- When the material is subjected to stresses, it undergoes to strains. After removal of stress, if the strain is not restored/recovered, then it is called inelastic material.
- For rigid plastic material:



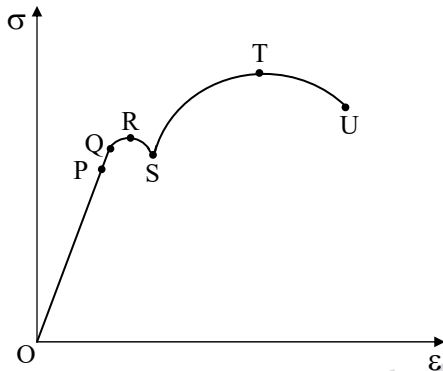
- Any material that can be subjected to large strains before it fractures is called a ductile material. Thus, it has large plastic zone.
- Materials that exhibit little or no yielding before failure are referred as brittle materials. Thus, they have no plastic zone.

03. Ans: (a)

Sol: Refer to the solution of Q. No. (01).

04. Ans: (b)

Sol: The stress-strain diagram for ductile material is shown below.



- P – Proportionality limit
- Q – Elastic limit
- R – Upper yield point
- S – Lower yield point
- T – Ultimate tensile strength
- U – Failure

From above,

- OP → Stage I
- PS → Stage II
- ST → Stage III
- TU → Stage IV

05. Ans: (b)

Sol:

- If the response of the material is independent of the orientation of the load axis of the sample, then we say that the material is **isotropic** or in other words we can say the isotropy of a material is its characteristics, which gives us the information that the properties are same in the three orthogonal directions x, y and z.

- A material is **homogeneous** if it has the same composition throughout the body. Hence, the elastic properties are the same at every point in the body in a given direction. However, the properties need not to be the same in all the directions for the material. Thus, both A and B are false.

06. Ans: (a)

Sol: **Strain hardening** increase in strength after plastic zone by rearrangement of molecules in material.

- **Visco-elastic material** exhibits a mixture of creep as well as elastic after effects at room temperature. Thus their behavior is time dependant

07. Ans: (a)

Sol: Refer to the solution of Q. No. (01).

08. Ans: (a)

Sol: Modulus of elasticity (Young's modulus) of some common materials are as follow:

Material	Young's Modulus (E)
Steel	200 GPa
Cast iron	100 GPa
Aluminum	60 to 70 GPa
Timber	10 GPa
Rubber	0.01 to 0.1 GPa

09. Ans: (a)

Sol: Addition of carbon will increase strength, thereby ductility will decrease.



Elastic Constants and Their Relationships

01. Ans (c)

Sol: We know that,

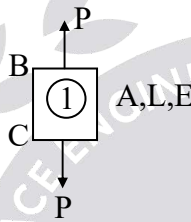
$$\text{Poisson's ratio} = \frac{\text{Lateral strain}}{\text{Linear strain}} = \frac{\Delta D/D}{\Delta L/L}$$

$$\therefore \mu = \frac{\frac{\Delta D/8}{PL}}{\frac{AE}{L}}$$

$$\therefore \mu = \frac{\Delta D}{8} \frac{AE}{P}$$

$$\therefore 0.25 = \frac{\Delta D}{8} \frac{\pi}{4} \frac{(8)^2 \times 10^6}{50000}$$

$$\Rightarrow \Delta D = 1.98 \times 10^{-3} \cong 0.002 \text{ cm}$$



02. Ans: (c)

Sol: We know that,

$$\text{Bulk modulus} = \frac{\delta P}{\delta V/V}$$

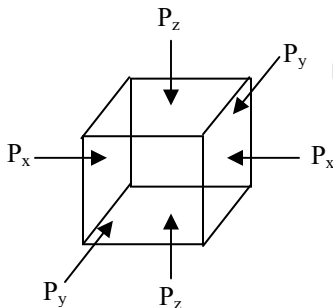
$$\Rightarrow 2.5 \times 10^5 = \frac{200 \times 20}{\delta V}$$

$$\Rightarrow \delta V = 0.016 \text{ m}^3$$

Linear and Volumetric Changes of Bodies

01. Ans: (d)

Sol:



Let $P_y = P_z = P$

$$\epsilon_y = 0,$$

$$\epsilon_z = 0$$

$$\epsilon_y = \frac{\sigma_y}{E} - \mu \frac{\sigma_z}{E} - \mu \frac{\sigma_x}{E}$$

$$\therefore 0 = \frac{(-P)}{E} - \mu \frac{(-P)}{E} - \mu \frac{(P_x)}{E}$$

$$\Rightarrow P = \frac{\mu \cdot P_x}{(1 - \mu)}$$



02. Ans: (a)

Sol: Given that, $\sigma_c = 4\tau$

Punching force = Shear resistance of plate

$$\therefore \sigma (\text{Cross section area}) = \tau (\text{surface Area})$$

$$\therefore 4 \times \tau \times \frac{\pi \cdot D^2}{4} = \tau (\pi \cdot D \cdot t)$$

$$\Rightarrow D = t = 10 \text{ mm}$$

03. Ans: (d)

Sol:



$$\sigma_s = 140 \text{ MPa} = \frac{P_s}{A_s}$$

$$\Rightarrow P_s = \frac{140 \times 500}{3} \approx 23,300 \text{ N}$$



$$\sigma_{Al} = 90 \text{ MPa} = \frac{P_{Al}}{A_{Al}}$$

$$\Rightarrow P_{Al} = 90 \times 400 = 36,000 \text{ N}$$



$$\sigma_B = 100 \text{ MPa} = \frac{P_B}{A_B}$$

$$\Rightarrow P_B = \frac{100 \times 200}{2} = 10,000 \text{ N}$$

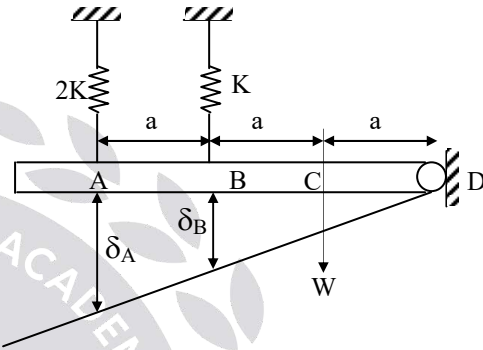
Take minimum value from P_s , A_{Al} and P_B .

$$\Rightarrow P = 10,000 \text{ N}$$

[Correct answer is (d)]

