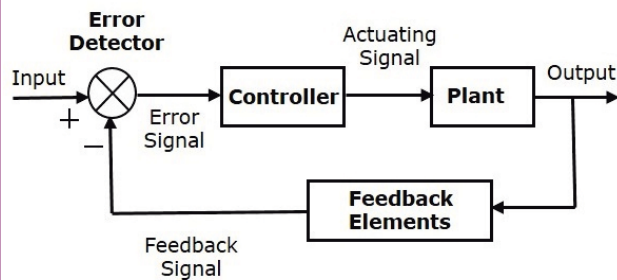




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INSTRUMENTATION ENGINEERING

CONTROL SYSTEMS & PROCESS CONTROL

Volume-1 : Study Material with Classroom Practice Questions

Control Systems & Process Control

(Solutions for Vol-1_Classroom Practice Questions)

1. Basics of Control Systems

01. Ans: (c)

Sol: $2 \frac{d^2 y(t)}{dt^2} + 3 \frac{dy(t)}{dt} + 4y(t) = r(t) + 2r(t-1)$

Apply LT on both sides

$$2s^2 Y(s) + 3sY(s) + 4Y(s) = R(s) + 2e^{-s}R(s)$$

$$Y(s)(2s^2 + 3s + 4) = R(s)(1 + 2e^{-s})$$

$$\frac{Y(s)}{R(s)} = \frac{1 + 2e^{-s}}{2s^2 + 3s + 4}$$

02. Ans: (b)

Sol: $I.R = 2.e^{-2t}u(t)$

Output response $c(t) = (1 - e^{-2t}) u(t)$

Input response $r(t) = ?$

$$T.F = \frac{C(s)}{R(s)}$$

$$T.F = L(I.R) = \frac{2}{s+2}$$

$$R(s) = \frac{C(s)}{T.F} = \frac{\frac{1}{s} - \frac{1}{s+2}}{\frac{2}{s+2}} = \frac{1}{s}$$

$$R(s) = \frac{1}{s}$$

$$r(t) = u(t)$$

03. Ans: (b)

Sol: Unit impulse response of unit-feedback control system is given

$$c(t) = t.e^{-t}$$

$$T.F = L(I.R)$$

$$= \frac{1}{(s+1)^2}$$

$$\text{Open Loop T.F} = \frac{\text{Closed Loop T.F}}{1 - \text{Closed Loop T.F}}$$

$$= \frac{\frac{1}{(s+1)^2}}{1 - \frac{1}{(s+1)^2}} = \frac{1}{s^2 + 2s}$$

04. Ans: (a)

Sol: G changes by 10%

$$\Rightarrow \frac{\Delta G}{G} \times 100 = 10\%$$

$C_1 = 10\%$ [$\because$ open loop] whose sensitivity is 100%]

%G change = 10%

$$\frac{\% \text{ of change in } M}{\% \text{ of change in } G} = \frac{1}{1 + GH}$$

$$\% \text{ of change in } M = \frac{10\%}{1 + (10)1} = 1\%$$

% change in C_2 by 1%

05.

Sol: $M = C/R$

$$\frac{C}{R} = M = \frac{GK}{1 + GH}$$

$$S_K^M = \frac{\partial M}{\partial K} \times \frac{K}{M} = 1$$

[$\because$ K is not in the loop $\Rightarrow$ sensitivity is 100%]

$$S_H^M = \frac{\partial M}{\partial H} \times \frac{H}{M} = \frac{\partial}{\partial H} \left(\frac{GK}{1 + GH} \right) \frac{H}{M}$$



$$= \left(\frac{GK(-G)}{(1+GH)^2} \right) \left[\frac{H}{GK} \right]$$

$$S_H^M = \frac{-GH}{(1+GH)}$$

06.

Sol: Given data

$$G = 2 \times 10^3, \partial G = 100$$

$$\% \text{ change in } G = \frac{\partial G}{G} \times 100 = 5\%$$

$$\% \text{ change in } M = 0.5\%$$

$$\frac{\% \text{ of change in } M}{\% \text{ of change in } G} = \frac{1}{1+GH}$$

$$\frac{0.5\%}{5\%} = \frac{1}{1+2 \times 10^3 H}$$

$$1+2 \times 10^3 H = 10$$

$$H = 4.5 \times 10^{-3}$$

07. **Ans: (b)**

Sol: $K = \frac{\text{output}}{\text{input}} = \frac{c(t)}{r(t)} = \frac{\text{mm}}{^\circ\text{C}}$

08. **Ans: (d)**

Sol: Introducing negative feedback in an amplifier results, increases bandwidth.

2. Signal Flow Graph and Block Diagram

01. **Ans: (d)**

Sol: No. of loops = 3

$$\text{Loop1: } -G_1 G_3 G_4 H_1 H_2 H_3$$

$$\text{Loop2: } -G_3 G_4 H_1 H_2$$

$$\text{Loop3: } -G_4 H_1$$

No. of Forward paths = 3

$$\text{Forward Path1: } G_1 G_3 G_4$$

$$\text{Forward Path 2: } G_2 G_3 G_4$$

$$\text{Forward Path 3: } G_2 G_4$$

$$= \frac{G_1 G_3 G_4 + G_2 G_3 G_4 + G_2 G_4}{1 + G_1 G_3 G_4 H_1 H_2 H_3 + G_3 G_4 H_1 H_2 + G_4 H_1}$$

02. **Ans: (a)**

Sol: Number of forward paths = 2

Number of loops = 3

$$\frac{Y(s)}{R(s)} = \frac{\frac{1}{s} \times \frac{1}{s} \times \frac{1}{s} [1-0] + \frac{1}{s}}{1 - \left[\frac{1}{s} \times (-1) \left(\frac{1}{s} \right) (-1) + \frac{1}{s} \times \frac{1}{s} (-1) + \left(\frac{1}{s} \times \frac{1}{s} (-1) \right) \right]}$$

$$= \frac{\frac{1}{s^3} + \frac{1}{s}}{1 - \left[\frac{1}{s^2} - \frac{1}{s^2} - \frac{1}{s^2} \right]} = \frac{\frac{1+s^2}{s^3}}{1 + \frac{1}{s^2}} = \frac{1+s^2}{s^3} \times \frac{s^2}{s^2+1} = \frac{1+s^2}{s(s^2+1)}$$

03.

Sol: Number of forward paths = 2

Number of loops = 5,

Two non touching loops=4

$$TF = \frac{24[1-(-0.5)] + 10[1-(-3)]}{1 - [-24-3-4+(5 \times 2 \times (-1)+(-0.5))] + [30+1.5+2] + \left(\left(\frac{-1}{2} \right) \times (-24) \right)}$$

$$= \frac{76}{88} = \frac{19}{22}$$

04.

Sol: Number of forward paths = 2

Number of loops = 5

$$T.F = \frac{G_1 G_2 G_3 + G_1 G_4}{1 + G_2 G_3 H_2 + G_1 G_2 H_1 + G_1 G_2 G_3 + G_4 H_2 + G_1 G_4}$$



05. Ans: (c)

Sol: From the network

$$V_o(s) = \frac{1}{sC} I(s) \quad \text{.....(1)}$$

$$-V_i(s) + RI(s) + V_o(s) = 0$$

$$I(s) = \frac{1}{R} V_i(s) + \left(\frac{-1}{R} \right) V_o(s) \quad \text{.....(2)}$$

From SFG

$$V_o(s) = x \cdot I(s) \quad \text{.....(3)}$$

$$I(s) = \frac{1}{R} V_i(s) + y V_o(s) \quad \text{.....(4)}$$

From equ(1) and (3)

$$x = \frac{1}{sC}$$

From equ(2) and (4)

$$y = -\frac{1}{R}$$

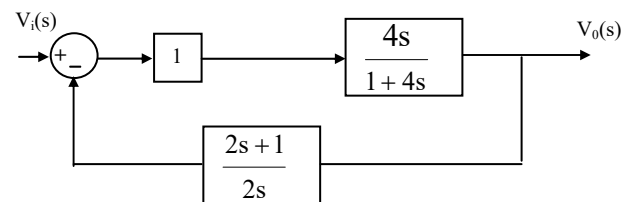
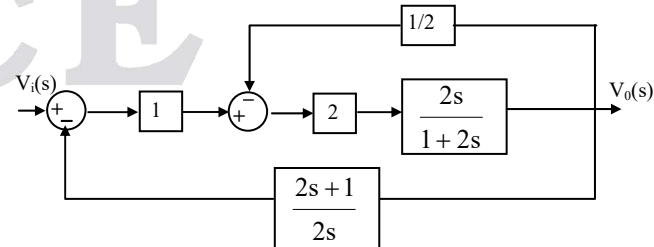
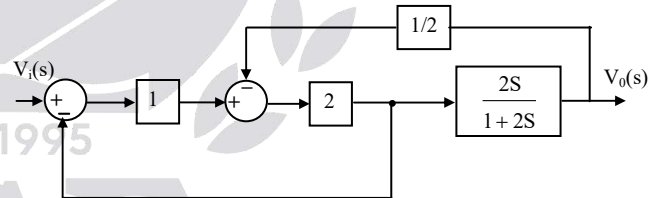
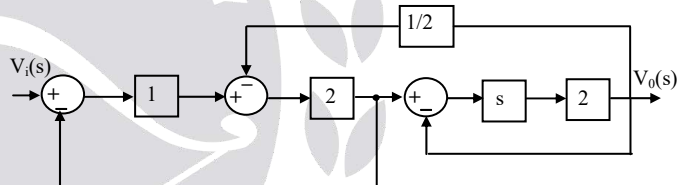
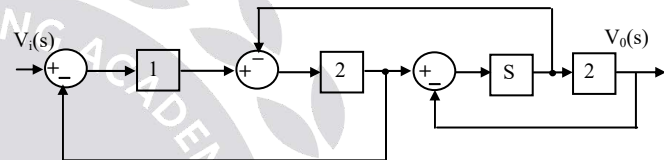
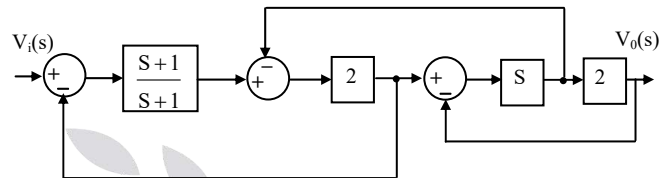
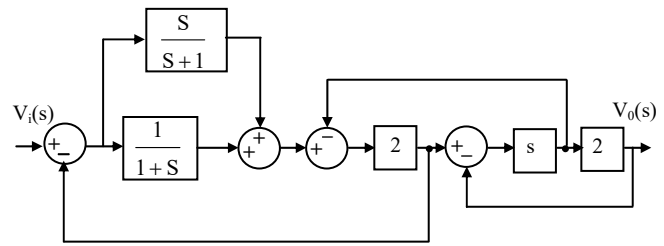
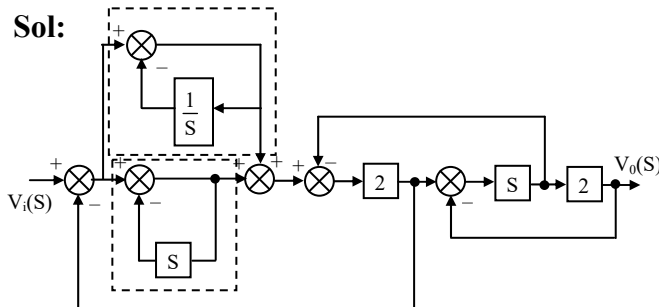
06. Ans: (a)

Sol: Use gain formula

$$\begin{aligned} \text{transfer function} &= \frac{G(s)}{1 - \left(G(s) \frac{1}{G(s)} + G(s) \right)} \\ &= \frac{G(s)}{1 - 1 - G(s)} = -1 \end{aligned}$$

07.

Sol:





$$\Rightarrow \frac{V_o(s)}{V_i(s)} = \frac{\frac{4s}{1+4s}}{1 + \frac{2(2s+1)}{1+4s}} = \frac{4s}{8s+3}$$

08.

Sol: Apply Mason's Gain formula

$$M = \frac{Y_{out}}{Y_{in}} = \frac{\sum_{k=1}^N M_k \Delta_k}{\Delta}$$

No. of forward paths = 2

First forward path gain = $G_1 G_2 G_3 G_4$

Second forward path gain = $G_5 G_6 G_7 G_8$

No. of loops = 4

First loop gain = $-G_2 H_2$

Second loop gain = $-G_6 H_6$

Third loop gain = $-G_3 H_3$

Fourth loop gain = $-G_7 H_7$

Non touching loops = 4

Loop gains $\rightarrow G_2 H_2 G_6 H_6$

$\rightarrow G_2 H_2 G_7 H_7$

$\rightarrow G_6 H_6 G_7 H_7$

$\rightarrow G_2 H_2 G_3 H_3$

Transfer function =

$$\frac{G_1 G_2 G_3 G_4 (1 + G_6 H_6 + G_7 H_7) + G_5 G_6 G_7 G_8 (1 + G_2 H_2 + G_3 H_3)}{1 + G_2 H_2 + G_3 H_3 + G_6 H_6 + G_7 H_7 + G_2 H_2 G_6 H_6 + G_2 H_2 G_7 H_7 + G_3 H_3 G_6 H_6 + G_3 H_3 G_7 H_7}$$

3. Time Response Analysis

01. **Ans: (a)**

Sol: $\frac{C(s)}{R(s)} = \frac{1}{1+sT}$, $R(s) = \frac{8}{s}$

$$C(s) = \frac{8}{s(1+sT)} \Rightarrow c(t) = 8(1 - e^{-t/T})$$

$$3.6 = 8 \left(1 - e^{\frac{-0.32}{T}} \right)$$

$$0.45 = 1 - e^{\frac{-0.32}{T}}$$

$$0.55 = e^{\frac{-0.32}{T}}$$

$$-0.59 = \frac{-0.32}{T}$$

$$T = 0.535 \text{ sec}$$

02. **Ans: (c)**

Sol: $\cos \phi = \xi$

$$\cos 60 = 0.5$$

$$\cos 45 = 0.707$$

$$\text{Poles left side } 0.5 \leq \xi \leq 0.707$$

$$\text{Poles right side } -0.707 \leq \xi \leq -0.5$$

$$\therefore 0.5 \leq |\xi| \leq 0.707$$

$$3 \text{ rad/s} \leq \omega_n \leq 5 \text{ rad/s}$$

03. **Ans: (c)**

Sol: For R-L-C circuit:

$$T.F = \frac{V_o(s)}{V_i(s)}$$

$$V_o(s) = \frac{1}{Cs} I(s)$$



$$= \frac{1}{C_s} \frac{V_i(s)}{R + Ls + \frac{1}{C_s}}$$

$$\text{T.F} = \frac{V_o(s)}{V_i(s)} = \frac{1}{RCs + LCs^2 + 1}$$

$$= \frac{\frac{1}{LC}}{s^2 + \frac{R}{L}s + \frac{1}{LC}}$$

$$s^2 + \frac{R}{L}s + \frac{1}{LC} = 0$$

$$s^2 + 2\xi\omega_n s + \omega_n^2 = 0$$

$$\omega_n = \frac{1}{\sqrt{LC}} \quad 2\xi\omega_n = \frac{R}{L}$$

$$\xi = \frac{R}{2} \sqrt{\frac{C}{L}}$$

$$\xi = \frac{10}{2} \sqrt{\frac{10 \times 10^{-6}}{1 \times 10^{-3}}} = 0.5$$

$$\text{M.P} = e^{-\frac{\xi\pi}{\sqrt{1-\xi^2}}}$$

$$= 16.3\% \approx 16\%$$

04. Ans: (b)

Sol: TF = $\frac{8/s(s+2)}{1 - \left(\frac{-8as}{s(s+2)} - \frac{8}{s(s+2)} \right)}$

$$= \frac{8}{s(s+2) + 8as + 8}$$

$$= \frac{8}{s^2 + 2s + 8as + 8}$$

$$= \frac{8}{s^2 + (2+8a)s + 8}$$

$$\omega_n^2 = 8 \Rightarrow \omega_n = 2\sqrt{2}$$

$$2\xi\omega_n = 2 + 8a$$

$$\xi = \frac{1+4a}{2\sqrt{2}}$$

$$\frac{1}{\sqrt{2}} = \frac{1+4a}{2\sqrt{2}} \Rightarrow a = 0.25$$

05. Ans: 4 sec

Sol: T.F = $\frac{100}{(s+1)(s+100)}$

$$= \frac{100}{s^2 + 101s + 100}$$

$$\omega_n^2 = 100$$

$$\omega_n = 10$$

$$2\xi\omega_n = 101$$

$$\xi = \frac{101}{20}$$

$\xi > 1 \rightarrow$ system is over damped i.e., roots are real & unequal.

Using dominate pole concept,

$$\text{T.F} = \frac{100}{100(s+1)} = \frac{1}{s+1}, \text{ Here } \tau = 1 \text{ sec}$$

$$\therefore \text{setting time for 2\% criterion} = 4\tau$$

$$= 4 \text{ sec}$$

06. $M_p = \frac{C(t_p) - C(\infty)}{C(\infty)}$

$$= \frac{1.254 - 1.04}{1.04} = 0.2$$

$$\xi = \sqrt{\frac{(\ln M_p)^2}{(\ln M_p)^2 + \pi^2}}$$

$$M_p = 0.2 ; \xi = 0.46$$

07. Ans: (d)

Sol: Given data: $\omega_n = 2, \zeta = 0.5$



Steady state gain = 1

$$\text{OLTF} = \frac{K_1}{s^2 + as + 2} \text{ and } H(s) = K_2$$

$$\text{CLTF} = \frac{G(s)}{1+G(s)}$$

$$\frac{C(s)}{R(s)} = \frac{K_1}{s^2 + as + 2 + K_1 K_2}$$

DC or steady state gain from the TF

$$\frac{K_1}{2 + K_1 K_2} = 1$$

$$K_1(1 - K_2) = 2 \quad \dots\dots\dots (1)$$

$$\text{CE is } s^2 + as + 2 + K_1 K_2 = 0$$

$$\omega_n = \sqrt{2 + K_1 K_2} = 2$$

$$4 = (2 + K_1 K_2)$$

$$K_1 K_2 = 2 \quad \dots\dots\dots (2)$$

Solving equations (1) & (2) we get

$$K_1 = 4, \quad K_2 = 0.5$$

$$2\zeta \omega_n = a$$

$$2 \times \frac{1}{2} \times 2 = a$$

$$a = 2$$

08. Ans: A – T, B – S, C- P, D – R, E – Q

Sol:

(A) If the poles are real & left side of s-plane, the step response approaches a steady state value without oscillations.

(B) If the poles are complex & left side of s-plane, the step response approaches a steady state value with the damped oscillations.

(C) If poles are non-repeated on the $j\omega$ axis, the step response will have fixed amplitude oscillations.

(D) If the poles are complex & right side of s-plane, response goes to ' ∞ ' with damped oscillations.

(E) If the poles are real & right side of s-plane, the step response goes to ' ∞ ' without any oscillations.

09. Ans: (c)

Sol: If $R \uparrow$ damping $\uparrow$

$$\Rightarrow \xi = \frac{R}{2} \sqrt{\frac{C}{L}}$$

(i) If $R \uparrow$, steady state voltage across C will be reduced (wrong)

(Since steady state value does not depend on ξ)

If $\xi \uparrow$, $C(\infty)$ = remain same

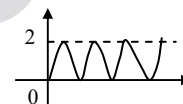
(ii) If $\xi \uparrow$, $\omega_d \downarrow$ ($\omega_d = \omega_n \sqrt{1 - \xi^2}$)

(iii) If $\xi \downarrow$, $t_s \uparrow \Rightarrow 3^{\text{rd}}$

Statement is false

(iv) If $\xi = 0$

True



$\Rightarrow 2$ and 4 are correct

10.

Sol: (i) Unstable system

$$\therefore \text{error} = \infty$$

$$(ii) G(s) = \frac{10(s+1)}{s^2}$$

$$\text{Step} \rightarrow R(s) = \frac{1}{s}$$

$$k_p = \infty$$

$$e_{ss} = \frac{A}{1 + k_p} = \frac{1}{1 + \infty} = 0$$



Parabolic $\Rightarrow k_a = 10$

$$e_{ss} = \frac{1}{10} = 0.1$$

11.

Sol: $G(s) = 10/s^2$ (marginally stable system)

$\therefore$ Error can't be determined

12.

Sol: $e_{ss} = \frac{1}{11}$, $R(s) = \frac{1}{s}$

$$e_{ss} = \frac{A}{1+k_p} = \frac{1}{1+k_p} = \frac{1}{11} = \frac{1}{1+10}$$

$$k_p = \lim_{s \rightarrow 0} s G(s)$$

$$10 = \lim_{s \rightarrow 0} s G(s)$$

$$k = 10$$

$$R(s) = \frac{1}{s^2} \text{ (ramp)}$$

$$e_{ss} = \frac{A}{k_v} = \frac{1}{k_v} = \frac{1}{10}$$

(System is increased by 1)

$$\Rightarrow e_{ss} = 0.1$$

13. **Ans: (a)**

Sol: $T(s) = \frac{(s-2)}{(s-1)(s+2)^2}$ (unstable system)