04. Ans: (c)

Sol:



From similar triangle

$$\frac{3a}{\delta_A} = \frac{2a}{\delta_B}$$

$$3\delta_B = 2\delta_A \dots\dots (1)$$

$$\text{Stiffness } K = \frac{W}{\delta}$$

$$\therefore K_A = \frac{W_A}{\delta_A} \Rightarrow \delta_A = \frac{W_A}{2K}$$

Similarly $\delta_B = \frac{W_B}{K}$

From equation (1) $3 \times \frac{W_B}{K} = 2 \times \frac{W_A}{2K}$

$$\Rightarrow \frac{W_A}{W_B} = 3$$



Thermal/Temperature Stresses

01. Ans: (b)

Sol: Free expansion = Expansion prevented

$$[\ell \alpha t]_s + [\ell \alpha t]_{Al} = \left[\frac{P\ell}{AE} \right]_s + \left[\frac{P\ell}{AE} \right]_{Al}$$

$$11 \times 10^{-6} \times 20 + 24 \times 10^{-6} \times 20 = \frac{P}{100 \times 10^3 \times 200} + \frac{P}{200 \times 10^3 \times 70}$$

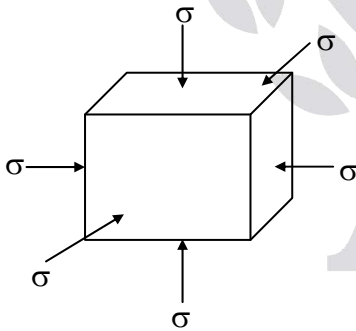
$$\Rightarrow P = 5.76 \text{ kN}$$

$$\sigma_s = \frac{P}{A_s} = \frac{5.76 \times 10^3}{100} = 57.65 \text{ MPa}$$

$$\sigma_{Al} = \frac{P}{A_{al}} = \frac{5.76 \times 10^3}{200} = 28.82 \text{ MPa}$$

02. Ans: (a)

Sol:



Strain in X-direction due to temperature,

$$\epsilon_t = \alpha (\Delta T)$$

Strain in X-direction due to volumetric stress,

$$\epsilon_x = \frac{\sigma_x}{E} - \mu \frac{\sigma_y}{E} - \mu \frac{\sigma_z}{E}$$

$$\therefore \epsilon_x = \frac{-\sigma}{E} (1 - 2\mu)$$

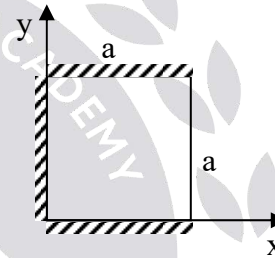
$$\therefore -\sigma = \frac{(\epsilon_x)(E)}{1 - 2\mu}$$

$$\therefore -\sigma = \frac{\alpha(\Delta T)E}{(1 - 2\mu)}$$

$$\Rightarrow \sigma = \frac{-\alpha(\Delta T)E}{1 - 2\mu}$$

03. Ans: (b)

Sol:



- Free expansion in x direction is $\alpha \Delta t$.
- Free expansion in y direction is $\alpha \Delta t$.
- Since there is restriction in y direction expansion doesn't take place. So in lateral direction, increase in expansion due to restriction is $\mu \alpha \Delta t$.

Thus, total expansion in x direction is,

$$= a \alpha \Delta t + \mu a \alpha \Delta t$$

$$= a \alpha \Delta t (1 + \mu)$$



Chapter- 2
Complex Stresses and Strains

01. Ans: (b)

Sol: Maximum principal stress $\sigma_1 = 18$

Minimum principal stress $\sigma_2 = -8$

$$\text{Maximum shear stress} = \frac{\sigma_1 - \sigma_2}{2} = 13$$

Normal stress on Maximum shear stress plane

$$= \frac{\sigma_1 + \sigma_2}{2} = \frac{18 + (-8)}{2} = 5$$

02. Ans: (b)

Sol: Radius of Mohr's circle, $\tau_{\max} = \frac{\sigma_1 - \sigma_2}{2}$

$$\therefore 20 = \frac{\sigma_1 - 10}{2}$$

$$\Rightarrow \sigma_1 = 50 \text{ N/mm}^2$$

03. Ans: (b)

Sol: Given data,

$$\sigma_x = 150 \text{ MPa}, \sigma_y = -300 \text{ MPa}, \mu = 0.3$$

Long dam \rightarrow plane strain member

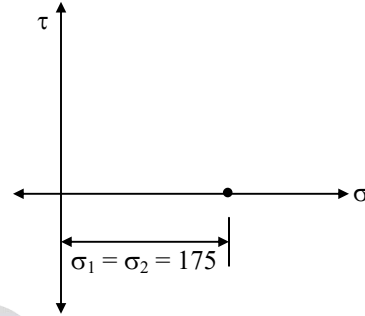
$$\epsilon_z = 0 = \frac{\sigma_z}{E} - \frac{\mu\sigma_x}{E} - \frac{\mu\sigma_y}{E}$$

$$\therefore 0 = \sigma_z - 0.3 \times 150 + 0.3 \times 300$$

$$\Rightarrow \sigma_z = 45 \text{ MPa}$$

04. Ans: (b)

Sol:



From the above, we can say that Mohr's circle is a point located at 175 MPa on normal stress axis.

Thus, $\sigma_1 = \sigma_2 = 175 \text{ MPa}$

05. Ans: (c)

Sol: Given that, $\sigma_2 = 0$

$$\therefore \sigma_2 = \frac{\sigma_x + \sigma_y}{2} - \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$$

$$\therefore \frac{\sigma_x + \sigma_y}{2} = \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$$

$$\therefore \left(\frac{\sigma_x + \sigma_y}{2}\right)^2 = \left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2$$

$$\therefore \tau_{xy}^2 = \left(\frac{\sigma_x + \sigma_y}{2}\right)^2 - \left(\frac{\sigma_x - \sigma_y}{2}\right)^2$$

$$\therefore \tau_{xy}^2 = \sigma_x \cdot \sigma_y$$

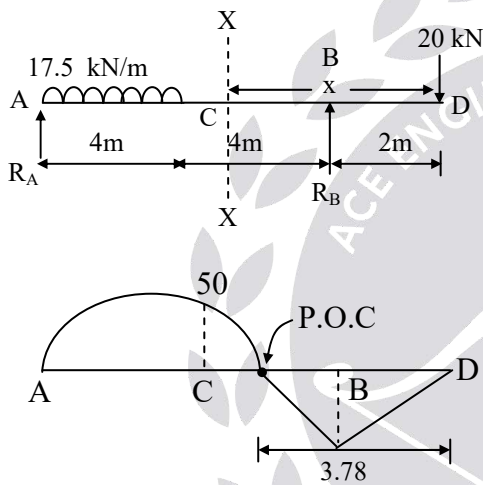
$$\Rightarrow \tau_{xy} = \sqrt{\sigma_x \cdot \sigma_y}$$



Chapter- 3
Shear Force and Bending Moment

01. Ans: (b)

Sol: Contra flexure is the point where BM is becoming zero.