14. **Ans: (b)**

Sol: Given data: $r(t) = 400tu(t)$ rad/sec

Steady state error $= 10^\circ$

$$\text{i.e., } e_{ss} = \frac{\pi}{180^\circ} (10^\circ) \text{ radians}$$

$$G(s) = \frac{20K}{s(1+0.1s)} \text{ and } H(s) = 1$$

$$r(t) = 400tu(t) \Rightarrow 400/s^2$$

$$\text{Error } (e_{ss}) = \frac{A}{K_v} = \frac{400}{K_v}$$

$$K_v = \lim_{s \rightarrow 0} s G(s)$$

$$K_v = \lim_{s \rightarrow 0} s \frac{20K}{s(1+0.1s)}$$

$$K_v = 20K$$

$$e_{ss} = \frac{400}{20K}$$

$$e_{ss} = \frac{20}{K} = \frac{\pi}{18}$$

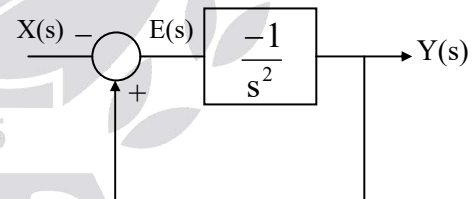
$$K = 114.5$$

15. **Ans: (d)**

Sol: $\frac{d^2 y}{dt^2} = -e(t)$

$$s^2 Y(s) = -E(s)$$

$$x(t) = t u(t) \Rightarrow X(s) = \frac{1}{s^2}$$



$$Y(s) = \frac{-1}{s^2} E(s)$$

$$\frac{Y(s)}{E(s)} = \frac{-1}{s^2}$$

$$\frac{E(s)}{X(s)} = \frac{-1}{1 + \frac{1}{s^2}}$$

$$E(s) = \frac{-s^2}{1 + s^2} X(s)$$



$$= \frac{-s^2}{1+s^2} \times \frac{1}{s^2} = \frac{-1}{1+s^2}$$

$$= L^{-1} \left[\frac{-1}{1+s^2} \right] = -\sin t$$

16. Ans: (a)

Sol: $e_{ss} = 0.1$ for step input

For pulse input = 10

time = 1 sec

error is function of input

$t \rightarrow \infty$ input = 0

$\therefore$ Error = zero

17. Ans: (c)

Sol: $\frac{C(s)}{R(s)} = \frac{100}{(s+1)(s+5)}$

$$1 + \frac{100 \times 0.2}{(s+1)(s+5)}$$

$$= \frac{100}{(s+1)(s+5) + 20}$$

$$= \frac{100}{s^2 + 6s + 5 + 20}$$

$$= \frac{100}{s^2 + 6s + 25}$$

$$\omega_n^2 = 25, \omega_n = 5$$

$$2\xi\omega_n = 6$$

$$\xi = \frac{6}{10} = \frac{3}{5}$$

$$\omega_d = \omega_n \sqrt{1 - \xi^2}$$

$$= 5 \sqrt{1 - \left(\frac{3}{5}\right)^2}$$

$$= 5 \times \frac{4}{5} = 4 \text{ rad/sec}$$

18. Ans: (c)

Sol: $f(t) = \frac{Md^2x}{dt^2} + B \frac{dx}{dt} + Kx(t)$

Applying Laplace transform on both sides,
with zero initial conditions

$$F(s) = Ms^2X(s) + BsX(s) + KX(s)$$

$$\frac{X(s)}{F(s)} = \frac{1}{Ms^2 + Bs + K}$$

Characteristic equation is $Ms^2 + Bs + K = 0$

$$s^2 + \frac{B}{M}s + \frac{K}{M} = 0$$

Compare with $s^2 + 2\xi\omega_n s + \omega_n^2 = 0$

$$2\xi\omega_n = \frac{B}{M}$$

$$\xi = \frac{B}{2\sqrt{MK}} \quad \omega_n = \sqrt{\frac{K}{M}}$$

$$\text{Time constant } T = \frac{1}{\xi\omega_n}$$

$$= \frac{1}{B} \times 2M$$

$$T = \frac{2M}{B}$$

Hence, statements 2 & 3 are correct

19. Ans: (c)

Sol: type 1 system has a infinite positional error constant.

20. Ans: (a)

Sol: Given $G(s) = \frac{1}{s(1+s)(s+2)}, H(s) = 1$.

It is type-I system

$$\text{Positional error constant } k_p = \lim_{s \rightarrow 0} G(s)H(s)$$



$$k_p = \lim_{s \rightarrow 0} \frac{1}{s(1+s)(s+2)}$$

$$= \infty$$

Steady state error due to step input

$$= \frac{1}{1+k_p} = 0$$

21.

Sol: Open loop T/F $G(s) = \frac{A}{s(s+P)}$

$$\text{C.L T/F} = \frac{A}{s^2 + SP + A}$$

$$\omega_n = \sqrt{A}$$

$$\text{Setting time} = 4/\xi\omega_n = 4$$

$$2\xi\omega_n = P \quad \therefore \frac{4}{P/2} = 4$$

$$\xi\omega_n = P/2 \quad \Rightarrow P = \frac{8}{4} = 2$$

$$e^{\frac{-\pi\xi}{\sqrt{1-\xi^2}}} = 0.1 \Rightarrow \frac{\pi\xi}{\sqrt{1-\xi^2}} = \ln 10$$

$$= 2.3$$

$$\Rightarrow \frac{\xi^2}{1-\xi^2} = 0.5373$$

$$\Rightarrow 1.5373 \xi^2 = 0.5373$$

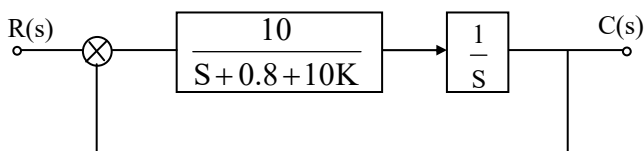
$$\xi = 0.59$$

$$\xi\omega_n = 1$$

$$\Rightarrow \omega_n = 1.694 \Rightarrow A = \omega_n^2 = 2.87$$

22.

Sol:



$$\frac{C(s)}{R(s)} = \frac{10}{s(s+0.8+10K)+10}$$

$$= \frac{10}{s^2 + s(0.8+10K)+10}$$

$$\omega_n = \sqrt{10} \quad 2\xi\omega_n = 0.8 + 10K$$

$$\Rightarrow 2 \times \frac{1}{2} \times \sqrt{10} = 0.8 + 10K$$

$$\Rightarrow K = 0.236$$

$$t_r = \frac{\pi - \phi}{\omega_d} = \frac{\pi - \cos^{-1}(\xi)}{\omega_n \sqrt{1-\xi^2}}$$

$$= \frac{\pi - \pi/3}{2.88} = 0.74 \text{ sec}$$

$$t_p = \frac{\pi}{\omega_d} = 1.1 \text{ sec}$$

$$\%M_p = e^{\frac{-\pi\xi}{\sqrt{1-\xi^2}}} = 0.163 \times 100 = 16.3\%$$

$$t_s \text{ (for 2\%)} = \frac{4}{\xi\omega_n} = \frac{4}{0.5 \times \sqrt{10}} = 2.53 \text{ sec}$$

4. Stability

01.

Sol: CE = $s^5 + 4s^4 + 8s^3 + 8s^2 + 7s + 4 = 0$

s^5	1	8	7	
s^4	4(1)	8(2)	4(1)	
s^3	6(1)	6(1)	0	
s^2	1	1	0	→ Row of AE
s^1	0(2)	0	0	→ Row of zero
s^0	1			



No. of AE roots = 2	No. of CE roots = 5
No. of sign changes	No. of sign changes
Below AE = 0	in 1 st column = 0
No. of RHP = 0	∴ No. of RHP = 0
No. of LHP = 0	No. of jωp = 2
No. of jωp = 2	⇒ No. of LHP = 3

System is marginally stable.

(ii) $s^2 + 1 = 0$

$s = \pm 1j = \pm j\omega_n$

$\omega_n = 1 \text{ rad/sec}$

Oscillating frequency $\omega_n = 1 \text{ rad/sec}$

02.

Sol: (i) $s^5 + s^4 + s^3 + s^2 + s + 1 = 0$

$+s^5$	1	1	1
$+s^4$	1	1	1
$+s^3$	0(2)	0(1)	0
$+s^2$	$\frac{1}{2}$	1	
$(1) - s^1$	-3	0	
$(2) + s^0$	1		

AE (1) $= s^4 + s^2 + 1 = 0$

$\frac{d(AE)}{ds} = 4s^3 + 2s = 0$

$\Rightarrow 2s^3 + s = 0$

AE	CE
No. of sign changes below AE = 2	No. of sign changes in 1 st column = 2
No. of AE roots = 4	No. of CE roots = 5
No. of RHP = 2	No. of RHP = 2
No. of LHP = 2	No. of LHP = 3
No. of jωp = 0	No. of jωp = 0

System is unstable

(ii) $s^6 + 2s^5 + 2s^4 + 0s^3 - s^2 - 2s - 2 = 0$

s^6	1	2	-1	-2
s^5	2(1)	0	-2(-1)	0
s^4	2(1)	+0	-2(-1)	0
s^3	0(4)	0	0	0
s^2	0(ε)	-1	0	0
s^1	4/ε			
$-s^0$	-1			

AE $= s^4 - 1 = 0$

$\frac{dAE}{ds} = 4s^3 + 0 = 0$

CE	AE
No. of CE roots = 6	No. of AE roots = 4
No. of sign changes in the 1 st column = 1	No. of sign changes below AE = 1
No. of RHP = 1	No. of RHP = 1
No. of LHP = 3	No. of jωp = 2
No. of jωp = 2	No. of LHP = 1



03.

Sol: CE = $s^3 + 20s^2 + 16s + 16K = 0$

$$\begin{array}{r|rr} s^3 & 1 & 16 \\ s^2 & 20 & 16K \\ s^1 & \frac{20(16) - 16K}{20} & 0 \\ s^0 & 16K & \end{array}$$

- (i) For stability $\frac{20(16) - 16K}{20} > 0$
 $\Rightarrow 20(16) - 16K > 0$
 $\Rightarrow K < 20$ and $16K > 0 \Rightarrow K > 0$
 Range of K for stability $0 < K < 20$

- (ii) For the system to oscillate with ω_n it must be marginally stable
 i.e., s^1 row should be 0
 s^2 row should be AE

$$\therefore \text{A.E roots} = \pm j\omega_n$$

$$\begin{aligned} \therefore s^1 \text{ row} &\Rightarrow 20(16) - 16K = 0 \\ &\Rightarrow K = 20 \\ \text{AE is } 20s^2 + 16K &= 0 \\ 20s^2 + 16(20) &= 0 \\ &\Rightarrow s = \pm j4 \\ \omega_n &= 4 \text{ rad/sec} \end{aligned}$$

04.

Sol: CE = $1 + \frac{K(s+1)}{s^3 + as^2 + 2s + 1} = 0$

$$\begin{aligned} s^3 + as^2 + (K+2)s + K+1 &= 0 \\ s^3 + as^2 + (K+2)s + (K+1) &= 0 \end{aligned}$$

$$\begin{array}{r|rr} s^3 & 1 & K+2 \\ s^2 & a & K+1 \\ s^1 & \frac{a(K+2) - (K+1)}{a} & 0 \\ s^0 & K+1 & \end{array}$$

Given,

$$\begin{aligned} \omega_n &= 2 \\ \Rightarrow s^1 \text{ row} &= 0 \\ s^2 \text{ row is A.E} \\ a(K+2) - (K+1) &= 0 \\ a &= \frac{K+1}{K+2} \\ \text{AE} = as^2 + K+1 &= 0 \\ &= \frac{K+1}{K+2} s^2 + K+1 = 0 \\ (K+1) \left(\frac{s^2}{K+2} + 1 \right) &= 0 \\ s^2 + K+2 &= 0 \\ s &= \pm j\sqrt{K+2} \\ \omega_n &= \sqrt{K+2} = 2 \\ K &= 2 \\ a &= \frac{K+1}{K+2} = \frac{3}{4} = 0.75 \end{aligned}$$



05.

Sol: $s^3 + ks^2 + 9s + 18$

s^3	1	9
s^2	K	18
s^1	$\frac{9K-18}{K}$	0
s^0	18	

Given that system is marginally stable,

Hence

$$s^1 \text{ row} = 0$$

$$\frac{9K-18}{K} = 0$$

$$9K = 18 \Rightarrow K = 2$$

$$\text{A.E is } 9s^2 + 18 = 0$$

$$Ks^2 + 18 = 0,$$

$$2s^2 + 18 = 0$$

$$2s^2 = -18$$

$$s = \pm j3$$

$$\therefore \omega_n = 3 \text{ rad/sec.}$$

06. **Ans: (d)**

Sol: Given transfer function $G(s) = \frac{k}{(s^2 + 1)^2}$

Characteristic equation $1 - G(s).H(s) = 0$

$$1 - \frac{k}{(s^2 + 1)^2} = 0$$

$$s^4 + 2s^2 + 1 - k = 0 \dots (1)$$

RH criteria

s^4	1	2	$1-K$
s^3	4	4	
s^2	1	$1-K$	
s^1	$4K$		
s^0	$1-K$		

$$AE = s^4 + 2s^2 + 1 - K$$

$$\frac{d}{ds}(AE) = 4s^3 + 4s$$

$1-K > 0$ no poles are on RHS plane and LHS plane.

All poles are on $j\omega$ - axis

$\therefore 0 < K < 1$ system marginally stable

07. **Ans: (d)**

Sol: Assertion: FALSE

Let the TF = s. "s" is the differentiator

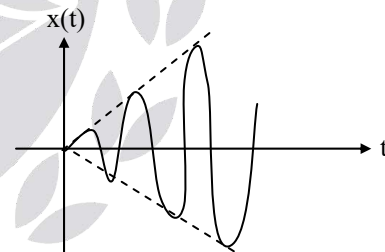
Impulse response $L^{-1}[TF] = L^{-1}[s] = \delta'(t)$

$$\lim_{t \rightarrow \infty} \delta'(t) = 0$$

$\therefore$ It is BIBO stable

Reason: True

$$x(t) = t \sin t$$



$$\lim_{t \rightarrow \infty} x(t) = \lim_{t \rightarrow \infty} t \sin t \text{ is unbounded}$$

08. **Ans: (a)**

Sol: Assertion: TRUE

If feedback is not properly utilized the closed loop system may become unstable.

Reason: True

Feedback changes the location of poles

$$\text{Let } G(s) = \frac{-2}{s+1} \quad H(s) = 1$$



Open loop pole $s = -1$ (stable)

$$CLTF = \frac{\frac{-2}{s+1}}{1 + \frac{-2}{s+1}} = \frac{-2}{s-1}$$

Closed loop pole is at $s = 1$ (unstable)

$\therefore$ After applying the feedback no more system is open loop. It becomes closed loop system. Hence poles are affected.

5. Root Locus Diagram

01. Ans: (a)

Sol: $s_1 = -1 + j\sqrt{3}$

$s_2 = -3 - j\sqrt{3}$

$$G(s).H(s) = \frac{K}{(s+2)^3}$$

$s_1 = -1 + j\sqrt{3}$

$$G(s).H(s) = \frac{K}{(-1 + j\sqrt{3} + 2)^3}$$

$$= \frac{K}{(1 + j\sqrt{3})^3}$$

$$= -3 \tan^{-1}(\sqrt{3})$$

$$= -180^\circ$$

It is odd multiples of 180° , Hence s_1 lies on Root locus

$s_2 = -3 - j\sqrt{3}$

$$G(s).H(s) = \frac{K}{(-3 - j\sqrt{3} + 2)^3}$$

$$= \frac{K}{(-1 - j\sqrt{3})^3}$$

$$= -3 [180^\circ + 60^\circ] = -720^\circ$$

It is not odd multiples of 180° , Hence s_2 is not lies on Root locus.

02. Ans: (a)

Sol: Over damped – roots are real & unequal

$$\Rightarrow 0 < k < 4$$

(b) $k = 4$ roots are real & equal

$$\Rightarrow \text{Critically damped } \xi = 1$$

(c) $k > 4 \Rightarrow$ roots are complex

$$0 < \xi < 1 \Rightarrow \text{under damped}$$

03. Ans: (a)

Sol: Asymptotes meeting point is nothing but centroid

$$\text{centroid } \sigma = \frac{\sum \text{poles} - \sum \text{zeros}}{p - z}$$

$$= \frac{-3 - 0}{3 - 0} = -1$$

$$\text{centroid} = (-1, 0)$$

04. Ans: (b)

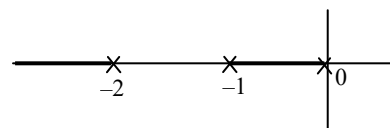
Sol: Break point = $\frac{dK}{ds} = 0$

$$\frac{d}{ds} (G_1(s).H_1(s)) = 0$$

$$\frac{d}{ds} [s(s+1)(s+2)] = 0$$

$$3s^2 + 6s + 2 = 0$$

$$s = -0.422, -1.57$$





But $s = -1.57$ do not lie on root locus

So, $s = -0.422$ is valid break point.

Point of intersection wrt $j\omega$ axis

$$s^3 + 3s^2 + 2s + k = 0$$

$$\begin{array}{r|rr} s^3 & 1 & 2 \\ s^2 & 3 & k \\ s^1 & 6-k & 0 \\ s^0 & 3 & k \end{array}$$

As s^1 Row = 0

$$k = 6$$

$$3s^2 + 6 = 0$$

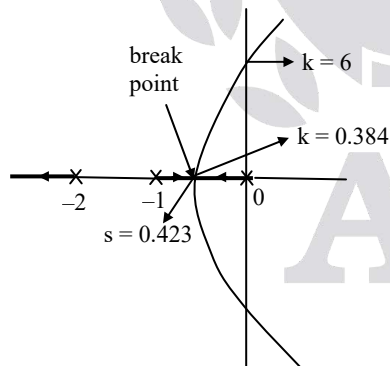
$$s^2 = -2$$

$$s = \pm j\sqrt{2}$$

point of inter section: $s = \pm j\sqrt{2}$

05. Ans: (b)

Sol:



$$\frac{K}{s(s+1)(s+2)}$$

substitute $s = -0.423$ and apply the magnitude criteria.

$$\left| \frac{K}{(-0.423)(-0.423+1)(-0.423+2)} \right| = 1$$

$$K = 0.354$$

when the roots are complex conjugate then the system response is under damped.

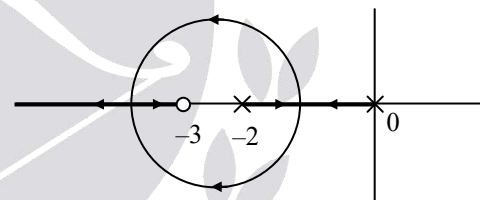
From $K > 0.384$ to $K < 6$ roots are complex conjugate then system to be under damped the values of k is $0.384 < K < 6$.

06. Ans: (c)

Sol: If the roots are lies on the real axis then system exhibits the non-oscillatory response. from $K \geq 0$ to $K \leq 0.384$ roots lies on the real axis. Hence for $0 \leq K \leq 0.384$ system exhibits the non-oscillatory response.

07. Ans: (a)

Sol:



$$\frac{d}{ds} [G(s).H(s)] = \frac{d}{ds} \left[\frac{k(s+3)}{s(s+2)} \right]$$

$$s^2 + 6s + 6 = 0$$

break points $-1.27, -4.73$

$$\text{radius} = \frac{4.73 - 1.27}{2} = 1.73$$

center = $(-3, 0)$

08. Ans: (c)

Sol: $G(s).H(s) = \frac{K(s+3)}{s(s+2)}$



$$k|_{s=-4} = \left| \frac{(-4)(-4+2)}{(-4+3)} \right|$$

$$= \left| \frac{(-4)(-2)}{(-1)} \right| = 8$$

09. Ans: (a)

Sol: $s^2 - 4s + 8 = 0 \Rightarrow s = 2 \pm 2j$ are two zeroes

$s^2 + 4s + 8 = 0 \Rightarrow s = -2 \pm 2j$ are two poles

$$\phi_A = 180 - \angle GH|_{s=2+2j}$$

$$GH = \frac{k[s - (2 + 2j)][s - (2 - 2j)]}{[s - (-2 + 2j)][s - (-2 - 2j)]}$$

$$\angle GH|_{s=2+2j} = \frac{\angle k \angle 4j}{\angle 4 \angle 4 + 4j}$$

$$= 90^\circ - 45^\circ = 45^\circ$$

$$\phi_A = 180^\circ - 45^\circ = \pm 135^\circ$$

10. Ans: (b)

Sol: $s^2 - 4s + 8 = 0 \Rightarrow s = 2 \pm 2j$ are two zeroes

$s^2 + 4s + 8 = 0 \Rightarrow s = -2 \pm 2j$ are two poles

$$\phi_d = 180^\circ + \angle GH|_{s=-2+2j}$$

$$\angle GH|_{s=-2+2j} = \angle \frac{k[s - (2 + 2j)][s - (2 - 2j)]}{[s - (-2 + 2j)][s - (-2 - 2j)]}|_{s=-2+2j}$$

$$= \frac{\angle k(-4)(-4+4j)}{\angle 4j}$$

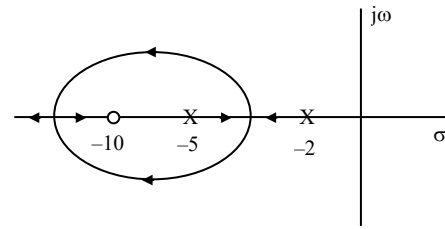
$$= 180^\circ + 180^\circ - 45^\circ - 90^\circ = 225^\circ$$

$$\phi_d = 180^\circ + 225^\circ = 405^\circ$$

$$\therefore \phi_d = \pm 45^\circ$$

11. Ans: (d)

Sol: Poles $s = -2, -5$; Zero $s = -10$



$\therefore$ Breakaway point exist between -2 and -5

12.

Sol: Refer Pg No: 79, Vol-1 Ex: 7

6. Frequency Response Analysis

01. Ans: (c)

$$\text{Sol: } G(s).H(s) = \frac{100}{s(s+4)(s+16)}$$

Phase crossover frequency (ω_{pc}):

$$\angle G(j\omega).H(j\omega)/\omega = \omega_{pc} = -180^\circ$$

$$-90^\circ - \tan^{-1}(\omega_{pc}/4) - \tan^{-1}(\omega_{pc}/16) = -180^\circ$$

$$-\tan^{-1}(\omega_{pc}/4) - \tan^{-1}(\omega_{pc}/16) = -90^\circ$$

$$\tan[\tan^{-1}(\omega_{pc}/4) + \tan^{-1}(\omega_{pc}/16)] = \tan(90^\circ)$$

$$\frac{\frac{\omega_{pc}}{4} + \frac{\omega_{pc}}{16}}{1 - \frac{\omega_{pc}}{4} \cdot \frac{\omega_{pc}}{16}} = \frac{1}{0}$$

$$\omega_{pc}^2 = 16 \times 4 \Rightarrow \omega_{pc} = 8 \text{ rad/sec}$$

02. Ans: (d)

$$\text{Sol: } G(s).H(s) = \frac{100}{s(s+2)(s+16)}$$

$$\text{Gain margin (G.M)} = \frac{1}{|G(j\omega)H(j\omega)|_{\omega=\omega_{pc}}}$$



$$\begin{aligned} |G(j\omega).H(j\omega)|_{\omega=\omega_{pc}} &= \frac{100}{\omega_{pc}\sqrt{\omega_{pc}^2+16}\sqrt{\omega_{pc}^2+16^2}} \\ &= \frac{5}{64} \\ G.M &= \frac{64}{5} = 12.8 \end{aligned}$$