Taking moment about A,

$$\Sigma M_A = 0$$

$$\therefore 17.5 \times 4 \times \frac{4}{2} + 20 \times 10 - R_B \times 8 = 0$$

$$\therefore R_B = 42.5 \text{ kN}$$

$$\text{Now, } M_x = -20x + R_B(x - 2)$$

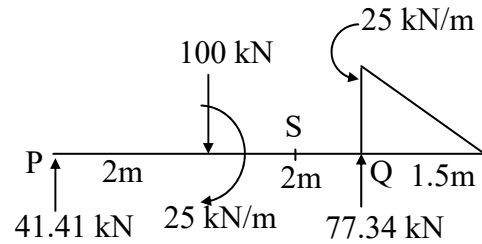
For bending moment be zero $M_x = 0$,

$$-20x + 42.5(x - 2) = 0$$

$$\Rightarrow x = 3.78 \text{ m from right i.e. from D.}$$

02. Ans: (b)

Sol:



Take $\Sigma M_P = 0$

$$\frac{1}{2} \times 25 \times 1.5 \times \left(\frac{1.5}{3} + 4 \right) - (R_Q \times 4) + 100 \times 2 + 25 = 0$$

$$\therefore R_Q = 77.34 \text{ kN}$$

Also, $\Sigma V = 0$

$$\therefore R_P + R_Q = 100 + \frac{1}{2} \times 25 \times 1.5 = 118.75 \text{ kN}$$

$$\therefore R_P = 41.41 \text{ kN}$$

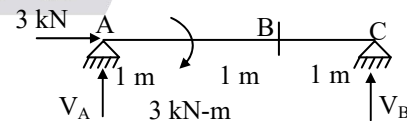
$$\Rightarrow \text{Shear force at P} = 41.41 \text{ kN}$$

03. Ans: (c)

$$\text{Sol: } M_S = R_P(3) + 25 - (100 \times 1) = 49.2 \text{ kN-m}$$

04. Ans: (c)

Sol:



$$-V_B \times 3 + 3 = 0$$

$$\therefore V_C = 1 \text{ kN}$$

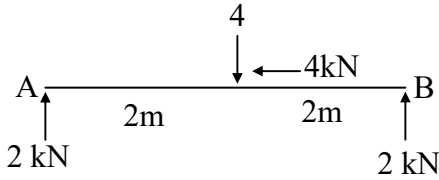
$$\therefore \text{Bending moment at B,}$$

$$\Rightarrow M_B = V_C \times 1 = 1 \text{ kN-m}$$



05. Ans: (a)

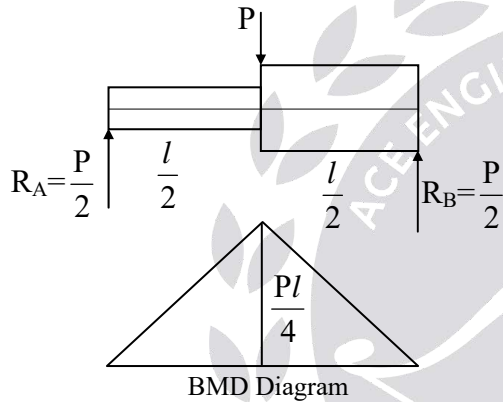
Sol:



Reaction at both the supports are 2 kN and in upward direction.

06. Ans: (c)

Sol:



Bending moment at $\frac{l}{2}$ from left is $\frac{Pl}{4}$.

The given beam is statically determinate structure. Therefore equilibrium equations are sufficient to analyze the problem.

In statically determinate structure the BMD, SFD and Axial force are not affected by section (I), material (E), thermal changes.

07. Ans: (a)

Sol: As the given support is hinge, for different set of loads in different direction beam will experience only axial load.

Chapter- 4 Centre of Gravity & Moment of Inertia

01. Ans: (a)

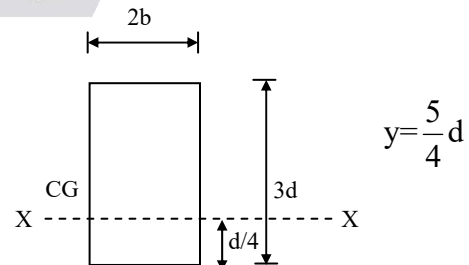
$$\begin{aligned} \bar{y} &= \frac{E_1 y_1 + E_2 y_2}{E_1 + E_2} \\ \Rightarrow \bar{y} &= \frac{2E_2 \left(h + \frac{h}{2} \right) + E_2 \times \frac{h}{2}}{2E_2 + E_2} \quad (\because E_1 = 2E_2) \\ \Rightarrow \bar{y} &= 1.167h \text{ from base} \end{aligned}$$

02. Ans: (b)

$$\begin{aligned} \bar{y} &= \frac{A_1 E_1 Y_1 + A_2 E_2 Y_2}{A_1 E_1 + A_2 E_2} \\ &= \frac{1.5a \times 3a^2 \times E_1 + 1.5a \times 6a^2 \times 2E_1}{3a^2 E_1 + 6a^2 (2E_1)} \\ &= \frac{22.5a^3 E_1}{15a^2 E_1} = 1.5a \end{aligned}$$

03. Ans: $13.875 bd^3$

Sol:



$$y = \frac{5}{4}d$$



$$\text{M.I about CG} = I_{CG} = \frac{2b(3d)^3}{12} = \frac{9}{2}bd^3$$

$$\begin{aligned} \text{M.I about X-X} \Big|_{\text{at } \frac{d}{4} \text{ distance}} &= I_G + Ay^2 \\ &= \frac{9}{2}bd^3 + 6bd\left(\frac{5}{4}\right)^2 d^2 \\ &= \frac{111}{8}bd^3 = 13.875bd^3 \end{aligned}$$