03. Ans: (c)

Sol: $G(s).H(s) = \frac{2e^{-0.5s}}{(s+1)}$

gain crossover frequency,

$$\omega_{gc} = |G(j\omega).H(j\omega)|_{\omega=\omega_{gc}} = 1$$

$$\frac{2}{\sqrt{\omega_{gc}^2+1}} = 1$$

$$\omega_{gc}^2 + 1 = 4 \Rightarrow \omega_{gc} = \sqrt{3} \text{ rad/sec}$$

04. Ans: (b)

Sol: $\omega_{gc} = \sqrt{3} \text{ rad/sec}$

$$P.M = 180^\circ + \angle G(j\omega).H(j\omega)/\omega = \omega_{gc}$$

$$\begin{aligned} \angle G(j\omega).H(j\omega)/\omega=\omega_{gc} &= -0.5 \omega_{gc} - \tan^{-1}(\omega_{gc}) \\ &= -109.62^\circ \end{aligned}$$

$$P.M = 70.39^\circ$$

05. Ans: (a)

Sol: $M_r = 2.5 = \frac{1}{2\xi\sqrt{1-\xi^2}}$

$$2\xi\sqrt{1-\xi^2} = \frac{1}{2.5}$$

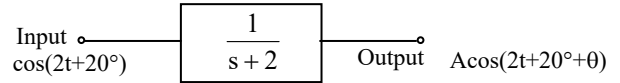
$$\xi^4 - \xi^2 + 0.04 = 0$$

$$\xi^2 = 0.958 \quad \xi^2 = 0.0417$$

$$\xi = 0.204 \quad (M_r > 1)$$

06. Ans: (a)

Sol: Closed loop T.F = $\frac{1}{s+2}$



$$A = \frac{1}{\sqrt{\omega^2+4}} = \frac{1}{\sqrt{4+4}} = \frac{1}{\sqrt{8}} = \frac{1}{2\sqrt{2}}$$

$$\phi = -\tan^{-1}\omega/2$$

$$= -\tan^{-1}2/2$$

$$\Rightarrow \phi = -\tan^{-1}(1) = -45^\circ$$

$$\begin{aligned} \text{output} &= \frac{1}{2\sqrt{2}} \cos(2t + 20^\circ - 45^\circ) \\ &= \frac{1}{2\sqrt{2}} \cos(2t - 25^\circ) \end{aligned}$$

07. Ans: (c)

Sol: Initial slope = -40 dB/dec

Two integral terms $\left(\frac{1}{s^2}\right)$

$$\therefore \text{Part of TF} = G(s)H(s) = \frac{K}{s^2}$$

at $\omega = 0.1$

$$\begin{aligned} \text{change in slope} &= -20 - (-40) \\ &= 20^\circ \end{aligned}$$

$$\text{Part of TF} = G(s)H(s) = \frac{K\left(1 + \frac{s}{0.1}\right)}{s^2}$$

At $\omega = 10$ slope changed to -60 dB/dec

$$\begin{aligned} \text{Change in slope} &= -60 - (-20) \\ &= -40 \text{ dB/dec} \end{aligned}$$

$$\text{TF } (G(s)H(s)) = \frac{K\left(1 + \frac{s}{0.1}\right)}{s^2\left(\frac{s}{10} + 1\right)^2}$$



$$20 \log K - 2 (20 \log 0.1) = 20 \text{ dB}$$

$$20 \log K = 20 - 40$$

$$20 \log K = -20$$

$$K = 0.1$$

$$G(s)H(s) = \frac{(0.1) \left(1 + \frac{s}{0.1}\right)}{s^2 \left(1 + \frac{s}{10}\right)^2}$$

$$= \frac{(0.1) \times 10^2 (s + 0.1)}{(0.1)s^2 (s + 10)^2}$$

$$G(s)H(s) = \frac{100(s + 0.1)}{s^2 (s + 10)^2}$$

08. Ans: (b)

Sol: $G(s)H(s) = \frac{Ks}{\left(1 + \frac{s}{2}\right) \left(1 + \frac{s}{10}\right)}$

$$12 = 20 \log K + 20 \log 0.5$$

$$12 = 20 \log K + (-6)$$

$$20 \log K = 18 \text{ dB} = 20 \log 2^3$$

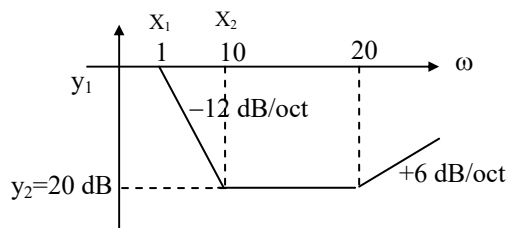
$$K = 8$$

$$G(s)H(s) = \frac{8s \times 2 \times 10}{(2 + s)(10 + s)}$$

$$G(s)H(s) = \frac{160s}{(2 + s)(10 + s)}$$

09. Ans: (b)

Sol:



$$G(s)H(s) = \frac{K \left(1 + \frac{s}{10}\right)^2 \left(1 + \frac{s}{20}\right)}{(1 + s)^2}$$

$$\frac{y_2 - y_1}{x_2 - x_1} = -40 \text{ dB/dec}$$

$$\frac{20 - y_1}{\log 10 - \log 1} = -40$$

$$y_1 = +60 \text{ dB} \big|_{\omega \leq 1}$$

$$\Rightarrow 20 \log K = 60$$

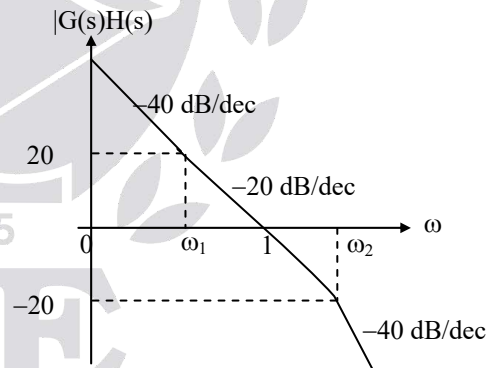
$$K = 10^3$$

$$G(s)H(s) = \frac{10^3 (s + 10)^2 (s + 20)}{10^2 \times 20 \times (s + 1)^2}$$

$$= \frac{(s + 10)^2 (s + 20)}{2(s + 1)^2}$$

10. Ans: (d)

Sol:



ω_1 calculation:

$$\frac{0 - 20}{\log 1 - \log \omega_1}$$

$$= -20 \text{ dB/dec}$$

$$\omega_1 = 0.1$$

ω_2 calculation:

$$\frac{-20 - 0}{\log \omega_2 - \log 1}$$



$$= -20\text{dB/dec}$$

$$\omega_2 = 10$$

$$G(s)H(s) = \frac{K \left(1 + \frac{s}{0.1}\right)}{s^2 \left(1 + \frac{s}{10}\right)}$$

$$20\log K - 2(20 \log 0.1) = 20$$

$$20 \log K = 20 - 40$$

$$K = 0.1$$

$$G(s)H(s) = \frac{0.1 \times \frac{1}{0.1} (0.1 + s)}{s^2 \frac{1}{10} (10 + s)}$$

$$= \frac{10(0.1 + s)}{s^2 (10 + s)}$$

11.

Sol: $\frac{200}{s(s+2)} = \frac{100}{s \left(1 + \frac{s}{2}\right)}$

$$x = -KT \Rightarrow -(100) \times \frac{1}{2} = x = -50$$

12. **Ans: (c)**

Sol: For stability $(-1, j0)$ should not be enclosed by the polar plot.

For stability

$$1 > 0.01 K$$

$$\Rightarrow K < 100$$

13.

Sol: $GM = -40 \text{ dB}$

$$20 \log \frac{1}{a} = -40 \Rightarrow a = 10^2$$

$$POI = 100$$

14.

Sol: (i) $GM = \frac{1}{0.1} = +10 = 20 \text{ dB}$

$$PM = 180^\circ - 140^\circ = 40^\circ$$

(ii) $PM = 180 - 150^\circ = 30^\circ$

$$GM = \frac{1}{0} = \infty \quad POI = 0$$

(iii) ω_{PC} does not exist

$$GM = \frac{1}{0} = \infty \quad PM = 180^\circ + 0^\circ = 180^\circ$$

(iv) ω_{gc} not exist

$$\omega_{pc} = \infty$$

$$GM = \frac{1}{0} = \infty$$

$$PM = \infty$$

(v) $GM = \frac{1}{0.5} = 2$

$$PM = 180 - 90 = 90^\circ$$

15. **Ans: (d)**

Sol: For stability $(-1, j0)$ should not be enclosed by the polar plot. In figures (1) & (2) $(-1, j0)$ is not enclosed.

$\therefore$ Systems represented by (1) & (2) are stable.

16. **Ans: (b)**

Sol: Open loop system is stable, since the open loop poles are lies in the left half of s-plane $\therefore P = 0$.

From the plot $N = -2$.

No. of encirclements $N = P - Z$

$N = -2, P = 0$ (Given)



$$\therefore N = P - Z$$

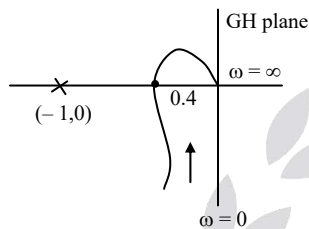
$$-2 = 0 - Z$$

$$Z = 2$$

Two closed loop poles are lies on RH of s-plane and hence the closed loop system is unstable.

17. Ans: (c)

Sol:

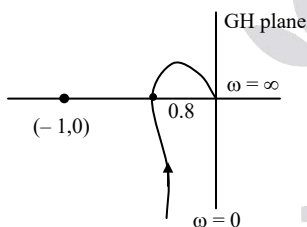


$$\frac{K_c}{K} = 0.4$$

When $K = 1$

$$\text{Now, } K \text{ double, } \frac{K_c}{K} = 0.4$$

$$K_c = 0.4 \times 2 = 0.8$$



even though the value of K is double, the system is stable (negative real axis magnitude is less than one)

Oscillations depends on 'ξ'

$$\xi \propto \frac{1}{\sqrt{K}} \text{ as } K \text{ is increased } \xi \text{ reduced, then}$$

more oscillations.

18. Ans: (a)

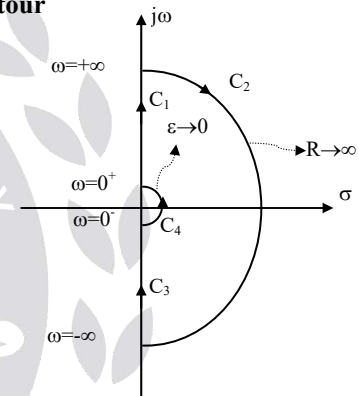
$$\text{Sol: Given system } G(s) = \frac{10(s-12)}{s(s+2)(s+3)}$$

It is a non minimum phase system since $s = 12$ is a zero on the right half of s-plane

19.

$$\text{Sol: Given that } G(s)H(s) = \frac{10(s+3)}{s(s-1)}$$

**s-plane
Nyquist Contour**



- Nyquist plot is the mapping of Nyquist contour(s-plane) into $G(s)H(s)$ plane.
- The Nyquist contour in the s-plane enclosing the entire right half of S-plane is shown figure.