04. Ans: $6.885 \times 10^6 \text{ mm}^4$

Sol:

$$\begin{aligned} I_x &= \frac{BD^3}{12} - 2\left(\frac{bd^3}{12} + Ah^2\right) \\ &= \frac{60 \times 120^3}{12} - 2\left(\frac{30 \times 30^3}{12} + (30 \times 30) \times 30^2\right) \\ &= 6.885 \times 10^6 \text{ mm}^4 \end{aligned}$$

05. Ans: 152146 mm^4

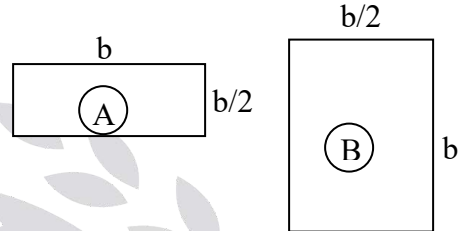
Sol:

$$\begin{aligned} I_x &= \frac{30 \times 40^3}{12} - \frac{\pi \times 20^4}{64} = 152146 \text{ mm}^4 \\ I_y &= \frac{40 \times 30^3}{12} - \left(\frac{\pi \times 20^4}{64} + 2\left(\frac{\pi}{2} \times 10^2 \times \left(15 - \frac{4 \times 10}{3\pi}\right)^2 \right) \right) \\ &= 45801.34 \text{ mm}^4 \end{aligned}$$

Chapter- 5 Theory of Simple Bending

01. Ans: (b)

Sol:



By using flexural formula, $\sigma = \frac{M}{Z}$

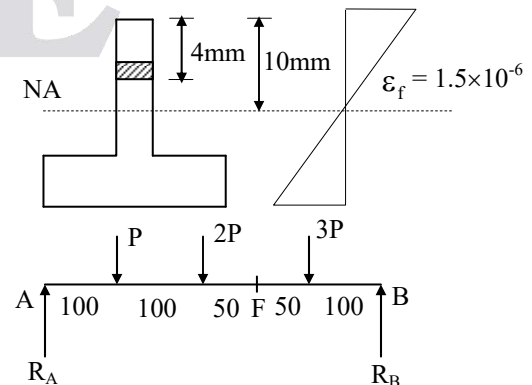
$$\therefore \sigma \propto \frac{1}{Z} \quad (\because M \text{ is constant})$$

$$\therefore \frac{\sigma_A}{\sigma_B} = \frac{Z_B}{Z_A} = \frac{\frac{6}{\left(\frac{b}{2}\right) \times b^2}}{b \times \left(\frac{b}{2}\right)^2} = 2$$

$$\Rightarrow \sigma_A = 2\sigma_B$$

02. Ans: (b)

Sol:





$$\therefore \sum M_A = 0$$

$$\therefore P \times 100 + 2P \times 200 + 3P \times 300 = R_B \times 400$$

$$\therefore R_B = 3.5P, R_A = 2.5P$$

Take moments about F and moment at F

$$M_F = R_B \times 150 - 3P \times 50 = 375P$$

$$\text{Also, } \frac{M_F}{I} = \frac{\sigma_b}{y_F}$$

$$\therefore \frac{375P}{2176} = \frac{(1.5 \times 10^{-6} \times 200 \times 10^3)}{6}$$

$$\Rightarrow P = 0.29 \text{ N}$$

03. Ans: (b)

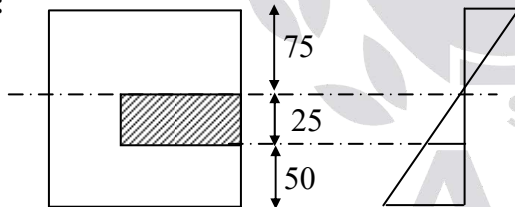
Sol: By using Flexural formula,

$$\frac{E}{R} = \frac{\sigma_b}{y_{\max}} \Rightarrow \frac{2 \times 10^5}{250} = \frac{\sigma_b}{(0.5/2)}$$

$$\Rightarrow \sigma_b = 200 \text{ N/mm}^2$$

04. Ans: (c)

Sol:



By using flexural formula,

$$\frac{M}{I} = \frac{f}{y}$$

$$\therefore \frac{16 \times 10^6}{100 \times 150^3} = \frac{f}{25} \Rightarrow f = 14.22 \text{ MPa}$$

Now, Force on hatched area

$$= \text{Average stress} \times \text{Hatched area}$$

$$= \left(\frac{0 + 14.22}{2} \right) (25 \times 50) = 8.9 \text{ kN}$$

05. Ans: (b)

Sol: By using flexural formula, $\frac{f_{\text{Tensile}}}{y_{\text{top}}} = \frac{M}{I}$

$$\Rightarrow f_{\text{Tensile}} = \frac{0.3 \times 3 \times 10^6}{3 \times 10^6} \times 70$$

(maximum bending stress will be at top fibre so $y_1 = 70 \text{ mm}$)

$$\Rightarrow f_{\text{Tensile}} = 21 \text{ N/mm}^2 = 21 \text{ MN/m}^2$$

06. Ans: (c)

Sol: Given data:

$$P = 200 \text{ N,}$$

$$M = 200 \text{ N.m}$$

$$A = 0.1 \text{ m}^2,$$

$$I = 1.33 \times 10^{-3} \text{ m}^4$$

$$y = 20 \text{ mm}$$

Due to direct tensile force P,

$$\sigma_d = \frac{P}{A} = \frac{200}{0.1}$$

$$= 2000 \text{ N/m}^2 \text{ (Tensile)}$$

Due to the moment M,

$$\sigma_b = \frac{M}{I} \times y$$

$$= \frac{200}{1.33 \times 10^{-3}} \times 20 \times 10^{-3}$$

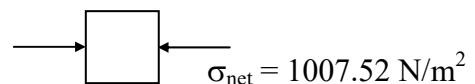
$$= 3007.52 \text{ N/m}^2 \text{ (Compressive)}$$

$$\sigma_{\text{net}} = \sigma_d - \sigma_b$$

$$= 2000 - 3007.52$$

$$= -1007.52 \text{ N/m}^2$$

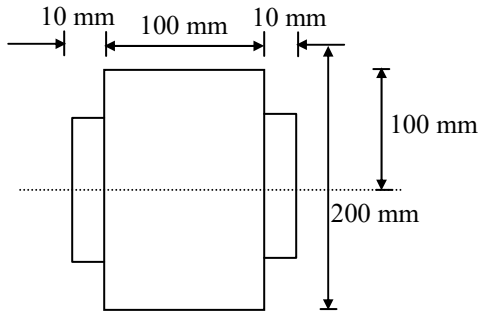
Negative sign indicates compressive stress.





07. Ans: 80 MPa

Sol:



Maximum stress in timber = 8 MPa

Modular ratio, $m = 20$

Stress in timber in steel level,

$$100 \rightarrow 8$$

$$50 \rightarrow f_w$$

$$\Rightarrow f_w = 4 \text{ MPa}$$

Maximum stress developed in steel is = $m \cdot f_w$
 $= 20 \times 4 = 80 \text{ MPa}$

Convert whole structure as a steel structure by using modular ratio.

08. Ans: 2.43 mm

Sol: From figure $A_1B_1 = l = 3 \text{ m}$ (given)

$$AB = \left(R - \frac{h}{2} \right) \alpha = l - l\alpha t_1 \text{ ----- (1)}$$

$$A_2B_2 = \left(R + \frac{h}{2} \right) \alpha = l + l\alpha t_2 \text{ ----- (2)}$$

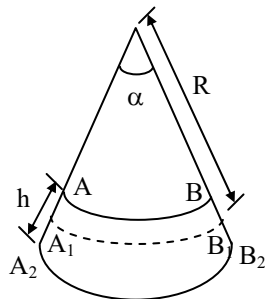
Subtracting above two equations (2) - (1)

$$h(\alpha) = l\alpha(t_2 - t_1)$$

but $A_1B_1 = l = R\alpha$

$$\Rightarrow \alpha = \frac{l}{R}$$

$$\therefore h \left(\frac{l}{R} \right) = l\alpha(\Delta T)$$



$$R = \frac{h}{\alpha(\Delta T)}$$

$$= \frac{250}{(1.5 \times 10^{-5})(72 - 36)}$$

$$R = 462.9 \text{ m}$$

From geometry of circles

$$(2R - \delta)\delta = \frac{L}{2} \cdot \frac{L}{2} \text{ \{ref. figure in Q.No.02\}}$$

$$2R\delta - \delta^2 = \frac{L^2}{4} \text{ (neglect } \delta^2)$$

$$\delta = \frac{L^2}{8R} = \frac{3^2}{8 \times 462.9} = 2.43 \text{ mm}$$

Shortcut:

Deflection is due to differential temperature of bottom and top ($\Delta T = 72^\circ - 36^\circ = 36^\circ$). Bottom temperature being more, the beam deflects down.

As derived in the Q2 (2 marks)

$$\delta = \frac{\alpha(\Delta T)l^2}{8h} = \frac{1.5 \times 10^{-5} \times 36 \times 3000^2}{8 \times 250}$$

$$= 2.43 \text{ mm (downward)}$$



Chapter- 6
Shear Stress Distribution in Beams

01. Ans: (a)

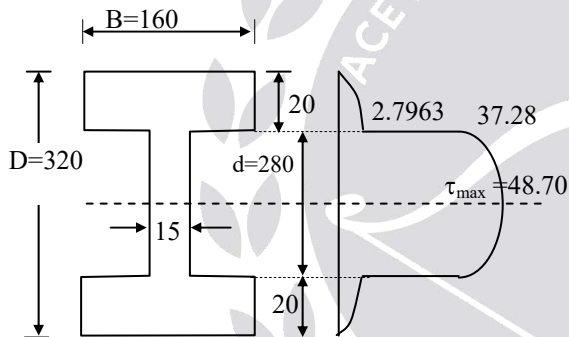
Sol: $\tau_{\max} = \frac{3}{2} \times \tau_{\text{avg}} = \frac{3}{2} \times \frac{f}{b.d}$

$$3 = \frac{3}{2} \times \frac{50 \times 10^3}{100 \times d}$$

$\therefore d = 250 \text{ mm} = 25 \text{ cm}$

02. Ans: 37.3

Sol:



All dimensions are in mm

Bending moment (M) = 100 kN-m,

Shear Force (SF) = f = 200 kN

$$I = \frac{160 \times 320^3}{12} - \frac{145 \times 280^3}{12}$$

$$= 171.65 \times 10^6 \text{ mm}^4$$

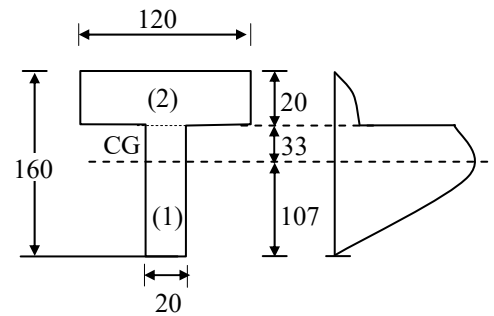
$$\tau_{\text{at interface of flange \& web}} = \frac{FA\bar{y}}{Ib}$$

$$= \frac{200 \times 10^3}{171.65 \times 10^6 \times 15} \times (160 \times 20 \times 150)$$

$$= 37.28 \text{ MPa}$$

03. Ans: 61.43 MPa

Sol:



All dimensions are in mm

$$I_{NA} = 13 \times 10^6 \text{ mm}^4$$

$$y_{CG} = 107 \text{ mm from base}$$

$$\tau_{\max} = \frac{FA\bar{y}}{Ib}$$

$$A\bar{y} = (120 \times 20 \times 43) + (33 \times 20 \times 16.5)$$

$$= 114090 \text{ mm}^3$$

$$\tau_{\max} = \frac{140 \times 10^3 \times 114090}{13 \times 10^6 \times 20} = 61.43 \text{ MPa}$$



Chapter- 7
Torsion

01. Ans: (c)

Sol: Twisting moment = $2 \times 0.5 + 1 \times 0.5$
= 1.5 kN-m

Correct answer is (c).