The Nyquist Contour has four sections C_1 , C_2 , C_3 and C_4 . These sections are mapped into $G(s)H(s)$ plane

Mapping of section C_1 : It is the positive imaginary axis, therefore sub $s = j\omega$, ($0 \leq \omega \leq \infty$) in the TF $G(s)H(s)$, which gives the polar plot

$$G(s)H(s) = \frac{10(s+3)}{s(s-1)}$$

Let $s = j\omega$



$$G(j\omega)H(j\omega) = \frac{10(j\omega + 3)}{j\omega(j\omega - 1)}$$

$$G(j\omega)H(j\omega) = \frac{10\sqrt{\omega^2 + 9}}{\omega\sqrt{\omega^2 + 1}} \angle \{ \tan^{-1}\left(\frac{\omega}{3}\right) - [90^\circ + 180^\circ - \tan^{-1}(\omega)] \}$$

$$\text{At } \omega = 0 \Rightarrow \infty \angle -270^\circ$$

$$\text{At } \omega = \omega_{pc} = \sqrt{3} \Rightarrow 10 \angle -180^\circ$$

$$\text{At } \omega = \infty \Rightarrow 0 \angle -90^\circ$$

point of intersection of the Nyquist plot with respect to negative real axis is calculated below

$$\begin{aligned} \text{Arg } G(j\omega)H(j\omega) &= \arg \frac{10(j\omega + 3)}{j\omega(j\omega - 1)} \\ &= -180^\circ \text{ will give the } \omega_{pc} \end{aligned}$$

Magnitude of $G(j\omega)H(j\omega)$ gives the point of intersection

$$\begin{aligned} \angle \tan^{-1}\left(\frac{\omega}{3}\right) - [90^\circ + 180^\circ - \tan^{-1}(\omega)] \\ = -180^\circ \big|_{\omega = \omega_{pc}} \\ \angle \tan^{-1}\left(\frac{\omega_{pc}}{3}\right) - [90^\circ + 180^\circ - \tan^{-1}(\omega_{pc})] = -180^\circ \end{aligned}$$

$$\tan^{-1}\left(\frac{\omega_{pc}}{3}\right) + \tan^{-1}(\omega_{pc}) = 90^\circ$$

Taking "tan" both the sides

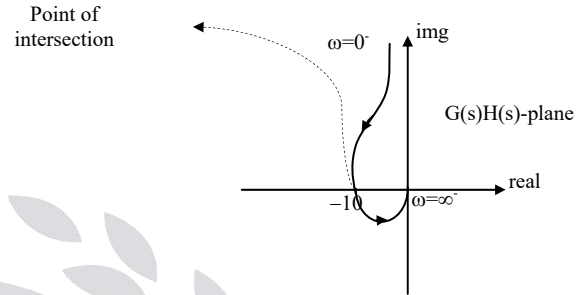
$$\frac{\frac{\omega_{pc}}{3} + \omega_{pc}}{1 - \frac{(\omega_{pc})^2}{3}} = \tan 90^\circ = \infty$$

$$1 - \frac{\omega_{pc}^2}{3} = 0$$

$$\omega_{pc} = \sqrt{3} \text{ rad/sec}$$

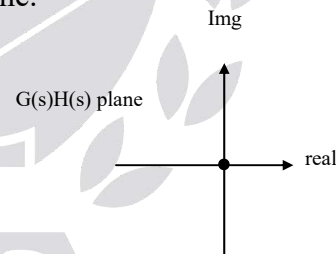
Therefore the point of intersection is

$$|G(j\omega)H(j\omega)| \text{ at } \omega_{pc} = \frac{10\sqrt{\omega_{pc}^2 + 3^2}}{\omega_{pc}\sqrt{1 + \omega_{pc}^2}} = 10$$



The mapping of the section C_1 is shown figure.

Mapping of section C_2 : It is the radius 'R' semicircle, therefore sub $s = \lim_{R \rightarrow \infty} R e^{j\theta}$ (θ is from 90° to 0° to -90°) in the TF $G(s)H(s)$, which merges to the origin in $G(s)H(s)$ plane.



$$G(s)H(s) = \frac{10(s + 3)}{s(s - 1)}$$

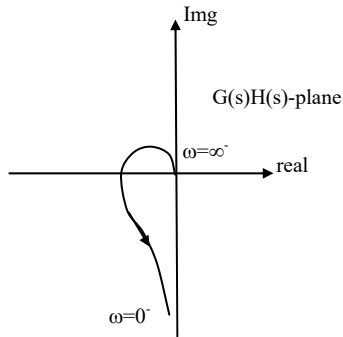
$$G(\text{Re}^{j\theta})H(\text{Re}^{j\theta}) = \frac{2(\text{Re}^{j\theta} + 3)}{\text{Re}^{j\theta}(\text{Re}^{j\theta} - 1)} \approx 0$$

The plot is shown in figure.

Mapping of section C_3 : It is the negative imaginary axis, therefore sub $s = j\omega$, ($-\infty \leq \omega \leq 0$) in the TF $G(s)H(s)$, which gives the mirror image of the polar plot and is symmetrical with respect to the real axis,



The plot is shown in figure.



Mapping of section C4: It is the radius 'ε' semicircle, therefore $\text{sub } s = \lim_{\epsilon \rightarrow 0} \epsilon e^{j\theta}$ ($-90^\circ \leq \theta \leq 90^\circ$) in the TF $G(s)H(s)$, which gives clockwise infinite radius semicircle in $G(s)H(s)$ plane.

The plot is shown below

$$G(\epsilon e^{j\theta})H(\epsilon e^{j\theta}) = \frac{10(\epsilon e^{j\theta} + 3)}{\epsilon e^{j\theta}(\epsilon e^{j\theta} - 1)}$$

$$G(\epsilon e^{j\theta})H(\epsilon e^{j\theta}) \approx \frac{10 \times 3}{-\epsilon e^{j\theta}} = \infty \angle 180^\circ - \theta$$

$$\text{When, } \theta = -90^\circ \quad \infty \angle 270^\circ$$

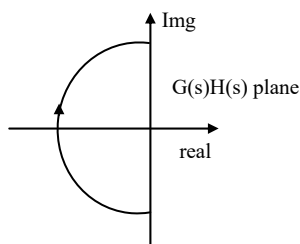
$$\theta = -40^\circ \quad \infty \angle 220^\circ$$

$$\theta = 0^\circ \quad \infty \angle 0^\circ$$

$$\theta = 40^\circ \quad \infty \angle 140^\circ$$

$$\theta = 90^\circ \quad \infty \angle 90^\circ$$

It is clear that the plot is clockwise '∞' radius semicircle centred at the origin



Combining all the above four sections, the

$$\text{Nyquist plot of } G(s)H(s) = \frac{10(s+3)}{s(s-1)}$$

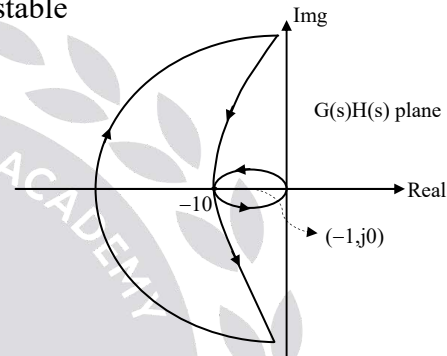
is shown in figure below

From the plot $N=1$

Given that $P=1$

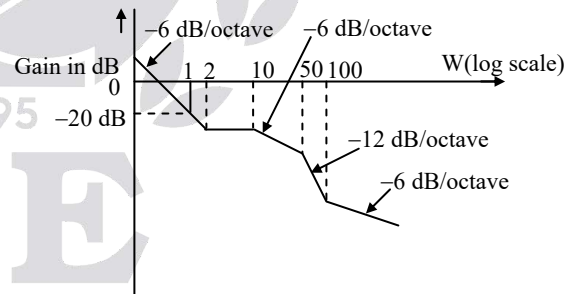
$$N=P-Z$$

$Z = P - N = 1 - 1 = 0$, therefore system is stable



20.

Sol: The given bode plot is shown below.



Initial slope = -6 db/octave.

i.e. there is one pole at origin (or) one integral term.

portion of transfer function

$$G(s) = \frac{K}{s}$$

At $\omega = 2$ rad/sec, slope is changed to 0dB/octave.



$\therefore$ change in slope = present slope
– previous slope
 $= 0 - (-6) = 6 \text{ dB/octave}$

$\therefore$ There is a real zero at corner frequency
 $\omega_1 = 2.$

$$(1 + sT_1) = \left(1 + \frac{s}{\omega_1}\right) = \left(1 + \frac{s}{2}\right)$$

At $\omega = 10 \text{ rad/sec}$, slope is changed to
 $-6 \text{ dB/octave}.$

$\therefore$ change in slope = $-6 - 0$
 $= -6 \text{ dB/octave}.$

$\therefore$ There is a real pole at corner frequency
 $\omega_2 = 2.$

$$\frac{1}{1 + sT_2} = \frac{1}{\left(1 + \frac{s}{\omega_2}\right)} = \frac{1}{\left(1 + \frac{s}{10}\right)}$$

At $\omega = 50 \text{ rad/sec}$, slope is changed to
 $-12 \text{ dB/octave}.$

$\therefore$ change in slope = $-12 - (-6)$
 $= -6 \text{ dB/octave}$

$\therefore$ There is a real pole at corner frequency
 $\omega_3 = 50 \text{ rad/sec}.$

$$\frac{1}{1 + sT_3} = \frac{1}{\left(1 + \frac{s}{\omega_3}\right)} = \frac{1}{\left(1 + \frac{s}{50}\right)}$$

At $\omega = 100 \text{ rad/sec}$, the slope changed to -6
 $\text{dB/octave}.$

$\therefore$ change in slope = $-6 - (-12) = 6$
 $\text{dB/octave}.$

$\therefore$ There is a real zero at corner frequency
 $\omega_4 = 100 \text{ rad/sec}.$

$$\therefore (1 + sT_4) = \left(1 + \frac{s}{\omega_4}\right) = \left(1 + \frac{s}{100}\right)$$

$$\therefore \text{Transfer function} = \frac{K \left(1 + \frac{s}{2}\right) \left(1 + \frac{s}{100}\right)}{s \left(1 + \frac{s}{50}\right) \left(1 + \frac{s}{10}\right)}$$

$$= \frac{K(s+2)(s+100)}{s(s+50)(s+10)} \cdot \frac{1}{2} \cdot \frac{1}{10}$$

$$= \frac{2.5K(s+2)(s+100)}{s(s+10)(s+50)}$$

In the given bode plot,

at $\omega = 1 \text{ rad/sec}$, Magnitude = $-20 \text{ dB}.$

$$\begin{aligned} -20 \text{ dB} &= 20 \log K - 20 \log \omega + 20 \sqrt{1 + \left(\frac{\omega}{2}\right)^2} + 20 \sqrt{1 + \left(\frac{\omega}{100}\right)^2} \\ &\quad - 20 \log \sqrt{1 + \left(\frac{\omega}{50}\right)^2} - 20 \log \sqrt{1 + \left(\frac{\omega}{10}\right)^2} \end{aligned}$$