02. Ans: (d)

Sol: $\frac{(\text{Strength})_{\text{solid}}}{(\text{Strength})_{\text{hollow}}} = \frac{1}{1 - K^4}$
= $\frac{1}{1 - \left(\frac{1}{2}\right)^4} = \frac{16}{15}$

03. Ans: 43.27 MPa & 37.5 MPa

Sol: Given $D_o = 30 \text{ mm}$, $t = 2 \text{ mm}$
 $\therefore D_i = 30 - 4 = 26 \text{ mm}$

We know that $\frac{\tau}{J} = \frac{q}{R}$

$$\frac{100 \times 10^3}{\pi(30^4 - 26^4)} = \frac{q_{\text{max}}}{\left(\frac{30}{2}\right)}$$

$$q_{\text{max}} = 43.279 \text{ N/mm}^2$$

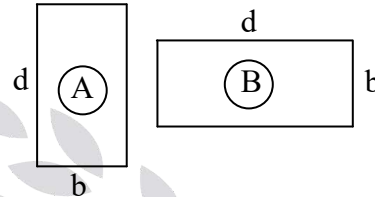
$$\frac{100 \times 10^3}{\pi(30^4 - 26^4)} = \frac{q_{\text{min}}}{\left(\frac{26}{2}\right)}$$

$$q_{\text{min}} = 37.5 \text{ N/mm}^2$$

Chapter- 8
Slopes and Deflections

01. Ans: (c)

Sol:



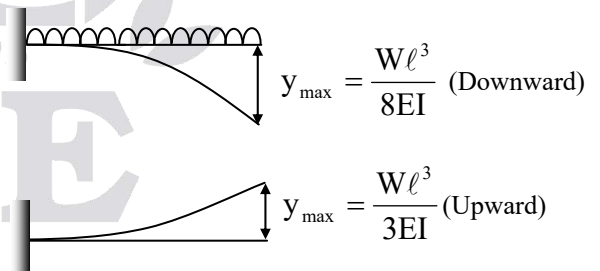
$$y_{\text{max}} \propto \frac{1}{I}$$

$$\therefore \frac{y_A}{y_B} = \frac{I_B}{I_A}$$

$$y_B = \frac{y_A \times bd^3 / 12}{db^3 / 12} \Rightarrow y_B = \left(\frac{d}{b}\right)^2 y_A$$

02. Ans: (b)

Sol: Total load $W = wl$



$$y_{\text{net}} = \downarrow y_{\text{udl}} - \uparrow y_w$$

$$\text{Total Net deflection} = \frac{WL^3}{8EI} - \frac{WL^3}{3EI}$$

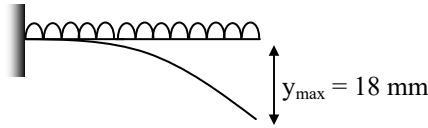
$$= \frac{-5WL^3}{24EI}$$

(Negative sign indicates upward deflection)



03. Ans: (c)

Sol:



$$\theta_{\max} = \frac{wl^3}{6EI} = 0.02 \quad \text{-----(i)}$$

$$y_{\max} = \frac{wL^4}{8EI}$$

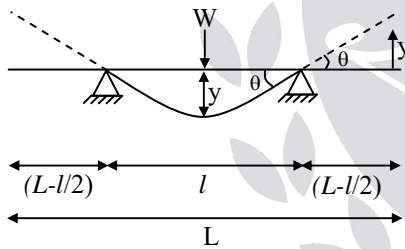
$$\therefore 0.018 = \left(\frac{WL^3}{6EI} \right) \times \frac{L \times 6}{8}$$

$$\therefore 0.018 = \frac{0.02 \times L \times 6}{8} \quad [\because \text{Equation (i)}]$$

$$\Rightarrow L = 1.2 \text{ m}$$

04. Ans: (a)

Sol:



Conditions given

$$\downarrow y = \frac{wl^3}{48EI}$$

$$\theta = \frac{wl^2}{16EI}$$

$$\tan\theta = \frac{y}{(L-l)/2}$$

θ is small $\Rightarrow \tan \theta = \theta$

$$\therefore \theta = \frac{y}{(L-l)/2}$$

$$\therefore y = \theta \left(\frac{L-l}{2} \right)$$

$$\uparrow y = \theta \left(\frac{L-l}{2} \right)$$

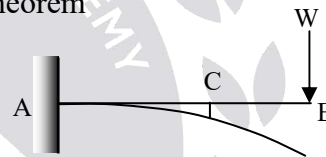
Thus $y \downarrow = y \uparrow$

$$\therefore \frac{wl^3}{48EI} = \frac{wl^2}{16EI} \times \left(\frac{L-l}{2} \right)$$

$$\Rightarrow \frac{L}{l} = \frac{5}{3}$$

05. Ans: (c)

Sol: By using Maxwell's law of reciprocals theorem



$$\delta_{C/B} = \delta_{B/C}$$

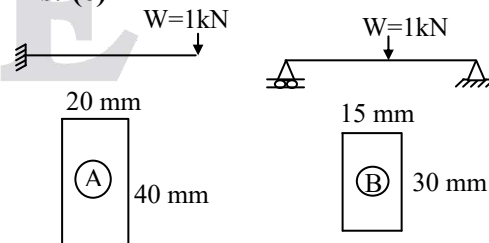
Deflection at 'C' due to unit load at 'B'

= Deflection at 'B' due to unit load at 'C'

As the load becomes half deflection becomes half.

06. Ans: (c)

Sol:



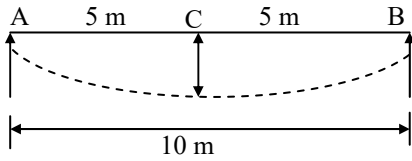
$$y_A = y_B \Rightarrow \left(\frac{wL^3}{3EI} \right)_A = \left(\frac{wL^3}{48EI} \right)_B$$

$$\therefore L_B = 400 \text{ mm}$$



07. Ans: 0.05

Sol:



$$\therefore \text{Curvature, } \frac{d^2y}{dx^2} = 0.004$$

Integrating with respect to x,

$$\text{We get, } \frac{dy}{dx} = 0.004x$$

$$y = \frac{0.004x^2}{2}$$

$$y = 0.002x^2$$

At mid span, $x = 5 \text{ m}$

$$\therefore y = 0.002 \times 5^2$$

$$y = 0.05 \text{ m}$$

Chapter- 9 Thin Pressure Vessels

01. Ans: (b)

$$\text{Sol: } \tau_{\max} = \sigma_1 = \frac{\sigma_h - 0}{2} = \frac{PD}{4t}$$

$$\therefore \tau_{\max} = \frac{1.6 \times 900}{4 \times 12} = 30 \text{ MPa}$$

02. Ans: 2.5 MPa & 2.5 MPa

Sol: Given data:

$$R = 0.5 \text{ m, } D = 1 \text{ m, } t = 1 \text{ mm,}$$

$$H = 1 \text{ m, } \gamma = 10 \text{ kN/m}^3, h = 0.5 \text{ m}$$

At mid-depth of cylindrical wall ($h = 0.5 \text{ m}$):

Circumferential (hoop) stress,

$$\begin{aligned} \sigma_c &= \frac{P_{\text{at } h=0.5\text{m}} \times D}{4t} = \frac{\gamma h \times D}{4t} \\ &= \frac{10 \times 10^3 \times (2 \times 0.5)}{4 \times 1 \times 10^{-3}} \\ &= 2.5 \times 10^6 \text{ N/m}^2 = 2.5 \text{ MPa} \end{aligned}$$

Longitudinal stress at mid-height,

$$\begin{aligned} \sigma_\ell &= \frac{\text{Net weight of the water}}{\text{Cross-section area}} \\ &= \frac{\gamma \times \text{Volume}}{\pi D \times t} \\ &= \frac{\gamma \times \frac{\pi}{4} D^2 L}{\pi D \times t} = \frac{\gamma \times DL}{4t} \\ &= \frac{10 \times 10^3 \times 1 \times 1}{4 \times 10^{-3}} \\ &= 2.5 \times 10^6 \text{ N/m}^2 = 2.5 \text{ MPa} \end{aligned}$$



Chapter- 10
Columns

01. Ans: (c)

Sol: By using Euler's formula, $P_e = \frac{\pi^2 \times EI}{l_e^2}$

For a given system, $l_e = \frac{l}{2}$

$$\therefore P_e = \frac{4\pi^2 \times EI}{l^2}$$

02. Ans: (b)

Sol: We know that, $P_{cr} = \frac{\pi^2 EI}{l_e^2}$

$$\therefore P_{cr} \propto \frac{1}{l_e^2}$$

$$\therefore \frac{P_1}{P_2} = \frac{l_{2e}^2}{l_{1e}^2}$$

$$\therefore \frac{P_1}{P_2} = \frac{l^2}{(2l)^2} \Rightarrow P_1 : P_2 = 1 : 4$$

03. Ans: 4

Sol: Euler's crippling load,

$$P = \frac{\pi^2}{l^2} EI$$

$$\therefore P \propto I$$

$$\Rightarrow \frac{P}{P_o} = \frac{I_{bonded}}{I_{loose}} = \frac{\left[\frac{b(2t)^3}{12} \right]}{2 \left[\frac{bt^3}{12} \right]} = 4$$

04. Ans: (c)

Sol: Euler's theory is applicable for axially loaded columns.

$$\text{Force in member AB, } P_{AB} = \frac{F}{\cos 45^\circ} = \sqrt{2}F$$

$$P_{AB} = \frac{\pi^2 EI}{L_e^2}$$

$$\therefore \sqrt{2} F = \frac{\pi^2 EI}{L_e^2}$$

$$\Rightarrow F = \frac{\pi^2 EI}{\sqrt{2} L^2} \quad \text{Correct answer is (c).}$$

05. Ans: (a)

Sol: Given data:

$$L_e = L = 3 \text{ m ,}$$

$$\alpha = 12 \times 10^{-6} / ^\circ\text{C,}$$

$$d = 50 \text{ mm} = 0.05 \text{ m}$$

$$\text{Buckling load, } P_e = \frac{\pi^2 EI}{L_c^2}$$

$$\therefore \frac{P_e L}{AE} = L \alpha \Delta T$$

$$\therefore \frac{\pi^2 EI \times L}{L^2 \times AE} = L \alpha \Delta T$$

$$\therefore \frac{\pi^2 \times E \times \frac{\pi}{64} \times d^4 \times L}{L^2 \times \frac{\pi}{4} d^2 \times E} = L \alpha \Delta T$$

$$\therefore \Delta T = \frac{\pi^2 \times d^2}{16 \times L^2 \times \alpha} = \frac{\pi^2 \times (0.05)^2}{16 \times 3^2 \times 12 \times 10^{-6}}$$

$$\Rightarrow \Delta T = 14.3^\circ\text{C}$$



**Chapter- 11
Strain Energy**

01. Ans: (*)

Sol:

- Slope of the stress-strain curve in the elastic region is called modulus of elasticity.

For the given curves,

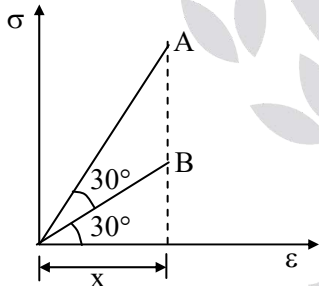
$$(\text{Modulus of elasticity})_A > (\text{Modulus of elasticity})_B$$

$$\therefore E_A > E_B$$

- The material for which plastic region is more is stress-strain curve is possessed high ductility. Thus, $D_B > D_A$.

02. Ans: (b)

Sol:

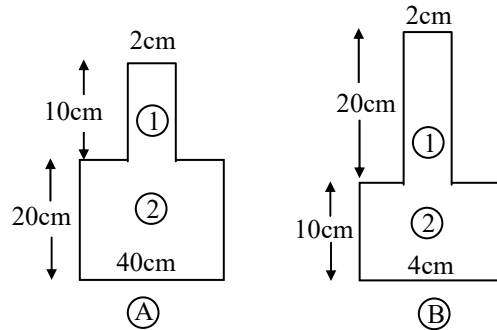


$$\frac{(SE)_A}{(SE)_B} = \frac{\text{Area under curve A}}{\text{Area under curve B}}$$

$$= \frac{\frac{1}{2} \times x \times x \tan 60^\circ}{\frac{1}{2} \times x \times x \tan 30^\circ} = \frac{3}{1}$$

03. Ans: (a)

Sol:



$$\frac{U_B}{U_A} = \frac{(V_1 + V_2)_B}{(V_1 + V_2)_A}$$

$$\begin{aligned} \therefore \frac{U_B}{U_A} &= \frac{\left[\frac{\sigma_1^2}{2E} \times V_1 + \frac{\sigma_2^2}{2E} \times V_2 \right]_B}{\left[\frac{\sigma_1^2}{2E} \times V_1 + \frac{\sigma_2^2}{2E} \times V_2 \right]_A} \\ &= \frac{\left[\frac{P^2}{A_1^2} \times A_1 \times L_1 + \frac{P^2 \times A_2 \times L_2}{A_2^2} \right]_B}{\left[\frac{P^2 \times A_1 \times L_1}{A_1^2} + \frac{P^2 \times A_2 \times L_2}{A_2^2} \right]_A} \\ \Rightarrow \frac{U_B}{U_A} &= \frac{\left[\frac{L_1}{A_1} + \frac{L_2}{A_2} \right]_B}{\left[\frac{L_1}{A_1} + \frac{L_2}{A_2} \right]_A} = \frac{7.165}{4.77} = \frac{3}{2} \end{aligned}$$