At $\omega = 1 \text{ rad/sec}$,

$$-20 = 20 \log K - 20 \log \omega / \omega = 1 \text{ rad/sec}$$

[$\therefore$ Remaining values eliminated]

$$-20 = 20 \log K$$

$$\Rightarrow K = 0.1$$

$\therefore$ Transfer function

$$\frac{C(s)}{R(s)} = \frac{0.25(s+2)(s+100)}{s(s+10)(s+50)}$$

7. Controllers & Compensators

01. Ans: (a)

$$\begin{aligned} \text{Sol: } G_C(s) &= (-1) \left(-\frac{Z_2}{Z_1} \right) \\ &= (-1)(-1) \left(\frac{R_2 + \frac{1}{sC}}{R_1} \right) \end{aligned}$$



$$G_c(s) = \frac{(100 \times 10^3) + \frac{1}{s \times 10^{-6}}}{10^6}$$

$$G_c(s) = \frac{1 + 0.1s}{s}$$

02. Ans: (c)

Sol: CE $\Rightarrow 1 + G_c(s) G_p(s) = 0$

$$= 1 + \frac{1 + 0.1s}{s} \times \frac{1}{(s+1)(1+0.1s)}$$

$$= 1 + \frac{1 + 0.1s}{s(s+1)(1+0.1s)} = 0$$

$$\Rightarrow s^2 + s + 1 = 0 \Rightarrow \omega_n = 1,$$

$$e^{\left[\frac{-\xi\pi}{\sqrt{1-\xi^2}} \right]_{\xi=0.5}} = 0.163$$

$$M_p = 16.3\%$$

03. Ans: (b)

Sol: T.F = $\frac{k(1+0.3s)}{1+0.17s}$

$$T = 0.17, aT = 0.3 \Rightarrow a = \frac{0.3}{0.17}$$

$$C = 1 \mu F$$

$$T = \frac{R_1 R_2}{R_1 + R_2} C, a = \frac{R_1 + R_2}{R_2}$$

$$\frac{R_1 R_2}{R_1 + R_2} = \frac{0.17}{1 \times 10^{-6}} = 170000$$

$$\frac{R_1 + R_2}{R_2} = 1.764$$

$$aT = R_1 C$$

$$R_1 = \frac{aT}{C} = \frac{0.3}{C} = (0.3)(10^6)$$

$$= 300 \text{ k}\Omega$$

Bv

$$300 \text{ k} + R_2 - 1.76 R_2 = 0$$

$$R_2 = \frac{300}{0.70} = 394.736$$

$$= 400 \text{ k}\Omega$$

04. Ans: (d)

Sol: PD controller improves transient stability and PI controller improves steady state stability. PID controller combines the advantages of the above two controllers.

05.

Sol: For $K_I = 0 \Rightarrow$

$$\frac{C(s)}{R(s)} = \frac{(K_p + K_D s)}{s(s+1) + (K_p + K_D s)}$$

$$= \frac{K_p + K_D s}{s^2 + (1 + K_D)s + K_p}$$

$$\omega_n = \sqrt{K_p}$$

$$2\xi\omega_n = 1 + K_D$$

$$\Rightarrow 2(0.9) \sqrt{K_p} = 1 + K_D$$

$$\Rightarrow 1.8 \sqrt{K_p} = 1 + K_D \quad \dots\dots\dots (1)$$

$$\text{Dominant time constant } \frac{1}{\xi\omega_n} = 1$$

$$\Rightarrow \omega_n = \frac{1}{0.9} = 1.111$$

$$K_p = \omega_n^2 = 1.11^2$$

$$= 1.234$$

From eq. (1),

$$\Rightarrow 1.8 \times \frac{1}{0.9} = 1 + K_D$$

$$\Rightarrow K_D = 1$$



8. State Space Analysis

01. Ans: (a)

Sol: $TF = \frac{1}{s^2 + 5s + 6}$

$$= \frac{1}{(s+2)(s+3)}$$

$$= \frac{1}{s+2} + \frac{-1}{s+3}$$

$$\therefore A = \begin{bmatrix} -2 & 0 \\ 0 & -3 \end{bmatrix} \quad B = \begin{bmatrix} 1 \\ -1 \end{bmatrix}$$

$$C = [1 \quad 1]$$

02. Ans: (c)

Sol: Given problem is Controllable canonical form.

(or)

$$TF = C[sI - A]^{-1}B + D$$

$$= [6 \quad 5 \quad 1] \begin{bmatrix} s & 1 & 0 \\ 0 & s & 1 \\ -5 & -3 & s+6 \end{bmatrix}^{-1} \begin{bmatrix} 0 \\ 0 \\ 3 \end{bmatrix}$$

$$= \frac{3s^2 + 15s + 18}{s^3 + 6s^2 + 3s + 5}$$

03. Ans: (d)

Sol: $\frac{d^2y}{dt^2} + \frac{3dy}{dt} + 2y = u(t)$

2nd order system hence two state variables are chosen

Let $x_1(t)$, $x_2(t)$ are the state variables

CCF – SSR

$$\text{Let } x_1(t) = y(t) \dots\dots\dots (1)$$

$$x_2(t) = \dot{y}(t) \dots\dots\dots (2)$$

Differentiating (1)

$$\dot{x}_1(t) = \dot{y}(t) = x_2(t) \dots\dots\dots (3)$$

$$\begin{aligned} \dot{x}_2(t) &= \ddot{y}(t) = u(t) - 3\dot{y}(t) - 2y(t) \\ &= u(t) - 3x_2(t) - 2x_1(t) \dots\dots\dots (4) \end{aligned}$$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \underbrace{\begin{bmatrix} 0 & 1 \\ -2 & -3 \end{bmatrix}}_A \underbrace{\begin{bmatrix} x_1 \\ x_2 \end{bmatrix}}_B + \underbrace{\begin{bmatrix} 0 \\ 1 \end{bmatrix}}_B u(t)$$

From equation 1. The output equation in matrix form

$$y(t) = [1 \quad 0] \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}, D = 0$$

04. Ans: (b)

Sol: OCF – SSR

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & -2 \\ 1 & -3 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 1 \\ 0 \end{bmatrix} u(t)$$

$$y(t) = [0 \quad 1] \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

05. Ans: (c)

Sol: Normal form – SSR

$$TF = \frac{Y(s)}{G(s)} = \frac{1}{s^2 + 3s + 2} = \frac{1}{(s+1)(s+2)}$$

$\Rightarrow$ Diagonal canonical form

The eigen values are distinct i.e., -1 & -2 .

$\therefore$ Corresponding normal form is called as diagonal canonical form

DCF – SSR

$$\frac{Y(s)}{U(s)} = \frac{b_1}{s+1} + \frac{b_2}{s+2}$$

$$b_1 = 1, b_2 = -1$$

$$Y(s) = \underbrace{\frac{b_1}{s+1}}_{x_1} U(s) + \underbrace{\frac{b_2}{s+2}}_{x_2} U(s)$$



Let $Y(s) = X_1(s) + X_2(s)$

Where $y(t) = x_1(t) + x_2(t) \dots\dots\dots (1)$

Where $X_1(s) = \frac{b_1}{s+1} U(s)$

$s X_1(s) + X_1(s) = b_1 U(s)$

Take Laplace Inverse

$\dot{x}_1 + x_1 = b_1 u(t) \dots\dots\dots (2)$

$X_2(s) = \frac{b_2}{s+2} U(s)$

$s X_2(s) + 2 X_2(s) = b_2 U(s)$

Laplace Inverse

$\dot{x}_2 + 2x_2 = b_2 u(t)$

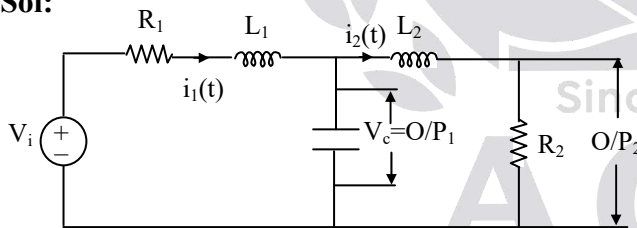
$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -1 & 0 \\ 0 & -2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 1 \\ -1 \end{bmatrix} u(t)$$

From(1) output equation.

$$y(t) = \begin{bmatrix} 1 & 1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

06. Ans: (c)

Sol:



$O/P_1 \Rightarrow y_1 = V_c$

$O/P_2 \Rightarrow y_2 = R_2 i_2$

$$y = \begin{bmatrix} y_1 \\ y_2 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 0 & R_2 \end{bmatrix} \begin{bmatrix} V_c \\ i_1 \\ i_2 \end{bmatrix}$$

$y = C X$

$$C = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 0 & R_2 \end{bmatrix}$$

07. Ans: (a)

Sol: T.F = $C[sI-A]^{-1}B + D$

$$= \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} s+4 & 1 \\ 3 & s+1 \end{bmatrix}^{-1} \begin{bmatrix} 1 \\ 1 \end{bmatrix}$$

$$= \begin{bmatrix} 1 & 0 \end{bmatrix} \frac{1}{s^2 + 5s + 1} \begin{bmatrix} s+1 & -1 \\ -3 & s+4 \end{bmatrix} \begin{bmatrix} 1 \\ 1 \end{bmatrix}$$

$$= \frac{1}{s^2 + 5s + 1} \begin{bmatrix} 1 & 0 \end{bmatrix}_{1 \times 2} \begin{bmatrix} s+1 & -1 \\ -3 & s+4 \end{bmatrix}_{2 \times 2} \begin{bmatrix} 1 \\ 1 \end{bmatrix}_{2 \times 1}$$

$$= \frac{1}{s^2 + 5s + 1} \begin{bmatrix} s+1 & -1 \end{bmatrix}_{1 \times 2} \begin{bmatrix} 1 \\ 1 \end{bmatrix}_{2 \times 1}$$

$$= \frac{1}{s^2 + 5s + 1} [s+1-1]$$

$$= \frac{s}{s^2 + 5s + 1}$$

08. Ans: (c)

Sol: State transition matrix $\phi(t) = L^{-1}[(sI-A)^{-1}]$

$$sI - A = \begin{bmatrix} s+3 & -1 \\ 0 & s+2 \end{bmatrix}$$

$$[sI - A]^{-1} = \frac{1}{(s+2)(s+3)} \begin{bmatrix} s+2 & 1 \\ 0 & s+3 \end{bmatrix}$$

$$= \begin{bmatrix} \frac{1}{s+3} & \frac{1}{(s+2)(s+3)} \\ 0 & \frac{1}{s+2} \end{bmatrix}$$

$$L^{-1}[[sI - A]^{-1}] = \begin{bmatrix} e^{-3t} & e^{-2t} - e^{-3t} \\ 0 & e^{-2t} \end{bmatrix}$$

09. Ans: (b)

Sol: Controllability

$$[M] = [B \quad AB \quad A^2B \dots A^{n-1}B]$$

$$AB = \begin{bmatrix} 0 & 1 \\ -2 & -3 \end{bmatrix} \begin{bmatrix} 0 \\ 1 \end{bmatrix} = \begin{bmatrix} 1 \\ -3 \end{bmatrix}$$



$$\Rightarrow \begin{vmatrix} S & -1 & 0 \\ 0 & S & -1 \\ 0 & 2 & S+3 \end{vmatrix} = 0$$

$$\Rightarrow s[s(s+3)+2]+1(0)=0$$

$$\Rightarrow s(s^2+3s+2)=0$$

$$\Rightarrow s(s+1)(s+2)=0$$

The roots are 0, -1, -2.

9. Mathematical Modeling of Mechanical Systems

01. Ans: (c)

$$\text{Sol: } M \frac{d^2 x_0}{dt^2} + B_2 \frac{dx_0}{dt} + B_1 \frac{d}{dt}(x_0 - x_i) = 0$$

$$(Ms^2 + B_2s + B_1s)X_0 = B_1sX_i$$

$$\frac{X_0(s)}{X_i(s)} = \frac{B_1}{Ms + B_1 + B_2}$$

02. Ans: (a)

$$\text{Sol: } \frac{\theta_1}{\theta_2} = \frac{N_2}{N_1} = \frac{T_2}{T_1}$$

$$T_2 = J_2 \ddot{\theta}_2 + B_2 \dot{\theta}_2$$

$$T_2 = J_2 \left(\frac{N_1}{N_2} \right) \ddot{\theta}_1 + B_2 \frac{N_1}{N_2} \dot{\theta}_1$$

$$T_1 = \frac{N_1}{N_2} T_2$$

$$= \frac{N_1}{N_2} \left[J_2 \left(\frac{N_1}{N_2} \right) \ddot{\theta}_1 + B_2 \left(\frac{N_1}{N_2} \right) \dot{\theta}_1 \right]$$

$$= J_2 \left(\frac{N_1}{N_2} \right)^2 \ddot{\theta}_1 + B_2 \left(\frac{N_1}{N_2} \right)^2 \dot{\theta}_1$$

03. Ans: (c)

Sol: For each variable one equation is written.