04. Ans: (c)

Sol: A_1 = Modulus of resilience

$A_1 + A_2$ = Modulus of toughness

$$A_1 = \frac{1}{2} \times 0.004 \times 70 \times 10^6 = 14 \times 10^4$$

$$\begin{aligned} A_2 &= \frac{1}{2} \times (0.008 \times 50 \times 10^6) + (0.008 \times 70 \times 10^6) \\ &= 76 \times 10^4 \end{aligned}$$

$$A_1 + A_2 = (14 + 76) \times 10^4 = 90 \times 10^4$$



05. Ans: (d)

Sol: Strain energy, $U = \frac{P^2}{2A^2E} \cdot V$

$\therefore U \propto P^2$

Due to the application of P_1 and P_2 one after the other

$(U_1 + U_2) \propto P_1^2 + P_2^2 \dots\dots\dots (1)$

Due to the application of P_1 and P_2 together at the same time.

$U \propto (P_1 + P_2)^2 \dots\dots\dots(2)$

It is obvious that,

$(P_1^2 + P_2^2) < (P_1 + P_2)^2$

$\Rightarrow (U_1 + U_2) < U$

06. Ans: 1.5

Sol: Given data:

$L = 100 \text{ mm}$

$G = 80 \times 10^3 \text{ N/mm}^2$

$J_1 = \frac{\pi}{32} (50)^4; J_2 = \frac{\pi}{32} (26)^4$

$U = U_1 + U_2 = \frac{T^2 L}{2GJ_1} + \frac{T^2 L}{2GJ_2}$

$\Rightarrow U = 1.5 \text{ N-mm}$

Chapter - 12
Springs

01. Ans: (b)

Sol: In the analysis of closed coiled helical spring, bending and axial force in spring are negligible.

Correct answer is (b).

02. Ans: (b)

Sol: Stiffness of Spring (S)

$S = \frac{Gd^4}{64nR^3} = \frac{G(2r)^4}{64nR^3}$

$S = \frac{Gr^4}{4nR^3}$

03. Ans: (d)

Sol: Spring stiffness, $k = \frac{Gd^4}{64R^3n}$

$\therefore k \propto d^4$

Let $d_1 = d$.

If d is doubles i.e $d_2 = 2d$.

$\therefore \frac{k_1}{k_2} = \frac{d_1^4}{d_2^4}$

$\Rightarrow \frac{k_1}{k_2} = \frac{d^4}{(2d)^4}$

$\Rightarrow k_2 = 16 k_1$



04. Ans: (a)

Sol: Spring deflection,

$$\delta = \frac{64WR^3n}{Gd^4}$$

$$\therefore \delta \propto R^3$$

$$\Rightarrow \frac{\delta_1}{\delta_2} = \frac{R_1^3}{R_2^3} = \frac{R_1^3}{\left(\frac{R_1}{2}\right)^3} = 8$$

05. Ans: (a)

Sol: For springs in series: effective stiffness is

$$\frac{1}{K_e} = \frac{1}{K_1} + \frac{1}{K_2}$$

$$\text{Therefore, } K_e = \frac{K_1 K_2}{K_1 + K_2}$$

06. Ans: (d)

Sol: Deflection of closely coiled spring

$$\delta = \frac{64R^3Wn}{Gd^4}$$

$$\therefore \delta \propto n$$

07. Ans: (d)

Sol: For springs connected in series

$$\frac{1}{K_e} = \frac{1}{S} + \frac{1}{2S} \Rightarrow K_e = \frac{2S}{3}$$

For springs connected in parallel

$$(K_e) = K_1 + K_2 = S + 2S = 3S$$

$$\therefore \frac{(K_e)_{\text{series}}}{(K_e)_{\text{parallel}}} = \frac{2S/3}{3S} = \frac{2}{9}$$

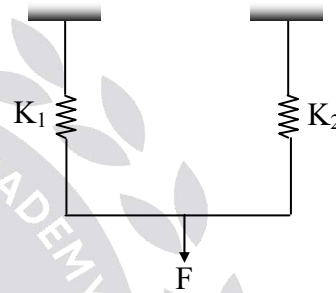
08. Ans: (d)

Sol: When one spring placed in other then those two springs will be in parallel. Hence combined stiffness is given by

$$K_e = K_A + K_B$$

09. Ans: (a)

Sol: Equivalent Load Diagram:



$$K_{eq} = K_1 + K_2 = 300 + 100$$

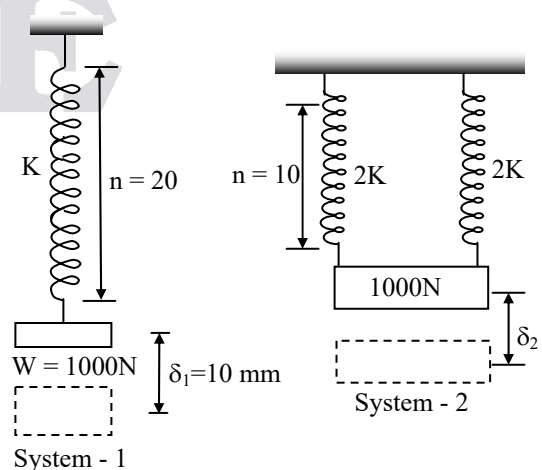
$$K_{eq} = 400 \text{ MN/m}$$

$$\delta = \frac{F}{K_{eq}} = \frac{400 \text{ kN}}{400 \times 10^3 \text{ kN/m}}$$

$$= \frac{1}{1000} \text{ m} = 1 \text{ mm}$$

10. Ans: (d)

Sol:





From system (1)

$$\delta_1 = \frac{1000}{K}$$

$$K = \frac{1000}{10} = 100 \text{ N/mm}$$

From system (2)

$$K_{eq} = 2K + 2K = 4K$$

$$K_{eq} = 4 \times 100 = 400 \text{ N/mm}$$

$$\delta_2 = \frac{W}{K_{eq}} = \frac{1000}{400} = 2.5 \text{ mm}$$