For the given system there are two variables and hence two differential equations.

At node x_1 :

$$F = M_1 \frac{d^2 x_1}{dt^2} + B_{12} \frac{d}{dt}(x_1 - x_2) + (k_{12} + k_1)(x_1 - x_2)$$

At node x_2 :

$$0 = M_2 \frac{d^2 x_2}{dt^2} + B_2 \frac{dx_2}{dt} + k_2 x_2 + B_{12} \frac{d}{dt}(x_2 - x_1) + (k_1 + k_{12})(x_2 - x_1)$$

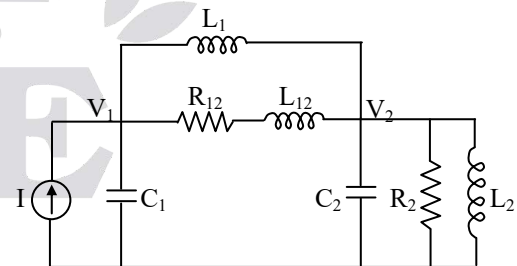
F-I analogy:

Corresponding F-I analogy equations for the above mechanical network is,

$$I = C_1 \frac{dV_1}{dt} + \frac{1}{R_{12}}(V_1 - V_2) + \left(\frac{1}{L_{12}} + \frac{1}{L_1} \right) \int (V_1 - V_2) dt$$

$$0 = C_2 \frac{dV_2}{dt} + \frac{1}{R_2}(V_2) + \frac{1}{L_2} \int V_2 dt + \frac{1}{R_{12}}(V_2 - V_1) + \left(\frac{1}{L_1} + \frac{1}{L_{12}} \right) \int (V_2 - V_1) dt$$

Therefore the corresponding electrical network with two nodes is written below.



04. Ans: (c)

$$\text{Sol: } \delta(t) = m \frac{d^2 x}{dt^2} + kx$$

$$1 = ms^2 X(s) + kX(s)$$

$$1 = (ms^2 + k)X(s)$$



$$X(s) = \frac{1}{ms^2 + k}$$

$$X(s) = \frac{\frac{1}{m}}{s^2 + \frac{k}{m}} = \frac{\frac{1}{m} \sqrt{\frac{k}{m}} \sqrt{\frac{m}{k}}}{s^2 + \left(\sqrt{\frac{k}{m}}\right)^2}$$

$$x(t) = \frac{1}{\sqrt{mk}} \sin\left(\sqrt{\frac{k}{m}} \cdot t\right)$$

05. Ans: (b)

Sol: $M \frac{d^2x}{dt^2} + f \frac{dx}{dt} + (K_1 + K_2)x = F$

$$\frac{X(s)}{F(s)} = \frac{1}{Ms^2 + fs + K_1 + K_2}$$

06. Ans: (b)

Sol: In force current analogy

$$F \rightarrow i$$

$$M \rightarrow C$$

$$B \rightarrow \frac{1}{R}$$

$$K \rightarrow \frac{1}{L}$$

10. Process Dynamics

01. Ans: (c)

Sol: For any first order instrument like thermocouple, the time to reach 98% of steady state value is equal to 4 times Time constant.

$$0.98 T_0 = T_0 (1 - e^{-t/\tau})$$

$$0.98 = (1 - e^{-t/\tau})$$

$$t = 4 \tau$$

02. Ans: (c)

Sol: Error is measurement when a ramp of magnitude 'K' is applied is

$$e_{ss} = K \tau$$

Where τ = time constant = 100 m sec;

$$e_{ss} = \frac{1^\circ \text{C}}{\text{sec}} \times 100 \times 10^{-3} \text{ sec}$$

$$= 0.1^\circ \text{C}$$

$\therefore$ The reading of thermocouple will be
 $= 70^\circ \text{C} - 0.1^\circ \text{C} = 69.9^\circ \text{C}$

03. Ans: (c)

Sol: $96.5 = 100(1 - e^{-t/\tau}) + 30(e^{-t/\tau})$

$$96.5 = 100 + e^{-30/\tau} (30 - 100)$$

$$\tau = 10.01 \text{ sec}$$

$$98 = 100(1 - e^{-t/10}) + 30 e^{-t/10}$$

$$e^{-t/10} (30 - 100) + 100 = 98$$

$$t = 35.6 \text{ sec}$$

04. Ans: (a)

Sol: $2 \frac{dT_i}{dt} + T_i - T_a = 0$

By applying Laplace Transform on both sides.

$$2sT_i(s) + T_i(s) - T_a(s) = 0.$$

$$T_i(s) [2s+1] = T_a(s)$$

$$\frac{T_i(s)}{T_a(s)} = \frac{1}{2s+1}$$

$$\frac{T_i(s)}{T_a(s)} = \frac{0.5}{s+0.5}$$

Here cut-off frequency

$$\omega_c = 0.5 = \frac{1}{2}$$

$$\text{or } 2\pi f_c = \frac{1}{2}$$

$$f_c = \frac{1}{4\pi} \text{ Hz}$$



11. Controller Tuning

01. Ans: (b)

Sol: $K_u = 10$

$P_u = 8\text{Hz}$

In case of Ziegler Nichols tuning for proportional controller

$K_P = 0.5 K_u = 0.5 \times 10 = 5.$

02. Ans: (a)

Sol: Distance between the roll point and the point at which the thickness is measured

$$= d = 0.5 \text{ m}$$

$v = \text{velocity of the sheet} = 0.2 \text{ m/s}$

$$\text{delay} = \frac{d}{v} = \frac{0.5}{0.2} = 2.5 \text{ sec}$$

$$\therefore \text{T.F} = e^{-2.5 s}$$

03. Ans: (c) & (d)

Sol: $\text{OLTF} = K e^{-2.5 s}$

$$\angle \text{OLTF} = -2.5 \omega, |\text{OLTF}| = K$$

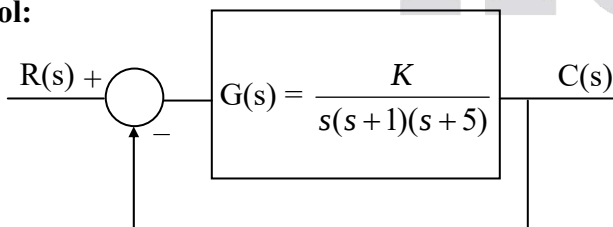
Ultimate value of K for stability = 1

$$-2.5 \omega = -\pi,$$

$$\omega = \frac{\pi}{2.5} = 0.4 \pi \text{ rad/sec}$$

04. Ans: (c)

Sol:



Characteristics equation

$$1 + \frac{k}{s(s+1)(s+5)} = 0$$

$$s^3 + 6s^2 + 5s + K = 0$$

By R-H criteria

$$s^3 \quad 1 \quad 5$$

$$s^2 \quad 6 \quad K$$

$$s^1 \quad \frac{30-k}{6} \quad 0$$

$$s^0 \quad K$$

$$K_u = 30$$

As, $0 < K < 30$ stable

$$6s^2 + k = 0$$

$$6s^2 + 30 = 0$$

$$s^2 = -30/6 = -5$$

$$s = \pm j\sqrt{5}$$

12. Control Strategies

01.

Sol: a) For, $U(s) = 0$

By, mason's gain formula

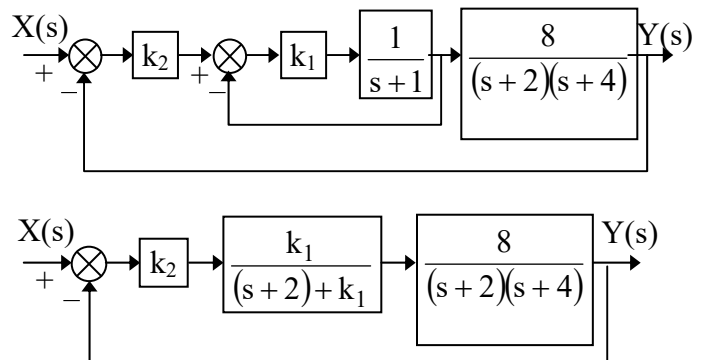
$$\frac{Y(s)}{W} = \frac{G_p(s)[1 + G_f(s)G_c(s)]}{1 + G_p(s)H(s)G_c(s)}$$

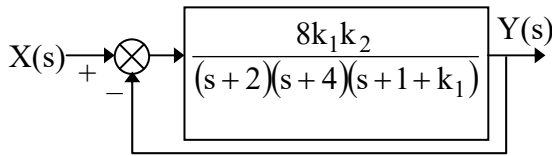
b) In order to eliminate the effect of W .

$$G_f(s) = -\frac{1}{G_c(s)}$$

02. Ans: (d)

Sol:





$$\frac{Y(s)}{X(s)} = \frac{8k_1k_2}{(s+2)(s+4)(s+1+k_1) + 8k_1k_2}$$

Thus, characteristics equation is

$$(s+2)(s+4)(s+1+k_1) + 8k_1k_2 = 0$$

$$s^3 + (7+k_1)s^2 + (14+6k_1)s + 8 + 8k_1 + 8k_1k_2 = 0$$

According to R-H array

$$\begin{array}{l|l} s^3 & 1 & 14+6k_1 \\ s^2 & 7+k_1 & 8(1+k_1+k_1k_2) \\ s^1 & \frac{(7+k_1)(14+6k_1) - 8(1+k_1+k_1k_2)}{7+k_1} & 0 \\ s^0 & 8(1+k_1+k_1k_2) & 0 \end{array}$$

For stable system, all the elements of first column should be greater than zero. By substituting all the given options in coefficient of s^1 will give negative and zero values except option (d).

03. Ans: (d)

Sol: Applying Mason's gain formula

$$TF = \frac{Y(s)}{D(s)} = \frac{1 + K \cdot \frac{1}{s+2}}{1 - \left[50 \cdot \frac{1}{s+2} (-1) \right]} = 0$$

$$1 + K \cdot \frac{1}{s+2} = 0$$

$$s+2 + K = 0$$

$$K = -(s+2)$$

At frequency ($\omega = 0$)

$$K = -2$$

13. Control Valves

01.

Sol: $P = 24 \times 0.433$
 $= 10.392 \text{ Psi}$

We know for valve

$$C_v = Q \sqrt{\frac{G}{\Delta P}}$$

Where, Q = flow rate

ΔP = differential pressure across the valve.

G = Specific gravity of water

So,

$$C_v = 120 \sqrt{\frac{1}{10.392}}$$

$$= 37.22$$

02.

Sol: Maximum out flow = maximum inflow
 $= 120 \text{ gpm}$

$$\Delta P = (26-24) \times (0.433)$$

$$= 5.196 \text{ Psi}$$

So, $C_v = Q \sqrt{\left(\frac{G}{\Delta P} \right)}$

$$= 120 \sqrt{\left(\frac{1}{5.19} \right)}$$

$$= 52.67$$